### Non-Volatile Chlorinated Organics Produced During Disinfection of Reclaimed Wastewaters

by

Michael K. Stenstrom, Ph.D. Professor

Sami A. Fam, Ph.D. Postgraduate Research Engineer

J.B. Neethling, Ph.D. Assistant Professor

Civil Engineering Department

A Final Report to the Department of Water Resources for Contract B-54863

UCLA-Eng 87-10

April 1987

# TABLE OF CONTENTS

.

Ι.	INTRODUCTION1				
II.	LII	ERATURE REVIEW	5		
	1.	BASIC CHLORINE CHEMISTRY AND DISINFECTION	5		
		<ul> <li>1.1 Dissociation of Chlorine</li></ul>	5 7 0 1		
	2.	ANALYSIS OF ORGANICS IN WATER BY GC AND GC/MS1	3		
	3.	VOLATILE CHLORINATED ORGANICS1	5		
		<ul> <li>3.1 Haloform Precursors</li></ul>	5 0 8		
	4.	NON-VOLATILE CHLORINATED ORGANICS (NVCO)	1		
		<ul> <li>4.1 Measurement of NVCO as TOX</li></ul>	2 5 6		
		<ul> <li>4.5 Precursors to NVCO</li></ul>	6 6 9		

٦,

	5.	LITI	ERATURE REVIEW SUMMARY	.50
III.	٥V	/ERVI	EW AND PROCEDURES	.52
	1.	OVE EX	ERVIEW OF EXPERIMENTAL TECHNIQUES AND PERIMENTS	.52
	2.	DES TR	CRIPTION OF THE SAN DIEGO WASTEWATER EATMENT PLANT	.56
	3.	ANA	ALYTICAL PROCEDURES	.59
		21	Extractable Organic Analysis	50
		2.1	Laboratory Chloringtion of Water Samples	62
		3.2 3 3	Chloringtion of Extracts	64
		3.5	Silica Gel Column Chromatography	65
		3.5	XAD8 Adsorption	65
		3.6	Illtrafiltration	66
		37	Chloringtion of Pure Compounds	.67
		3.8	Addition of Sodium Sulfite to Pure	
		5.0	Compounds	.67
		39	TOC and Gravimetric Analysis	67
		3 10	Other Procedures	68
		3.11	Reagents	.68
IV.	RE	SULT	'S AND DISCUSSION	.70
	1.	SOL	VENT EXTRACTABLE ORGANICS AT SAN DIEGO	)
		(BA	CKGROUND ORGANICS)	.70
	2.	IDEN GC/	TIFICATION OF SOME OF THE NVCO BY MS	. <b>9</b> 0
	3.	PREC	CURSORS TO THE OBSERVED NVCO1	05
		3.1	Chlorination of XAD8 Extracts from the	06
		2 7	Aquatuluit Elliptic of $C U C I$ Extracto	00
		3.2 2 2	Laboratory Chloridation of $CH_2Ct_2$ Extracts	07
		5.5	Dreamon Collection - 1	12
				14

τ.

	3.4	Chlorination of Organic Solvent Eluted Fractions	
		from XAD8 Columns	113
	3.5	Chlorination of Humic/Fulvic Fractions	114
	3.6	Chlorination of Two pH Eluates from XAD8	
		Columns	116
	3.7	Chlorination of Ultrafiltration Fractions	116
	38	Chlorination of XAD Extracts from other	
	5.0	Treatment Plants	
	3.9	Chlorination of Pure Compounds	122
4.	EFF	ECT OF CHLORINATION PARAMETERS ON TH	Æ
	PR	ODUCTION OF THE NVCO	137
	4.1	Effect of Chlorine Dose	137
	4.2	Effect of Contact Time	139
	43	Effects of pH	143
	ΔΔ	Effect of Bromide	143
	45	Summary of the Effects of the Chlorination	
	-1.2	Variables	148
5.	EFF	ECTS OF DECHLORINATING AGENTS	151
	5.1	Addition of Sodium Sulfite to Pure	
		Halogenated Compounds	152
	5.2	Addition of Sodium Sulfite to the	
		Chlorinated Effluent	154
	5.3	Addition of Sodium Sulfite to Chlorinated	
		XAD8 Extract	157
	5.4	Summary of the Effects of Sodium Sulfite	157
6.	TRE	EATMENT OF THE OBSERVED HALOGENATED	)
	OF	RGANICS	162
	6.1	Treatment with Powdered Activated Carbon	162
	6.2	Chloramines	163
	6.3	Aeration	167
	6.4	Ozonation	168
	6.5	Dechlorination	170

V. SUMMARY, CONCLUSIONS AND RECOMMENDATIONS	176
VI REFERENCES	
ADDENIDIX 1 DO SELECTIVITY TEST	100
APPENDIX 1 KO SELECTIVITI TEST	
APPENDIX 3 CHLORINATION PARAMETER DATA APPENDIX 4 AERATION DATA	211
APPENDIX 5 COMPARISON BETWEEN AQUACULTU ACTIVATED SLUDGE EXTRACTS	RE AND251

# LIST OF FIGURES

Fig. 1	Distribution of Hypochlorous Acid and Hypochlorite Ion at Different pH
Fig. 2	Breakpoint Chlorination Curve9
Fig. 3	Reactions of Hypochlorous Acid with Organic Compounds12
Fig. 4	Model of Aquatic Humic Macromolecule; reproduced from Christman, et al. 198121
Fig. 5a	Molecular Structure of Resorcinol
Fig. 5b	Molecular Structure of Substituted Resorcinol22
Fig. 6a	Effect of Chlorine Dose on THM Formation25
Fig. 6b	Effect of Contact Time and pH on THM Formation26
Fig. 7	Reaction Pathways for THM Formation27
Fig. 8a	Formation of Halogenated Compounds with Respect to Contact Time (Reproduced from Miller, 1983)
Fig. 8b	Formation of Halogenated Compounds with Respect to Chlorine Dose (Reproduced from Miller, 1983)
Fig. 8c	Formation of Halogenated Compounds with Respect to pH (Reproduced from Miller, 1983)40
Fig. 8d	GC of Chlorinated Fulvic Acid Breakdown Products (Reproduced from Quimby, 1980)41

Fig.	8e	GC of Chlorinated Humic Acid Breakdown Products (Reproduced from Quimby, 1980)4	1
Fig.	9	Chlorination of Phenol at Various Chlorine Doses (Reproduced from Onodera, 1984)4	7
Fig.	10	Schematic of the San Diego Wastewater Treatment Plant5	8
Fig.	11	Extraction Apparatus6	50
Fig.	12	GC of the Aquaculture Effluent Total Extract	30
Fig.	13	Reconstructed GC/MS of the Aquaculture Effluent Total Extract	33
Fig.	14	GC of Fraction 1 of the Aquaculture Effluent Extract	34
Fig.	15	GC of Fraction 2 of the Aquaculture Effluent Extract	36
Fig.	16	GC of The RO Effluent Total Extract	37
Fig.	17	V Rejection of Straight Chain Fatty Acids by the RO Unit	39
Fig.	18	GC of the Chlorinated Final Effluent	<b>)</b> 8
Fig.	19	GC of Chlorinated XAD8 Aquaculture Extract (1 mg)10	)0
Fig.	20	GC of Chlorinated Concentrated XAD8 Aquaculture Extract (30 mg)10	)2
Fig.	21	Reconstructed GC/MS of Chlorinated XAD8 Aquaculture Extract	)4
Fig.	22	ECD Areas of the Chlorinated XAD8 Aquaculture Extract	)8

τ.

-

Fig. 23 Fractionation Scheme of the Chlorinated Methylene Chloride Extracts
Fig. 24 ECD Areas of the Chlorinated Silica Gel Fractions
Fig. 25 ECD Areas of the Chlorinated Humic/Fulvic Fractions117
Fig. 26 ECD Areas of the Chlorinated Ultrafilter Fractions120
Fig. 27 GC of Chlorinated XAD8 Extract from Whittier Narrows Wastewater Treatment Plant
Fig. 28 GC of Chlorinated XAD8 Extract from the Water Hyacinth Wastewater Treatment Plant
Fig. 29 ECD Areas of Chlorinated XAD8 Fractions from Whittier Narrows Wastewater Treatment Plant
Fig. 30 ECD Areas of Chlorinated XAD8 Fractions from the Water Hyacinth Wastewater Treatment Plant
Fig. 31 GC of the Breakdown Products of Chlorinated Morin134
Fig. 32 Molecular Structure of Flavone and Kaempherol136
Fig. 33 GC's of Chlorinated Aquaculture XAD8 Extract at Various Chlorine Doses
Fig. 34 Effects of Chlorine Dose on the Breakdown Products of Chlorinated XAD8 Extract
Fig. 35 GC's of Chlorinated Aquaculture XAD8 Extract at Various Contact Times
Fig. 36 Effect of Contact Time on the Breakdown Products of Chlorinated XAD8 Extract
Fig. 37 GC's of Chlorinated Aquaculture XAD8 Extract at Various pH values

.

