

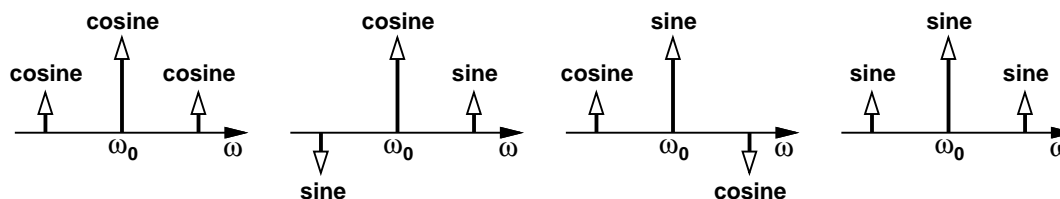
# RF Microelectronics, Second Edition

## Errata

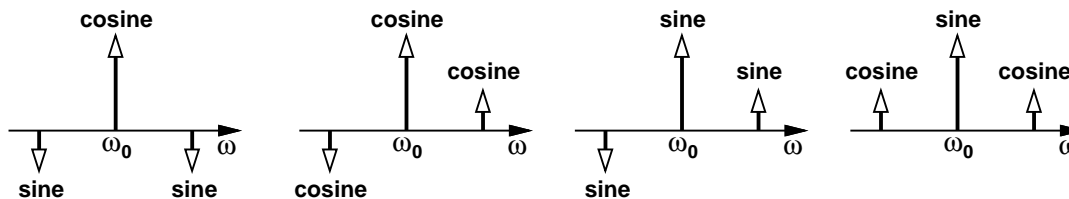
Behzad Razavi

- Example 2.11, change Eq. (2.53) to  $3.16 V_p$  and Eq. (2.54) to  $+20$  dBm.
- On page 40, last paragraph, the noise current of a resistor should read  $\overline{I_n^2} = \overline{V_n^2}/R_1^2$ .
- Prob. 2.3, second line should read: consider the cascade of identical ...
- Prob. 2.5 should read  $\omega_3 - \omega_2 = \omega_2 - \omega_1$ .
- Fig. 3.9 should be changed as shown below:

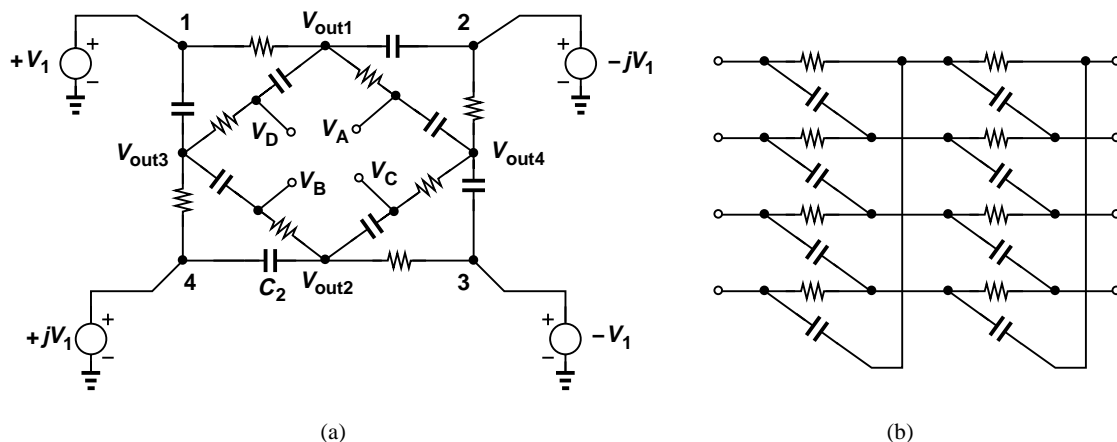
AM



NBFM



- In the first paragraph of Section 3.3.3, change the last sentence to ... decrease this bandwidth to about  $1/T_b$ .
- On page 115, in the paragraph starting with “The concept of QAM ...” change eight to six.
- In Fig. 4.15(b), change  $2\omega_{in} - \omega_{LO}$  to  $2\omega_{LO} - \omega_{in}$ .
- In Example 4.27, page 202, change  $\exp(-j\omega_c t)$  to  $\exp(+j\omega_c t)$ .
- Fig. 4.81(a) should be changed as shown on the next page.
- Example 4.36, the first sentence in solution should read: We have  $V_{out1} = (1/2)(1 - j)V_1$  and ...



- Example 5.5, third line in solution: Since it is desired that  $R_{in} = R_S$ ,
- The  $R_S$  in the denominators of (5.96) and (5.100) must be multiplied by  $j$ .
- On page 349, first paragraph, change Fig. 6.16(b) to Fig. 6.16.
- In Fig. 6.14(b), the spectral density on the right should change from  $2kTR_S$  to  $kTR_S$ .
- Equation (6.65) should read:

$$R_{D,max} = \frac{V_{R,max}}{I_{D1}} \quad (1)$$

because  $R_D$  carries all of the tail current under this condition. Equations (6.67), (6.68), and (6.69) should also be scaled down by a factor of 2.