Fig. 38 Effect of p Chlorinate	pH on the Breakdown Products of d XAD8 Extract	147
Fig. 39 GC's of C the Presen	Chlorinated Aquaculture XAD8 Extract ince of Bromide	n 149
Fig. 40 Effect of Chlorinated	Bromide on the Breakdown Products of d XAD8 Extract	150
Fig. 41 Reaction	of Sodium Sulfite with 3-Bromopropene	156
Fig. 42 GC's of the Chlorin	the Reaction between Sodium Sulfite and inated San Diego Final Effluent	158
Fig. 43 GC's of the Chlorinate	the Reaction between Sodium Sulfite and ed Aquaculture XAD8 Extract	l 160
Fig. 44 Treatment	t of NVCO by PAC	164
Fig. 45 Reduction	n of NVCO Levels by the use of Chlora	mines166
Fig. 46 GC's of t Formation	the Effects of Pre-Ozonation on NVCO	
Fig. 47 Schematic Scheme	c of the Proposed 2-Stage Chlorination	174
Fig. 48 Treatmen	t of NVCO Levels by 2-Stage Chlorinat	ion175

٦

## LIST OF TABLES

Table 1.	Research Goals and Achievements4
Table 2.	Classification of Humic Materials17
Table 3.	Halogenated Compounds Observed by Quimby et al
Table 4.	Halogenated Compounds Observed by Coleman et al44
Table 5.	Halogenated Compounds Observed by Kringstad et al45
Table 6.	List of Performed Experiments54
Table 7.	Method Extraction Efficiency63
Table 8.	Other Procedures
Table 9.	Gravimetric Data for Total Acid Extracted Organics71
Table 10.	General Makeup of Aquaculture Effluent Extract72
Table 11.	Comparison of Reduction Efficiencies74
Table 12.	Compounds Identified in the Aquaculture Effluent during the 4/86 Sampling by GC/MS77
Table 13.	Treatment of Some of the Identified Compounds in the Aquaculture Effluent during the 7/85 Sampling
Table 14.	Halogenated Compounds Produced during Disinfection95
Table 15.	Experiments to Fractionate the Precursors

Table 16.	Organic Solvent Fractionated XAD8 Extract114
Table 17.	Ultrafilter Fractionated XAD8 Extract119
Table 18.	Chlorinated Pure Compounds
Table 19.	Addition of Sodium Sulfite to Pure Compounds155
Table 20.	Effects of Sodium Sulfite on Chlorinated XAD8 Extract
Table 21.	Treatment of NVCO by Aeration
Table 22.	Precursors Characteristics

-

## ACKNOWLEDGMENTS

This work was supported by the California Department of Water Resources under Contract B-54863.

The authors are grateful for the help of the San Diego Aqua One treatment facility, and particularly to Mr. Greg Elliot. Mr. Ed Ruth assisted us with the GC/MS analysis. Ms. Debby Haines was particularly helpful in the preparation of this final report. Mr. Bich Huynh helped with many of the laboratory procedures.

#### ABSTRACT

This report describes three years of work at the San Diego Aqua One experimental wastewater reclamation facility. The project was supported by the California Department of Water Resources as a part of its efforts to encourage water reclamation in the State of California.

The original orientation of the project was to investigate the effects of fouling materials on reverse osmosis (RO) membranes. A second and lesser objective was to evaluate the selectivity of several new, low pressure membranes which were candidates for future work at the San Diego facility. As the project progressed it became obvious that the intermittent operation and daily flushing of the RO membranes precluded fouling studies.

In preparing for the investigation of fouling materials on RO membranes, several surveys or organic compounds and their removal across the treatment plant were made. These surveys indicated that the aqua culture system, sand filters, reverse osmosis unit, and activated carbon adsorber were removing the great majority of the organic contaminants. Unfortunately, the chlorination disinfection procedure was negating the positive effects of the reverse osmosis and adsorption process by producing a number of high molecular weight, nonvolatile chlorinated organics. The emphasis of this project gradually changed from finding RO fouling materials to reducing chlorinated by-products.

It was observed that many of the halogenated organics formed during disinfection are reactive with dechlorinating agents (sodium sulfite). Most of these sulfite reactive compounds were found to be unsaturated halogenated molecules. Dechlorination with sulfite prior to sample extraction is consequently only advocated in instances where the compounds of interest are known to be unreactive with the sulfite ion. Many of the observed compounds have escaped detection in the past due to laboratory dechlorination prior to sample extraction.

The major precursors to the observed halogenated compounds were found to be slightly organic solvent soluble (methylene chloride) and to have molecular weights less than 1000 daltons.

It was observed that pH, chlorine dose, contact time, as well as bromide ion concentration, greatly affect the relative distribution, as well as total amounts of chlorination by-products. To minimize the formation of the compounds observed in this study, low pH, long contact time and medium chlorine doses should be used. A general recommendation of these chlorination conditions is however intentionally not advocated. The compounds which were monitored in this work are only a fraction of the Total Organic Halogen (TOX) formed upon chlorination. A recommendation of general chlorination conditions is dependent on the minimization of the most harmful components of TOX.

The choice of chlorination conditions can potentially be tailored to minimize the most harmful components of TOX. In addition, chlorination conditions may be chosen to form components of TOX which are amenable to a subsequent treatment step.

Several treatment alternatives were screened for their ability to reduce the formation of the observed halogenated compounds. Disinfection with chloramines, carbon adsorption treatment, partial dechlorination, aeration and preozonation were investigated. Carbon adsorption after chlorination was found to be the most effective treatment scheme.

#### I. INTRODUCTION

The use of chlorine in water treatment dates to the 1850's when it was used to deodorize London sewage. The first use of chlorine as a potable water disinfectant was 1903. In addition to disinfection, chlorine is commonly used for many other purposes including odor and taste removal, iron and manganese removal, hydrogen sulfide oxidation and prevention of biofouling on the filters and membranes used in treatment plants (White 1978).

Despite the many beneficial uses of chlorine in water treatment, there has been concern over the health effects of the chlorinated organic compounds produced during the chlorination process (Bull 1982, Cotruva 1981). These chlorinated organic compounds are produced by the reaction of aqueous chlorine with organic carbon in water. The source of the organic carbon may be naturally occurring plant and animal decay products (humic and fulvic acids), animal or bacterial metabolic products or many organic pollutants (e.g. phenols) which may be present in the chlorinated water. The chlorinated organic compounds which have received the most attention thus far, are the trihalomethanes (THM's) (Rook 1974, Rook 1976, Oliver 1979, Minear and Bird 1979).

The most commonly produced THM's in water chlorination are  $CHCl_3$ ,  $CHCl_2Br$ ,  $CHClBr_2$  and  $CHBr_3$ . These compounds are also suspected carcinogens. Although it is not possible at this date to state what renders a chemical species carcinogenic, many compounds which contain carbon-halogen bonds, such as pesticides and THM's, are often implicated as possible carcinogens (Robbins and Cotran 1983).

The presence of THM's in water indicates that carbon sources in sufficient quantities to react with chlorine were present in the water prior to chlorination, which in turn implies the formation of other halogenated, oxidized and potentially harmful chlorination by-products. Since THM's are readily analyzed in the laboratory by either EPA recommended methods or other well documented techniques (US EPA 1979, Kaiser 1976, Henderson 1976, Glaze 1981, Mieure 1977, Richard 1977, Bellar 1974, Nicholson 1977), they have become "indicator compounds" for the extent of chlorination-side reactions in drinking water, in the same manner that coliforms are "indicator bacteria" for disinfection efficiency.

During the past seven years, there has been increased attention to the non-THM chlorination by-products. Glaze (1979) found that the ratio of non-volatile to volatile chlorinated organic compounds produced from the chlorination of fulvic acids (natural carbon sources in water) to be 2:1.

Volatile compounds in the water are those species with low boiling points (BP), whereas non-volatile compounds have high boiling points. There is no classical BP cutoff to distinguish between volatile and non-volatile compounds. For the purpose of this work, a volatile compound has a boiling point less than 120°C. Chloroform, a THM with a BP of 61°C is an example of a volatile chlorinated organic compound. Non-volatile Chlorinated Organics are also often labeled Non-purgeable Total Organic Halogens (NPTOX). This large group of compounds can be further divided into gas chromatographable and non-gas chromatographable compounds. The overall goal of this research is to gain a broader understanding of the formation of gas chromatographable non-volatile halogenated organics. Currently the EPA sets standards for maximum allowable total THM's (volatile compounds) in drinking water supplies, but does not set any standards for other groups of halogenated compounds. It is quite plausible that the heavier chlorinated organics may be more harmful than THM's, and that they should be monitoried more carefully with greater attention (Cummings 1983, Coleman 1984).

In order to gain this broader understanding of gas chromatographable non-volatile chlorinated organics (NVCO), there are several basic questions that this research addresses. First, an analytical technique for extraction of NVCO and the consequent gas chromatographic separation of the extract was developed. Several interesting and significant findings were discovered during the development of the protocol for NVCO analysis. Secondly, the major organic precursors which react with chlorine to yield the gas chromatographable NVCO are classified by molecular weight and solubility and are also tentatively characterized. Third, identification and molecular characterization of some of the observed NVCO by gas chromatography/mass spectroscopy are performed. Fourth, various parameters which affect the production of NVCO upon chlorination such as pH, chlorine dose, and contact time are varied to assess their importance in producing NVCO. The final achievement of this work is the recommendation of treatment schemes and chlorination conditions which minimize the formation of the observed NVCO. The water samples used in this work were collected at a tertiary treatment plant in San Diego, California. The examination of the chlorinated organics at the San Diego plant is part of a larger California Department of Water Resources (DWR) funded study on the presence and treatment of organic compounds at the San Diego facility. The observation that many of the NVCO seen in the treatment plant's chlorinated final effluent are also present in chlorinated drinking water and other wastewater treatment plant effluents have greatly enlarged the scope of this research.

This research intends to incorporate the concern for NVCO formation into the design of treatment plant chlorination schemes. The other novelty in this work is that unlike other research work on chlorination by-products, the premise that humic materials are the precursors to the observed halogenated compounds is not made a priori.

The achievements of this research are stated in Table 1.

#### Table 1

#### **Research Goals and Achievements**

- 1. Development of an improved analytical technique for analysis of gas chromatographable non-volatile chlorinated organics (NVCO).
- 2. Characterization of the major precursors for NVCO formation.
- 3. Identification by GC/MS of some of the formed NVCO.
- 4. Analysis of the effects of chlorination operating parameters on the production of gas chromatographable NVCO.
- 5. Recommendation of treatment schemes and chlorination conditions which would minimize the formation of gas chromatographable NVCO.

#### **II. LITERATURE REVIEW**

#### **1. BASIC CHLORINE CHEMISTRY AND DISINFECTION**

The most important use of chlorine is the disinfection of potable water. As a result of the 1972 Federal Water Pollution Control Act, all wastewater treatment plants in the United States are subject to disinfection requirements. The reactions of aqueous chlorine in potable and wastewater are very similar, but wastewater exerts a much greater chlorine demand.

#### **1.1 Dissociation of Chlorine**

Chlorine is most often applied in its elemental gaseous form. The hydrolysis proceeds according to equation (1).

$$Cl_2 + H_2O \rightarrow HOCl + H^+ + Cl^-$$

(1)

The hydrolysis constant is  $4.0 \times 10^4 \text{ mole}^2/\text{liter}^2$  at 25°C. The hydrolysis reaction is very rapid and goes to completion in less than one second. (Morris 1978). Hypochlorous acid is a weak acid with a dissociation constant of  $3.2 \times 10^4$  mole/liter at 25°C.

$$HOCl \stackrel{\rightharpoonup}{=} H^+ + OCl^- \tag{2}$$

As can be seen from equation (2), pH is critical in determining the dominant species in solution (Figure 1). The time to reach equilibrium is instantaneous, being much less than one second.



.

Fig. 1 Distribution of Hypochlorous Acid and Hypochlorite Ion at Different pH

6

#### **1.2 Formation of Chloramines**

Ammonia is commonly present in wastewater and traces often occur in many drinking water supplies. Furthermore, ammonia is often added before chlorination in order to provide stable combined chlorine residuals. Chlorine reacts with ammonia to produce chloramines. The empirical reactions of chlorine with ammonia proceed as follows:

$$NH_3 + H_2O \longrightarrow NH_4^+ + OH^-$$
(3)

$$HOCl + NH_3 \longrightarrow NH_2Cl + H_2O \tag{4}$$

$$HOCl + NH_2Cl \longrightarrow NHCl_2 + H_2O \tag{5}$$

$$HOCl + NHCl_2 \longrightarrow NCl_3 + H_2O \tag{6}$$

where

NH <sub>2</sub> Cl	=	Monochloramine
NHCl <sub>2</sub>	=	Dichloramine
NCl <sub>3</sub>	=	Nitrogen Trichloride

The products shown in equations (4), (5) and (6) represent the several forms of combined chlorine. The rates of chloramine formation and the ratio of  $NH_2Cl$  to  $NHCl_2$  depend on pH and the ratio of  $HOCl:NH_3$ . High pH favors dichloramine formation and low pH favors monochloramine formation prior to the breakpoint. The addition of increasing amounts of chlorine to  $NH_3$  free water results in a near linear increase in free chlorine residual. The first combined residual to be formed is monochloramine (Saunier and Selleck 1979). As the ratio of chlorine added to  $NH_3$  increases, dichloramine is formed.

Increased addition of chlorine results in the breakdown of chloramines to nitrogen gas and a drop in total chlorine residual. Once the breakpoint is reached, additional chlorine produces free chlorine residuals. Figure 2 illustrates the breakpoint reactions.

The time required for chloramine formation is greater than the time required for chlorine dissociation, but is generally also rapid (Morris, 1965). The monochloramine reactions proceed most rapidly at pH 8.3 and are 99% complete in less than one second for 1 millimole  $NH_4^+$ -N and 20 millimole chlorine. At pH 2 it takes 7 minutes to complete the reactions.



Fig. 2 Breakpoint Chlorination Curve

9

#### **1.3 Disinfection Efficiencies of Chlorine Residuals**

Although there is still some controversy about the disinfection efficiency of the various chlorine residuals, some generalizations can be made. Many workers have noted that hypochlorous acid is the strongest disinfectant (White 1986). Butterfield et al. (1943) noted that one hundred times more hypochlorite ion than hypochlorous acid is required to deactivate equivalent amounts of E. Coli. Chloramine residuals typically are less germicidal than hypochlorous acid, but given adequate contact time, monochloramine is nearly as effective as free chlorine in achieving disinfection of most bacteria (Collins 1971). Selleck, Saunier and Collins (1978) observed that breakpoint residuals in the pH range of 7-8 produce the most rapid disinfection. Sepp (1981) pointed out that disinfection efficiency can be improved by rapid initial mixing in the contact chamber.

#### **1.4 Reaction of Chlorine with Inorganic Ions**

The displacement of either  $Cl^-$  or  $OH^+$  from the HOCl molecule results in the oxidation of  $Mn^{+2}$  to  $Mn^{+3}$ ,  $Fe^{+2}$  to  $Fe^{+3}$ ,  $NO_2$ - to  $NO_3^-$  as well as many similar reactions. Equation (7) serves as an illustration

$$NO_{2}^{-} + HOCl \longrightarrow NO_{2}OH + Cl^{-}$$
(7)

These reactions are relatively slow and according to Kokoropoulos and Manos (1973) exhibit little reaction during the contact times used to obtain disinfection.

#### 1.5 Reactions of Chlorine with Organic Molecules

The reactions of chlorine with organic carbon sources is the subject of this dissertation. A full discussion is presented in later sections. Chlorine may undergo oxidative reactions with organics and produce  $CO_2$ , cleave bonds, or raise the oxidation state of the compound. Substitution reactions are also very common, which lead to the production of chlorinated organics. Figure 3 shows some illustrative reactions.

**NITROGEN SUBSTITUTION:** 



Fig. 3 Reactions of Hypochlorous Acid with Organic Compounds

#### 2. ANALYSIS OF ORGANICS IN WATER BY GC AND GC/MS

The analysis of organic chemicals in water is becoming an increasingly important issue. Trace amounts of organics in drinking water may cause illness, cancer, taste and odor. Volatile organic compound may be collected for GC analysis by purge and trap techniques, liquid-liquid extraction, or head space methods. Non-volatile organic compounds in the aqueous phase (not adsorbed to particulates in the water) are concentrated by solvent extraction (Baker 1967, Andelman 1965, Thomas 1980), carbon adsorption, adsorption on macroreticular resins (Burnham 1972, Junk 1974, Shinohara 1981), reverse osmosis (Coleman 1980), or closed loop stripping (Coleman 1984).

The adsorption of organic contaminants from large volumes of water and their consequent desorption with small volumes of organic solvents is an attractive collection and concentration method. The use of activated carbon for this purpose has fallen out of favor because many compounds are not quantitatively desorbable from the carbon. Macroreticular resins (ex: Rohm and Hass brand XAD1-9) are effective in adsorbing many compounds. Their binding energies are small, so desorption is less problematic than with activated carbon. These resins, however, are extremely dirty and contaminated and require extensive and meticulous cleaning before use.

Solvent extraction is the most commonly used method for organics concentration. Although solvent extraction is simple and effective for numerous compounds, it suffers form many drawbacks. The distribution coefficient for the contaminants between water and the extraction solvent must be favorable, and is often unfavorable for highly polar compounds. Second, most solvents are health hazards. The most versatile extraction solvent is diethyl ether (low cost, low boiling point, high polarity, low toxicity), but its potent anesthetic effects make its use prohibitive except in hoods and well ventilated laboratories. Although dichloromethane is more toxic than ether, it has little anesthetic effect and has thus become popular with many analysts (Miller 1983, Coleman 1985, Quimby 1980). Trichlorotrifloroethane (Freon 113) is the recommended extraction solvent for oil and grease analysis due to its low toxicity *Standard Methods* (1985). The cost of Freon 113, as well as it boiling point, make it less attractive than methylene chloride and diethyl ether.

Coleman, et al. (1980) combined solvent extraction with an additional concentration step using reverse osmosis. The pre-concentration step using RO allowed for lower detection limits. The increased sensitivity of this protocol enabled the identification of four hundred and sixty organic compounds in Cincinnati, Ohio drinking water. The extract was from four hundred gallons, which were concentrated by reserve osmosis, before ether extraction. Coleman's list of organic pollutants contains chloro-phenols, chloro-aliphatic hydrocarbons, chloro-aromatic hydrocarbons, chlorinated alcohols, chlorinated ketones, chlorinated aldehydes, chlorinated ethers and acids, chlorinated esters, amides and amines. Some of these chlorinated compounds are a result of industrial dumping, but many others are chlorination by-products.

#### 3. VOLATILE CHLORINATED ORGANICS

In 1974, Rook discovered that trace concentrations of chloroform are produced as side reactions during the chlorination of untreated river water. Since Rook's initial discovery, extensive research has been conducted on the various factors affecting THM production. Several related research areas have converged to give a nearly complete picture of haloform formation during chlorination. Work has been done on developing methods for haloform analysis (US EPA 1979, Kaiser 1976, Henderson 1976, Glaze 1981, Mieure 1977, Richard 1977, Bellar 1974, Nicholson 1977), identifying the major THM precursors (Rook 1974, Line 1984, Stevens 1976, Oliver 1979, Oliver 1980, Urano 1983, Boyce 1979, Boyce 1983, Morris and Baum 1978, Hoehn 1979), as well as efforts to reduce haloform levels by use of chloramines (Norman 1980), carbon adsorption (Rook 1974, Stevens 1976, Digiano 1983), reverse osmosis (Odegaard 1982), alum coagulation followed by sand filtration (Oliver 1979), as well as air stripping (Rook 1974).

The abundance of published literature on THM's makes it prohibitive to conduct a thorough review. Only the aspects of THM's relevant to this research are examined. Haloform precursors, the effects of pH and other variables on THM production, as well as efforts to minimize haloform formation during water chlorination, are reviewed.