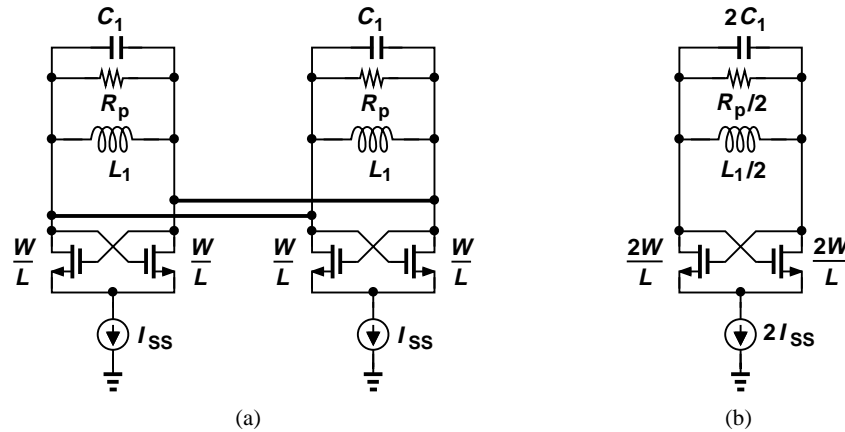
- Example 6.21, last three lines of solution: Note that  $V_{n2}(f)$  is typically very large because  $M_2$  and  $M_3$  are relatively small.
- Example 7.6, Eq. (7.33) should read:

$$C_{eq} = \frac{C_1 + \dots + C_{4(N-1)}}{[4(N-1)]^2} \quad (2)$$

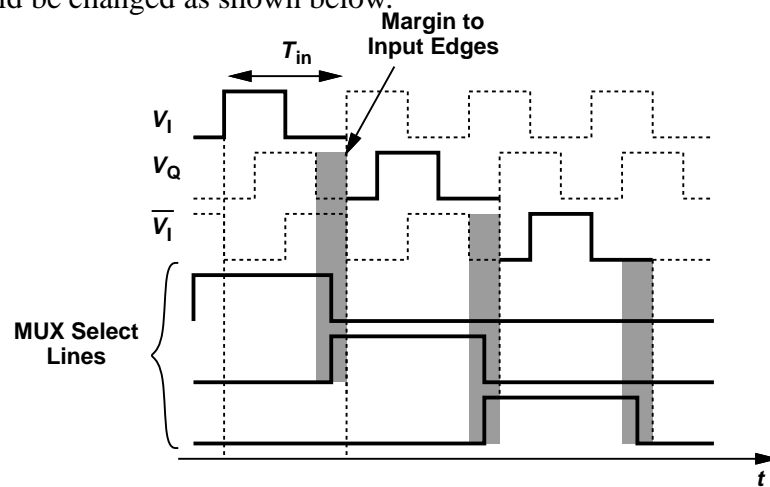
Eq. (7.125) in Problem 7.3 must also be corrected as above.

- The line above Eq. (7.48) should read: equal to  $K|I_{u,n}|^2 R_{sub}$ .
- p. 488, the sentence below Eq. (7.114) should read  $Z_{1d} = R_{tot}/2$  and  $Y_{1d} = C_{tot}s/2$ .
- Prob. 7.10, Assume the inductance is about 9 times that of one spiral.
- Eq. (8.5): the sign before the second fraction should change from positive to negative.

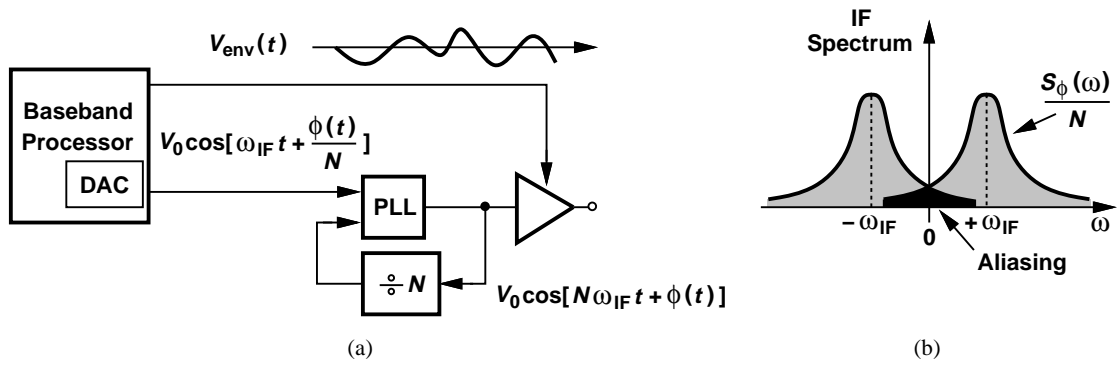
- In Eq. (8.19), change  $\phi_0$  to  $\phi_1$ .
- In the sentence above Eq. (8.43), change rad/Hz/V to rad/s/V.
- Fig. 8.84 (b) should be changed as shown on the next page.



- The inverting and non-inverting inputs of  $A_0$  in Fig. 9.53 should be swapped (because  $C_X$  is usually much less than  $C_1 + C_2$  and hence the feedback loop on the left dominates).
- The denominator of (10.75) should read  $N_s$  rather than  $NS$ .
- Fig. 11.45 should be changed as shown below.



- Fig. 12.53(b) should be changed as shown below.
- Problem 12.3 should read: Prove that in Fig. 12.17, the voltage swings above and below  $V_{DD}$  are equal to  $V_p/\pi$  and  $V_p(\pi - 1)/\pi$ , respectively, where  $V_p$  denotes the peak voltage at each node. (Hint: the average value of  $V_X$  and  $V_Y$  must be equal to  $V_{DD}$ .)
- In the solution of Example 13.1, the second line should read: However, a 64QAM OFDM signal exhibits ... . And the last sentence should read: The  $-82$ -dBm PSK OFDM signal



has roughly the same behavior. Note that this correction affects the gain calculations after this example.

- In Figs. 13.17, 13.19, and 13.22, change the length of the baseband PMOS devices from 1.2 to 0.12.