#### **3.1 Haloform Precursors**

The initial observations that THM's were present in essentially every chlorinated water supply lead early researchers to conclude that the carbon source (precursor) for their production is ubiquitously present in all natural waters. Aquatic humic material is present in all waters and it is sufficiently similar in time and space that it has become the 'prime suspect' (Babcock 1979, Rook 1974, Stevens 1976). There are numerous other compounds which have been shown to be capable of THM production upon chlorination.

Morris and Baum (1978), showed that chlorophyll yields THM's in its reaction with aqueous chlorine. Hoehn et al. (1979) demonstrated that algal extracellular products (ECP) are potent THM precursors. Briley et al. (1979) concluded that ECP from algal growth, as well as algae biomass produce THM concentrations comparable to yields from humic and fulvic acids.

Phenol and ketones (Boyce and Hornig 1979, Boyce 1983, Onodera 1984), as well as a host of other simple organic compounds, are also capable of producing THM's upon chlorination. The concentrations of these compounds have always been deemed too low to consider them major THM precursors.

Due to the abundance of aquatic humic substances, rightly or wrongly, they have always been labeled the primary precursor for THM formation. Humic substances will consequently be described in some detail before discussing chlorination experiments of humic materials.

Christman (1981, 1983), as well as Gjessing (1976) have done extensive research on the nature of aquatic humic substances. Humic substances are a complex assemblage of decayed plant and soil materials and of the polymeric compounds produced by the random combination of these various biomonomers (Gilliam 1982). As can be inferred from such a broad and vague definition, the nature of humic material is at best poorly understood. The substances which are collectively called humic material can be further separated and classified. In 1919 Oden described a classification system which is still the most commonly used today (Table 2). The differentiation criteria used in this system are the varying solubilities of aquatic humic fractions in acids and bases.

Oden's classification system, as well as several other fractionation schemes in use today, should be regarded more as operative than absolute definitions. Some of the other classification systems can separate humic materials into thirteen chemically and spectroscopically different fractions using adsorption column chromatography (Dragunev 1969).

# Table 2Classification of Humic Materials

Group	Description	
Humas coal	insoluble in base and acid	
Fulvic acid	soluble in base and acid	
Hyatomelanic acid	soluble in base, insoluble in acid, soluble in alcohol	
Humic acid	soluble in base, insoluble in acid and alcohol	

In addition to their solubility differences, the humic material fractions also contain differing percentages of elemental carbon, oxygen, nitrogen, sulfur and hydrogen. Although humic and fulvic acids vary slightly from location to location, the following generalizations are made. Aquatic humic acid contains larger amounts of hydrogen and lower amounts of carbon and nitrogen than aquatic fulvic acid. Additionally, aquatic humic materials are mostly fulvic acid (60-90%) with smaller amounts of hyatomelanic acid (9-30%) and humic acid (1-20%) and even smaller amounts of humas coal (Christman 1981).

X-ray crystallography and chemical degradation of the large humic molecules and the consequent gas chromatographic analysis of the breakdown products by Christman (1981) and others (Liao 1982, Gilliam 1982) has lead to the formulation of several models of the structure of these humic macromolecules. Figure 4 is a model proposed by Christman of a structure which is capable of producing most of the observed degradation products. It should be emphasized that this is only a model and it is likely that no such exact entity exists in nature.

Humic materials have been implicated as sinks and chelating agents for volatile chlorinated compounds as well as for their role as chlorination precursors (Gabitta, et al. 1985; Gabitta, 1986). Calloway, Gabitta and Vilker (1984) also noted that low molecular weight halocarbons exhibit greater solubility in humate solutions than in distilled water. These observations indicate that humic materials may contribute to elevated halocarbon levels in water supplies in numerous ways.

Reinhard (1984) used ultrafiltration to show that the molecular weight ranges of dissolved organic carbon can range from less than 500 to greater than 10,000. It is generally believed that the color humic macromolecule's molecular weight may range from 500 to an excess of 100,000. There are conflicting reports in the literature and little, or no, agreement on the MW of the fulvic vs. humic vs. hyatomelanic fractions. It is generally agreed upon however, that fulvic acids are of lower MW (500-20,000) and that humic acids cover the larger MW range (10,000-200,000).

Rook (1974) postulated the importance of aromatic carbon rings with two OH groups in the meta position as precursors for haloform formation (Figure 5).

Resorcinol (Fig. 5) is considered to be a building block of the humic and fulvic acids as can be seen by comparing Figs. 4 and 5. Rook chlorinated fulvic acid samples, as well as solutions of resorcinol, other diols and diketones and showed them to be capable of significant  $CHCl_3$  production.

Boyce and Hornig (1983), using isotopically labeled resorcinol, elegantly showed the production of isotopically labeled chloroform. In later work, Boyce and Hornig also showed that aromatic di-ketones are also capable of  $CHCl_3$  formation upon chlorination (1979). In similar experiments, Secholing (1984) also chlorinated model aqueous humus compounds which resulted in significant THM production. Stevens (1976) conducted bench and pilot scale chlorinations on humic materials (humic and fulvic acids) as well as low molecular weight compounds containing the acetyl moeity (C = 0), and concluded that both classes of compounds are capable of THM formation.

Oliver, Simon and Visser (1980) fractionated humic and fulvic acids into different molecular weight ranges by ultrafiltration. The fractionated material was then redissolved in high grade water and chlorinated with sodium hypochlorite (15 mg/L) at pH 11 for 72 hours. After quenching the residual chlorine, the chloroform concentrations were determined by GC analysis following an extraction step using pentane. They observed that 72-80% of the chloroform came from the fulvic acid rather than the humic acid components. They also noted that the 1,000-10,000 MW fulvic acid fraction was the most  $CHCl_3$  productive component.

## 3.2 Effects of pH, and other Parameters on THM Production

Stevens et al. (1976) conducted bench and pilot scale experiments to determine the effect of humic acid concentration, pH, temperature, free vs. combined chlorine and reaction time on THM production. They observed an increase of THM concentration with time at a given chlorine dose and found high pH to yield greater amounts of haloforms. Free chlorine produced four times more haloforms than combined residuals. Higher temperatures also greatly increased haloform production. After 100 hours of contact time 225  $\mu$ g/L chloroform were produced from 10 mg/L free chlorine, 1 mg/L humic acid at pH 7 and 40°C. Only 45  $\mu$ g/L of chloroform were produced at 3°C. Oliver (1979) also observed similar results. Figure 6 summarizes the trends in their observations.

Peters, Young and Perry (1980) also examined the reactions of free chlorine at varying pH's and temperatures with humic and fulvic acids extracted from the Thames River. They observed similar trends to those observed by Stevens et al. Peters et al. however, made the further distinction between chloroform which was formed directly from humic molecules and chloroform which was formed from a non-volatile chlorinated organic intermediate. The NVCO would be semi-stable chlorinated molecules produced





Fig. 4 Model of Aquatic Humic Macromolecule; reproduced from Christman, et al. 1981.



Figure 5: Molecular Structure of Resorcinol
by the chlorination of humic acid.

They were able to make the distinction between the two sources of chloroform by stripping the chlorinated water with nitrogen gas (the stripped water should contain no chloroform) and the consequent direct aqueous injection of a water sample in the GC. The high temperature of the GC injection port accelerates the breakdown of  $CHCl_3$  from the NVCO. This chloroform was termed residual  $CHCl_3$ . Total chloroform was measured without stripping the chlorinated sample. Dissolved chloroform, resulting from the immediate breakdown of humic materials, is calculated as a difference between total and residual chloroform. Figure 7 is a schematic of these two reaction paths.

Urano et al. (1983) observed the increasing haloform production with increasing chlorine dose while chlorinating humic substances with free chlorine. They observed similar pH, temperature and time relations as previously discussed increased THM formation at high pH, high initial chlorine concentrations, long contact times and higher temperatures. They consequently derived the following empirical rate equation, which summarizes the various parameter effects on haloform production.

$$[THM] = 3.5 \ x \ 10^3 e^{-4.47 x 10^3 / T} (pH - 2.8) [TOC] [Cl_2]_o^{.25} \ t^{.36}$$
(8)

where

[THM]	=	trihalomethane concentration
Т	=	temperature (°C)
[TOC]	=	total organic carbon concentration
[ <i>Cl</i> <sub>2]</sub>	=	initial free chlorine concentration
t	=	time (hours)

.



Fig. 6a Effect of Chlorine Dose on THM Formation After Stevens et al. (1976)

.



Contact time, hours

Fig. 6b Effects of Contact Time and pH on THM Formation After Stevens et al. (1976)



Fig. 7 Reaction Pathways for THM Formation

#### 3.3 Efforts to Minimize Haloform Production

The efforts to minimize the THM levels in chlorinated waters include alternate forms of disinfection, precursor removal prior to chlorination or removal of the THM's after their production.

Norman et al. (1980) investigated the use of chloramines at the Huron, South Dakota treatment plant in order to reduce their high THM levels (137  $\mu$ g/L). Ammonium sulfate was added at a location which would allow 30 minute contact time with free chlorine before the formation of chloramines. The free chlorine contact period was a compromise in order to allow maximum disinfection with minimum THM formation. This practice resulted in a 75% reduction in the THM levels (37  $\mu$ g/L).

Oliver and Lawrence (1979) observed that filtering with a 0.45 micron prior to chlorination only marginally reduced THM formation. Alum coagulation and flocculation followed by filtration through a sand filter caused a 67% reduction in THM formation and a 34% drop in TOC. They reasoned that the most likely explanation for the drop in haloform production is the removal of humic materials (precursors) by the coagulation flocculation step. The authors had previously observed that about half of commercially purchased humic and fulvic acids are removed from a 5 mg/L aqueous solution with their alum treatment.

Rook (1976) used several pilot scale treatment schemes to reduce haloform formation. Under his reaction conditions 65  $\mu$ g/L of chloroform were produced without treatment. Coagulation prior to chlorination reduced the levels of chloroform to 28  $\mu$ g/L. Coagulation followed by sorption on anion exchange resins reduced the levels even further (9  $\mu$ g/L). The use of this anion resin however, is costly and its regeneration is an added source of contamination to the environment.

Rook also used ozonation in conjunction with chlorination in order to reduce haloform levels. The ozonation was supposed to render the precursors unreactive to the consequent chlorination. Only slight improvement was observed using this technique.

In another series of experiments, Rook studied the removal of haloforms following their formation. Carbon adsorption, as well as air stripping, were tested. Activated carbon was found very effective for THM removal, but the haloforms broke through in a relatively short time (2 weeks) even though the carbon was still very effective in removing other larger molecules. As would be expected, air stripping of the haloforms is a successful technique.

Odegaard and Koottatep (1982) used reverse osmosis to remove the humic precursors prior to chlorination. 80-100% color removal was achieved using small pore membranes. No data however, were given for haloform reduction.

McCreary and Snoeyink (1980) used activated carbon for the removal of different MW fractions (separated by gel filtration and ultrafiltration) of humic material in an effort to remove haloform precursors. They found the lower MW fractions of the humic macromolecule to be better removed by carbon adsorption. Additionally, functional group analysis of the fractionated humics showed that activated carbon treatment efficiency decreases with increasing total carboxyl groups (polar moiety) in the particular fraction. They were unable to correlate haloform production with total carboxyl groups however. As has been previously stated, the lower molecular weight fractions have a higher THM formation potential (THMFP) than the higher MW humic fractions. Despite the higher removal efficiency of the lower molecular weight fractions by the activated carbon, THM formation is only moderately reduced by carbon treatment, since the high MW fractions react with chlorine to a greater extent in the absence of the lighter MW fractions.

### 4. NON-VOLATILE CHLORINATED ORGANICS (NVCO)

Non-volatile chlorinated organic compounds (NVCO) have not been extensively studied for a variety of reasons. Rook's initial finding of chloroform in chlorinated water in 1974 set a trend for analysis of volatile compounds, which has only recently been revised. Secondly, non-volatile compounds are more difficult to analyze chromatographically because of column and temperature requirements. The low concentrations of individual NVCO (collectively the total NVCO may be greater than THM's however) may have prevented their detection by some researchers. Furthermore, the bulk of the organic matter in water is non-volatile, which makes identification and separation more difficult.

Non-volatile halogenated compounds can be analyzed collectively as a lump parameter by microcoulometry and labeled as total organic halogen (TOX) (Glaze 1977). Alternately, a subset of these compounds can be examined in detail by a chromatographic procedure.

High pressure liquid chromatography (HPLC) has frequently been used as the chromatographic procedure to separate the TOX. HPLC enables the separation and analysis of components of very large molecular weight. HPLC is consequently potentially capable of analyzing most of the chlorination byproducts. HPLC however suffers from low sensitivity and poor resolution in comparison to a GC system. In addition, HPLC retention times may be very long and peak width may exceed several minutes, which makes matching to known standards difficult. Gas chromatography (GC) and gas chromatography/mass spectroscopy (GC/MS) techniques provide the best available techniques for positive identification of organic compounds. GC and GC/MS protocols are only capable of analyzing relatively light, and relatively non-polar compounds. Consequently, only a fraction (5-50%) of the components of TOX are amenable GC analysis.

#### 4.1 Measurement of NVCO as TOX

The parameter TOX has recently been standardized as a US EPA procedure (US EPA 1980). The method often involves an adsorption concentration step with the subsequent combustion of the organic halides in an organic halide analyzer. The analysis is done in a gaseous stream and a titration by silver of the hydrogen halide generated (ASTM 1981). The measurement of TOX includes volatile and non-volatile halogenated compounds. Glaze, Peyton and Rawley (1977) demonstrated the utility and accuracy of the TOX parameter using both volatile and non-volatile halogenated compounds. Their test solutions included THM's and chlorophenols.

Jenkel and Roberts (1980) provide examples of the utility of the TOX parameter for the examination of chlorinated wastewater.

In a recent review publication Johnson and Jensen (1986) point out that pH and chlorine dose affect the extent of oxidation and substitution reactions of chlorine with organic matter in water. In summarizing the work of others, they note that large chlorine doses increase the percentage of TOX that is THM's. Low pH favors the formation of Non-purgeable TOX (NPTOX), whereas high pH favors THM formation. Fleischacker and Randtke (1983) chlorinated extracted fulvic acids, a commercially available humic acid and municipal secondary effluent extract (XAD8 adsorption). They observed that under most chlorination conditions chloroform represents only a small fraction of TOX. If chlorination is performed at high pH, chloroform becomes a sizeable amount of TOX. The authors also note that chloroform production is more strongly influenced by temperature than NPTOX.

Reckhow and Singer (1984) extracted lake fulvic acids by adsorption on XAD8 macroreticular resins. 320 ml solutions of 4.1 mg/L TOC were chlorinated at various pH, chlorine dose, and reaction times. Chloroform, Dichloroacetic acid (DCAA), Trichloroacetic acid (TCAA), and TOX were monitored. Alum coagulation and ozone treatment were evaluated for effectiveness in reducing the levels of the four measured parameters. Reckhow observed an increase in TOX, chloroform, DCAA, and TCAA as HOCl dose was increased. Longer reaction times also resulted in higher levels for all of the measured components. High pH favors light species, and chloroform levels become a smaller fraction of TOX at low pH. Surprisingly, humic acid fractions had higher yields than fulvic acid fractions for all species. The effectiveness of alum and ozone in reducing organic halides is discussed in a later section.

Wachter and Andelman (1984) chlorinated algal extracellular products as well as chlorophyll and measured TOX, Purgeable Organic Halide (POX), as well as NPTOX. The molecular size distribution of NPTOX was determined by HPLC, followed by TOX detection of the effluent. pH had the same effects on organohalide distribution as previously mentioned. As contact time increased, the ratio TOX/TOC increased as well as the ratio  $CHCl_3/TOC$ . The results of their size exclusion analysis point out that the majority of NPTOX has a MW greater than 1000 Daltons.

Chow and Roberts (1981) also observed that longer reaction times and higher chlorine doses tended to favor THM production and reduced levels of NPTOX. These workers chlorinated three liter volumes of secondary municipal effluents.

Norwood et al. (1983) extracted fulvic and humic acids and chlorinated concentrated samples in their laboratories. Their 1000 mg TOC samples were chlorinated with 4000 mg of free chlorine. The residual chlorine was then quenched after 24 hours. TOX and acid extractable organics were analyzed. Extraction efficiency was quite high for the produced TOX. 29.9 mg of organic halide were present in the unextracted sample. After ether extraction only 7.8 mg of TOX were measured representing a 74% extraction efficiency. This indicates that the majority of their observed TOX is relatively non-polar or slightly polar.

Bean, Mann and Neitzel (1983) analyzed chlorinated effluents from nuclear power station cooling waters. THM's, TOX and phenols were analyzed. Chlorophenols were a large portion of TOX (12-37%). THM's also represented a significant portion of TOX (up to 71%). The differences from previously mentioned values emphasize the point that chlorination byproducts are very dependent on the source water as well as the chlorination conditions.

#### 4.2 Analysis of NVCO by HPLC

Jolley (1978) identified several carbohydrates, polyols, organic acids, amides, amino acids, indoles, pyridine derivatives, purine derivatives and pyrimidine derivatives in domestic wastewater effluent. He observed chlorinated derivatives of many of these compounds in the chlorinated effluents. His laboratory chlorination was done with  $Cl^{36}$  tagged chlorine gas. His detector was a  $Cl^{36}$  radio counter using HPLC separation.

Jolley's HPLC output consisted of peaks with half hour widths and a total run time of sixty hours. These chromatogram characteristics make positive identification of compounds a difficult task. Jolley calculated that 0.5 to 3.1 percent of the applied chlorine is incorporated in the observed chlorinated organics.

Glaze et al. (1979) note that the reduced MW of extracted fulvic acids after chlorination (from  $10.5 \times 10^3$  to  $8.2 \times 10^3$ ). Using TOC, TOX and average molecular weight data, the authors estimate that the broken down fulvic polymer molecule contains 7 chlorine atoms.

Saleh and Mokti (1983) used three HPLC separation modes to fractionate both chlorinated and unchlorinated fulvic acids extracted from Texas, Oklahoma and Louisiana reservoirs. They discerned the formation of new compounds, most likely halogenated fulvic acids by the dual use of UV and fluorescence detectors.

Becher, Gjessing et al. (1985) fractionated natural humic water (no extraction) into seven fractions by high performance size exclusion chroma-

tography (HPSEC). The seven fractions were chlorinated and TOX was measured. Each of the seven fractions was TOX productive. The lightest MW fraction produced the highest TOX values upon chlorination. In a parallel analytical route, ultrafiltration of the original water sample lead to the observation that 82% of the TOX resulted from chlorination of the less than 1,000 MW fraction. The authors commented that the ultrafilter MW readings were slightly lower than the values given by the HPSEC.

#### 4.3 Analysis of NVCO by GC and GC/MS

In a recent publication, Miller and Uden (1983) discussed their studies on the effects of reaction time, NaOCl dose, pH and source of humic material with respect to the quantitative formation of chloroform and three non-volatile chlorinated organics. The three NVCO were dichloroacetic acid, trichloroacetic acid and chloral hydrate. They also followed the formation of seventeen other unidentified NVCO.

Humic and fulvic acids were isolated by adsorption on XAD resins. The extracted humic material (mostly fulvic acid) was redissolved in 40 ml of distilled water in an air tight container for chloroform quantification. One hundred ml volumes were used in the NVCO studies. 5 mg/L of fulvic acid (measured as TOC), 25 mg/L NaOCl, pH 7 phosphate buffer, and 24 hour reaction time were the base parameters for the experimental work. Four to five variations of chlorine dose, reaction time and pH were used while maintaining the other parameters constant in their quantitative studies. Sodium thiosulfate was added to quench residual chlorine before all analyses. Haloforms were measured by purge and trap techniques and the NVCO were extracted with diethyl ether. The NVCO extract was chromatographed with and without diazomethane derivitization. The reaction of diazomethane with the ether extracts results in the formation of methyl esters from the corresponding acids and yields methyl ethers from phenols. These nonpolar derivatives are more amenable to gas chromatographic analysis. More peaks were observed after derivatization than before, indicating the presence of acids, alcohols and phenolics in the original ether extract. Figures 8a, 8b and 8c show the quantitative trends of their observations.

In an earlier publication, Quimby, along with Uden, Delaney and Barnes (1980), using a very similar experimental protocol to Uden's previously described work, identified the chlorinated compounds listed in Table 3. This list of compounds contains both volatile and non-volatile chlorinated organics. Figures 8d and 8e show the gas chromatographs of some of these compounds.

Coleman et al. (1984) identified many NVCO produced by the chlorination of aquatic humic material. Many of these identified compounds had previously been observed in chlorinated drinking waters and are suspected mutagenic agents. It is worthy to note that these workers did not add any dechlorinating agents before extraction, but allowed the chlorine to be fully consumed by the humic macromolecules (reaction times in excess of ninety hours). The significance of this point shall be discussed in a later section.

Table 3 Halogenated Compounds Observed by Quimby, et al.

- 1 chloroform
- 8 2-chlorophenol
- 2 trichloroacetic acid
- 3 dichloroacetic acid
- 4 chloral hydrate
- 5 1-chlorophenol
- 6 2,4,6 trichlorphenol
- 7 2-chlorobenzoic acid

- 9 pentachloro-phenol
- 10 bromodichloromethane
- 11 chlorodibromomethane
- 12 3-bromophenol
- 13 bromoform
- 14 1-bromobenzoic acid





Figure 8a



Formation curves with respect to the NaOCi to C ratio of the four major aqueous chlorination products of fulvic acid: (O) TCAA; (D) DCAA; ( $\Delta$ ) chloroform; ( $\nabla$ ) chloral hydrate.

Figure 8b





Figure 8c

Figs. 8a, 8b, 8c:

Formation of halogenated compounds with respect to contact time (8a), chlorine dose (8b) and pH (8c). Reproduced with permission from Env. Sci. and Tech., Vol. 17, p. 153, 1983. Copyright 1983, American Chemical Society. Article authored by J.W. Miller and P.C. Uden.





Chlorine selective capillary gas chromatogram of nonmethylated chlorinated fulvic ackl extract (above) and chlorinated fulvic ackl extract methylated with diazomethane (below). Peak identities: (above) (1) chloroform, (2) trichloroacetic acid, (3) 1-chlorophenol; (below) (1) chloroform, (2) trichloroacetic acid methyl ester, (3) 2,4,6-trichlorophenol methyl ester, (4) 2-chlorobenzolc acid methyl ester, (5) 3,5-dichlorobenzolc acid methyl ester, (6) 1-chlorophenol, (7) 2chlorophenol, (8) pentachlorphenol methyl ether. Column 100 m × 0.4 mm i.d. OV 225 glass support coated open tubular (SCOT) column







Figs. 8d, 8e: GC's of chlorinated fulvic acid (8d) and humic acid (8e) breakdown products. Reproduced with permission from Analytical Chemistry, Vol. 52, p. 261, 1980. Copyright 1980 American Chemical Society. Article authored by B.D. Quimby, M.J. Delaney and P.C. Uden.

The work of Coleman et al. is impressive in many ways. Two different extraction solvents were used (dichloromethane and diethyl ether), as well as closed loop stripping (CLS), a relatively new analytical method for nonvolatile organics analysis were compared. Derivatization of the extracts was employed prior to GC/MS using state of the art fused silica capillary columns. Mutagenic assays (Ames tests) were performed on the NVCO extracts. In summary, the work was broad in its scope and combined to yield interesting and significant results.

They observed that the methylene chloride extract contained the most compounds, but that the ether extract was more mutagenic. They interpreted this to mean that the ether extract contained highly polar compounds that were not suitable for gas chromatography, but that these polar compounds result in the increased mutagenic activity. It was also observed that the gas chromotographable NVCO account for only 25% of the total organic halogen (TOX) measured by coulometry. Table 4 contains some of the NVCO observed by Coleman et al.

The authors conclude that much research remains to be done on NVCO and that it is likely that most of the mutagenic activity observed in the extracts was not represented by resolved GC peaks. They imply that much work remains to be done on developing and validating practical techniques for uncovering highly polar compounds from chlorinated water. Christman et al. (1981) had previously noted that humic breakdown products are extremely polar di and tri acids.

In a 1985 publication, Kringstad, Sousa and Stromberg (1985) observed the similarity between chlorination by-products of humic materials and bleaching liquors in the pulp industry. These extracts were found to be Ames test mutagenic. Many of these NVCO were aromatic and included several chlorophenols. No chemical dechlorinating agents were used to arrest the chlorination reaction. Excess residual chlorine was removed by rotoevaporation at 25°C. Table 5 lists some of the NVCO which were identified.

Christman et al. (1979, 1981), chlorinated extracted humic materials and identified the breakdown products by GC/MS. Excess chlorine was quenched with sodium arsenite before ether extraction. Derivatized methyl esters were then prepared before GC/MS analysis. An abundance of nonchlorinated breakdown products were observed which frequently contained an aromatic ring. No aromatic chlorinated products were observed however. Most of the identified NVCO were aliphatic acids including dichloroacetic acid and trichloroacetic acid. Miller (1983), Coleman (1984), Kringstad (1985), Quimby (1980), Snoeyink (1981) and McCreary (1981) on the other hand, observed several aromatic NVCO. This point is currently unclear in the literature. Clarifying this point is important because aromaticity often implies increased health risk.

Leer (1985) discovered the presence of highly chlorinated ethers in river sediments near an epichlorohydrin production plant. These compounds are formed during the aqueous chlorination of allyl chloride. Although the production of these chloroethers is a purely industrial problem, it points out that new classes of chlorinated compounds are continuous being discovered. All the chloroethers observed by Leer had not been previously identified.

# Table 4 Halogenated Compounds Observed (by Coleman, et al.)

trichloracetonitrile	1,1,1 trichloro-2-butanone
dichloroacetonitrile	hexachloroethane
1,1 dichloro-2-propanone	pentachloropene
3,3 dichloro-2-butanone	1,1,1,3,3 pentachloropropanone
3,3 dichloropropenal	tetrachlorothiophene
dichloropropenenitrile	bromotrichlorothiophene
1,1 dichloro-2-butanone	tetrabromothiophene
bromochloroacetonitrile	tetrachlorocyclopropene
1,1,1 trichloro-2-propanone	pentachloro-3-buten-2-one
2,2 dichloro-3-pentanone	hexachlorocyclopentadiene
trichloropropenitrile	bromodichlorophenol, acetate ester
tribromophenol, acetate ester	dichlorodihydroxybenzene
dibromodihydroxybenzene, acetate ester	

trichlorodihydroxybenzene, acetate ester

# Table 5Halogenated Compounds Observed by Kringstad, et al.

2,4,5 trichlorophenol	3,4,5 trichlorocatechol
2,3,4,6 tetrachlorophenol	tetrachlorocatechol
pentachlorophenol	3,4,5 trichloroguaicol
3,4,5 trichlorocatechol	2-chloropropenal
pentachloroacetone	hexachloroacetone
1,3 dichloroacetone	1,1,3,3 tetrachloroacetone

# 4.4 Summary of Effects of Chlorine Dose on NVCO Formation

As previously discussed, the chlorination of humic materials at low pH favors the formation of heavier products. Low chlorine doses also favor the formation of high MW components. Several workers have observed the same trends in the chlorination of pure compounds. Norwood et al. (1980) made these observations while chlorinating resorcinol. Rook (1979) observed an increase in  $CHCl_3$  concentrations, but a decrease in the larger chloro-resorcinol molecule. Onodera et al. (1984) observed the formation of chlorophenols and polychlorophenols upon the chlorination of aqueous solutions. These chlorophenols however, were further oxidized upon increased chlorine dosages (Fig. 9).

The results from the chlorination of these pure compounds may serve to illustrate the point that an optimum dose of chlorine exists, which would minimize the harmful products (possibly a choice between less toxic and very toxic).

#### 4.5 Precursors to NVCO

The notion that one precursor is responsible for all NVCO formation is as fruitless as the idea that only one precursor is responsible for THM formation. It now becomes a question of what is the major component that is most reactive with aqueous chlorine and is most responsible for the observed haloorganics.

The broadest observation and probably the least debatable assessment is made by Jolley. Jolley (1978) noted the great variety of natural organic



Residual amounts of reaction products in aqueous phenol solutions (50  $\mu$ mol/l) after treatment with hypochlorite at various equivalents of chlorine per mole of compound and 20°C for 1 h. Yields derived from GC peak areas, relative to the peak area of starting material. O, Phenol;  $\oplus$ , chlorophenols;  $\triangle$ , polychloropolyhydroxyphenols;  $\triangle$ , chlorophenol dimers.

Fig. 9: Chlorination of phenol at various chlorine doses. Reproduced with permission from Journal of Chromatography, Vol. 288, p. 98, 1984. Copyright 1984 Elsevier Science Publishers. Article authored by S. Onodera, K. Yamada, Y. Yamaji and S. Ishikura.

compounds in water and stated that most of them are reactive with chlorine.

Other workers have attempted to narrow Jolley's observations. Wong and Oatts (1984) filtered Chesapeake Bay water using ultrafilters with nominal MW cutoffs of 1000, 10,000, 30,000, and 100,000. They stated that ten to thirty percent of the chlorine demand was attributable to fractions with nominal MW above 10,000. The less than 1000 MW fraction had the greatest chlorine demand. The authors interpret the results to mean that fulvic acids are the most responsible for aqueous chlorine demand.

The results of Becher's (1985) ultrafiltration work corroborate Wong and Oatts' results. 82% of the TOX was from the less than 1000 MW fraction.

The findings of Reckhow and Singer (1984), however, contradict these claims. Reckhow asserts that humic acids are more TOX productive than fulvic acids. The discrepancy may lie in the difference of the water samples. In addition, Reckhow was working with concentrated extracts, whereas Becher and Wong and Oatts were using unextracted water. Reckhow's extraction methods may not have been effective for the low MW components.

Reinhard (1984) states that the less than 1000 MW fraction increases from 27% to 53% of TOC after tertiary treatment. This implies that the higher MW fractions are well removed by lime clarification, filtration, ozonation, biological activated carbon and a second filtration step at the Palo Alto, California water reclamation plant. These findings mean that lower MW TOC may be a very important reactant with aqueous chlorine in tertiary treated effluents. Wachter and Andelman (1984) note that both algal biomass and algal extracellular products (ECP) are as potent as humic materials in producing equivalent levels of TOX, THM and NPTOX.

Jolley (1978) had stated that carbohydrates are oxidized by chlorine and yield no chlorinated organics. Malcolm, Thurman et al. (1981) observed that the amount of carbohydrates associated with aquatic humics and fulvics changed significantly after chlorination. The carbohydrate content is reduced by 50% after chlorination. No work was done on the nature of the breakdown products.

The amino acids proline, analine (Stanbro 1979) and tryptophan yield chlorinated derivatives upon chlorination (Ingols 1954). In their work at the Yuma Desalting plant, Malcolm and Thurman (1981) observed changes in the concentrations of several amino acids after chlorination, implying their reaction with chlorine.

#### 4.6 Efforts to Minimize NVCO Formation

The efforts to minimize NVCO formation due to water chlorination are very similar to the efforts to combat THM production. One may remove the NVCO precursor before chlorination or remove the NVCO in the post chlorination water.

McCreary and Snoeyink used activated carbon to successfully reduce NVCO levels after chlorination. Johnson and Randtke (1983) used coagulation to decrease NVCO levels in chlorinated waters. Johnson and Randtke found the coagulation-flocculation scheme capable of removing both NVCO precursors and the formed NVCO. Both workers used total organic halogen (TOX) as the parameter to measure NVCO.

Reckhow and Singer (1984) found alum coagulation to remove THM, TOX, trichloroacetic acid, dichloroacetic acid and dichloroacetonitrile precursors to a significant extent. Ozone treatment in conjunction with alum treatment sometimes reduced treatment efficiency (compared to alum coagulation alone), presumably by breaking up larger molecules which were more amenable to coagulation.

Fleischacker and Randtke (1983) recommend low chlorine doses, high pH and the use of chloramines in order to minimize TOX levels. NPTOX levels were reduced by 79% by the addition of ammonia prior to chlorination.

Chow and Roberts (1981) found chlorine dioxide to produce only 17% of the TOX levels produced by free chlorine. The authors chlorinated secondary municipal wastewater effluent from Palo Alto, California. 20 mg of residual were applied for a 24 hour contact period. The TOX produced from the chlorination of another California treatment plan was reduced by 99% by using chlorine dioxide instead of free chlorine.

#### 5. LITERATURE REVIEW SUMMARY

Chlorination by-products can be subdivided into volatile (THM's) and non-volatile components. Volatile halogenated organics are best analyzed by GC. The non-volatile fraction (NPTOX) can be analyzed by GC, HPLC or TOX. Volatile chlorinated organics (THM's) are formed upon the chlorination of most drinking waters. Humic acids, fulvic acids, algal biomass and algal extracellular products were shown to be THM precursors. High pH, high chlorine dose, long contact time and elevated temperature maximize THM formation. Carbon adsorption, aeration, and disinfection using chloramines are viable THM remediation techniques.

NPTOX is also formed during the disinfection of water. Most organic carbon is reactive with chlorine to a certain extent leading to NPTOX formation. Some workers, with disagreement from others, state that the low MW fractions of TOC (in the water) are the most NPTOX productive upon chlorination. Carbon adsorption, chlorination with chloramines and alum coagulation followed by sand filtration have been shown to reduce NPTOX levels.

The formation of THM's and NPTOX during the chlorination of water are intimately related. Often the levels of one of the components of TOX is reduced, while the concentration of the other component is raised by varying chlorination parameters (chlorine dose, pH and contact time).

In the upcoming chapter (Results and Discussion), a similar relationship and dependence on chlorination parameters for the light and heavy components of gas chromatographable non-volatile chlorinated by-products is discerned. The precursors to these gas chromatographable halogenated compounds are characterized by MW and solubility. In addition, the treatment alternatives discussed in this chapter are examined for the reduction of this sub-group of TOX. An improved analytical protocol is also introduced for the analysis of the observed halogenated organics.

## **III. OVERVIEW AND PROCEDURES**

# 1. OVERVIEW OF EXPERIMENTAL TECHNIQUES AND EXPERI-MENTS

This research work has involved the development of an analytical technique for the analysis of gas chromatographable non-volatile chlorinated organics (NVCO), and the use of the developed protocol in a variety of experiments. Some of these experiments examined the nature of the NVCO. Another set of experiments focused on the identity of the precursors to the formation of these halogenated compounds. A third group of experiments were designed to assess the effect of chlorination parameters on the formation of the NVCO. The last group of experiments screened several treatment schemes to quantify their ability to reduce the levels of these chlorination by-products.

The experimental procedures used to achieve these goals can be divided into four broad categories. The ultimate sample analysis was always done using GC or GC/MS of a solvent extract. The sample extract, however, came from different origins. First, water from a tertiary wastewater treatment plant in San Diego, California was extracted with methylene chloride and the extract was analyzed gravimetrically, by GC and by GC/MS. This first category of experiments studied the nature of the extractable organics at the San Diego facility. Extractable organics were analyzed at various locations along the plant's treatment scheme. The results from the first category of experiments pointed out that chlorination produces an abundance of halogenated organic compounds in the plant's effluent.

The second category of experimental procedures involves laboratory chlorination of the pre-chlorination water from the San Diego facility. This category of experiments studied the effects of chlorination parameters, such as chlorine dose, pH and contact time on the production of the halogenated organics observed at San Diego facility. These experiments also confirmed that chlorination is the cause of the produced halogenated organics. Laboratory chlorination experiments were also used to assess the utility of various treatment schemes to reduce NVCO levels.

The third category of experimental procedures is laboratory chlorination of extractable (solvent extractable and XAD8 adsorbable) organics from the San Diego treatment plant. These experiments were used to assess the effect of chlorination parameters on the production of NVCO, and examine various treatment schemes. Fractionation of the organic extracts and the consequent chlorination of the various fractions yields information on the nature of the organic precursors which react with chlorine.

The last category of experimental procedures involved work with pure compounds. Various pure compounds were chlorinated as aqueous solutions in the laboratory and the breakdown products were analyzed by GC. In addition, sodium sulfite was added to pure compounds (as aqueous solutions) to assess the reactivity of the compounds with the  $SO_3^-$  ion.

Table 6 lists the experiments which will be discussed, classifies the experiments by one of the above mentioned categories and references the reader to the appropriate sections in the procedures description. Table 6 also indicates the research goal (goals listed in Table 1) that the experiment sup-

Experiment Number	Description of Experiment	lab procedure category	goal experiment supports	reference sections in procedures
1	Extractable organics at the San Diego treatment plant. 15 sampling dates; 6/84-3/86	1	1,3,B	1,4,5
2	Solvent extraction vs. XAD8 adsorption for collec- tion of NVCO precursors	2	2	1,2,4,5
3	Organic solvent elution of XAD8 extract and chlori- nation of the fractions	3	2	1,3,5,9
4	Humic/Fulvic split of XAD8 extract and chlorination of the fractions	3	2	1,3,5,9
5	Elution of XAD8 extract by pH gradients and chlori- nation of the fractions	3	2	1,3,5,9
6	Separation of XAD8 extract on enzacryl gel and chlorination of the fractions	3	2	1,3,5,9
7	Ultrafiltration of XAD8 extract and chlorination of the fractions	3	2	1,3,5,6
8	NVCO precursors in other treatment plants and other water samples	1,2,3	2	1,3,4,5,6,9
9	Chlorination of pure compounds	4	2	1,7
10	Addition of sodium sulfite to pure compounds	4	1,2	1,8
11	Chlorination of carbon adsorption effluent from San Diego Wastewater Treatment Plant	2	4	1,2

## Table 6 List of Performed Experiments

### Table 6 (continued)

Experiment Number	Description of Experiment	lab procedure category	goal experiment supports	reference sections in procedures
12	Chlorination of XAD8 extract	3	2,3,4	1,3,4,5
13	Effect of bromide ion on NVCO formation	3	4	1,3,5
14	Treatment of NVCO by activated carbon	2	5	1,2,9
15 16	Treatment of NVCO by use of chloramines Treatment of NVCO by use of ozone	3 3	4,5 5	1,3,5 1,3,5,9
17	Treatment of NVCO by 2 stage chlorination	2,3	5	1,2,3,5

Key: Category No.

analysis of solvent extracts
 chlorination of water samples
 chlorination of extracts
 work with pure compounds

Goal No. (see Table 1)

B = background information

ports.

# 2. DESCRIPTION OF THE SAN DIEGO WASTEWATER TREAT-MENT PLANT

The majority of the water samples used in this work were collected at the San Diego water hyacinth tertiary wastewater treatment plant named "Aqua I". The treatment plant is a pilot testing and demonstration facility. It is the first step in the City of San Diego's plan to build a large (MGD scale) aquaculture based treatment facility.

Raw sewage (85% domestic, 15% industrial) is first subjected to mechanical grinding. The sewage, free of large debris, next passes to several mildly aerated aquaculture fields. Water hyacinth, small fish and other aquatic organisms provide the secondary treatment. The aquaculture effluent next passes through UV sterilizers en route to a sand filter. Before entering a reverse osmosis (RO) unit, UV sterilization is again performed. The pH also is lowered to 4-5 in order to preserve the membranes. The RO unit operates at 400-600 psi with a permeate flow of 50 gpm. Cellulose acetate membranes are used in conjunction with other thin layer composite membranes that the treatment plant is testing. The RO effluent next passes over activated carbon before final chlorination at pH 5.

The chlorination is done using sodium hypochlorite (NaOCl). A free chlorine residual of 1.0 to 1.5 mg/L is maintained in the 10,000 gallon chlorination tank. The chlorination procedure is non-standard. The chlorine residual is periodically checked and always maintained above 1 mg/L. New (unchlorinated) water is only added to the tank when the water level drops

below 3000-4000 gallons. The chlorinated product water is used to feed animals kept at the plant, and for irrigation around the plant. Most of the plant's effluent is discharged after reverse osmosis. Water passes through the carbon adsorption columns and is chlorinated only when the water level in the chlorination tank drops. Figure 10 provides a schematic of the treatment plant.

The schematic shown in Figure 10 represents the treatment process train which was selected by the City of San Diego for its ultimate MGD scale expansion. Other unit operations including ultrafiltration and ozonation exist at the plant but were tested and not selected for the eventual expansion.



Fig. 10 Schematic of the San Diego Wastewater Treatment Plant
#### **3. ANALYTICAL PROCEDURES**

#### 3.1 Extractable Organic Analysis

A modification of an extraction procedure previously developed to quantify total extractable organics in runoff waters was used (Stenstrom, Fam, Silverman, 1984). Using the automated shaker/stirrer shown in Figure 11, up to four liters of water may be easily extracted. This methodology enables the extraction of large amounts of extractable organics for accurate gravimetric analysis. Gravimetric analysis was used in the preliminary screening of the extractable organics present in the San Diego plant.

A large volume of water (1 to 4 liters) was acidified to pH 2 with concentrated sulfuric acid. Sodium chloride (5 g/l of water) was added to the extraction vessel before extraction. The sample was then extracted with three successive portions of methylene chloride (60 ml  $CH_2Cl_2$  per liter of water) for five minutes. 1-bromohexadecane, hexadecene, tetradecane, m-cresol, or o-chlorophenol was used as a recovery standard depending on the chromatographic pattern of the sample. All of these standards interfered with some of the peaks to a certain extent due to the complexity of the chromatographs. The areas of these standards were subtracted prior to all quantitative calculations. No corrections were made to any of the GC results. If a sample showed low recovery (<90%) it was repeated. The recovery standards consequently were used only as a check that the extractions were of high efficiency. Most of the GC's shown in this dissertation were chosen without internal standards to minimize interference with the sample peaks. The combined methylene chloride extract was then reduced to approximately 40 ml by rotoevaporation



Fig. 11 Extraction Apparatus

at 32°C. The concentrated extract was then dried with sodium sulfate to adsorb any remaining water. The water free samples were stored in 5 to 10 ml of methylene chloride in a stoppered 25 ml round bottom flask at 2°C until they were analyzed (storage period was usually less than four hours).

GC analysis is performed with a Varian Vista 6000 instrument equipped with both a flame ionization and an electron capture detector in a splitless mode. The two detectors work in parallel by means of an SGE fused silica splitter.

A fused silica column (30m) wall coated with Carbowax 20M (.25 mm id) and a 22 meter fused silica SP2100 column were used for the initial chromatograms. Neither column performed optimally, the SP2100 provided a high temperature capability, but poor resolution. The Carbowax column provided good separation of the light compounds, but was unable to handle the heavier components. A Supelcowax 10, 30 meter fused silica column was finally chosen. The resolution is as good as the Carbowax column and the maximum safe operating temperature is 260°C which is almost as good as the SP2100. All chromatograms discussed henceforth are produced using the Supelcowax column, unless specifically stated otherwise.

Extracted samples were very gently evaporated to near dryness (one drop left) at 32° and low evaporator pressure. The sample residue was then redissolved (no visible, undissolved residue was observed) in an appropriate amount of methylene chloride (usually 1.0 ml) to render a good chromatogram at range  $10^{-12}$  and an attenuation of 16 or 32 (about 5 ng/ul injected). Helium was used as the carrier gas at a pressure of 14-16 psig. The initial column

temperature was 65°C with an initial four minute hold. The oven temperature was then programmed to 260 at 4° per minute. The column temperature was held at 260 for 30-55 minutes. The injection port was set at 250°C and the detector oven maintained a 280°C temperature. Peak areas were integrated using a Hewlett Packard model integrator. The integrated area report was stored on floppy disks by a personal computer (PC) connected to the integrator. All calculations and data analysis were performed on the PC using the stored data.

GC/MS samples were run using the Supelcowax 10 column. The MS instrument is a Finnigan 4000 series. Table 7 shows the extraction efficiency of this procedure for a variety of compounds and points out the reproducibility of the method.

#### **3.2 Laboratory Chlorination of Water Samples**

One liter volumes were used for all chlorinations. The appropriate amount of calcium hypochlorite solution is added from a prepared and calibrated solution. A 4 mg/ml stock solution of  $CaOCl_2$  was prepared in distilled Arrowhead water. The pH of the chlorinated water is then immediately adjusted with 1N HCl or 1N NaOH to the desired acidity. The pH adjustment is done in less than one minute. In the instance where ammonia or bromide ion was added, the addition was done before pH adjustment. The ammonia solution was prepared as 70 mg  $N-NH_4/ml$  from  $NH_4Cl$  in distilled Arrowhead water

## Table 7

# Method Extraction Efficiency

Compound	Area of Standard	Extract 1	Extract 2	% Recovery
	$(x10^{-3})$	Area	Area	(Average)
2-octanone	54.9	50.6	50.9	92.4
2-nonanone	67.8	65.4	66.7	97.3
tridecane	95.1	90.2	87.2	93.2
1-tridecene	86.6	80.1	82.5	93.7
hexadecane	55.1	54.5	56.5	100.7
1-hexadecene	79.0	78.9	81.8	101.6
decanol	49.7	51.7	55.7	108.0
octadecane	65.4	68.8	71.0	106.0
1-octadecene	91.5	94.4	97.1	104.0
1-chloro-phenol	27.5	21.3	23.2	80.7
phenol	52.6	22.6	20.1	40.4
2,5 dimethylphenol	49.7	48.8	48.4	97.7
m-cresol	76.6	62.8	59.0	79.5
hexadecanone	78.3	83.6	83.6	106.0
O-N-propylphenol	67.7	67.2	69.4	101.0
2,3 dimethylphenol	97.6	96.5	96.5	98.8
4-t-butylphenol	162.2	162.8	162.8	101.0
2,4,5 trichlorophenol	9.9	9.7	10.0	100.0
1-hexadecanol	41.1	44.6	43.8	107.0
1-octadecanol	18.0	17.9	16.1	95.0

The chlorinated solution was stirred in a constant temperature  $(25^{\circ}C)$  bath for the appropriate time before extraction. The extraction and GC analysis proceeded as previously described. Sodium sulfite was only added in experiments where sodium sulfite dose was used as a variable. In such instances a 6 mg/ml solution was used.

#### **3.3** Chlorination of Extracts

Solvent extractable organics and XAD8 adsorbable organics from the aquaculture effluent were subjected to chlorinations as concentrated 15 ml solutions. One mg (measured as TOC) of XAD8 extract (procedure described below) was added to an appropriate amount of distilled Arrowhead water so that after addition of chlorine (and ammonia) solution, the total volume is 15 ml. Chlorine was added as a 4 mg/ml solution followed by pH adjustment. The 25 ml flask was then stirred for the appropriate time before extraction.

The aquaculture effluent solvent extractable organics were extracted as previously described. The aquaculture solvent extract was consequently fractionated into three fractions by silica gel column chromatography (described below). Each of these three fractions, as well as the total extract, were chlorinated. It was found necessary to add 2 ml of methanol to dissolve some of the extracts. Procedural blanks using methanol showed that addition of alcohol does not introduce any new variables. The chlorination of the organic extracts was identical to chlorination of the XAD8 extracts except for the initial solubilization of the organic solvent extract in 2 ml of methanol. Extractions were done in 60 ml separatory funnels. After the addition of NaCl and sulfuric acid, the reaction flask was rinsed with 25 ml of methylene chloride. The wash was added to the separatory funnel. The funnel was violently shaken by hand for one minute. The combined three extracts were evaporated and dried as previously described.

#### 3.4 Silica Gel Column Chromatography

A 14 cm silica gel packed column (1.9 cm diameter ) was used to separate the extracted organics into three fractions. The silica gel was soxhlet extracted with  $CH_2Cl_2$  overnight prior to use as well as being rinsed with two column lengths of each solvent used. An aliphatic non-polar fraction was eluted with two column lengths of hexane. An aromatic non-polar fraction was eluted with two column lengths of benzene and a third polar fraction was collected with two column lengths of 1:1  $CH_2Cl_2$ :methanol and two column lengths of methanol.

#### **3.5 XAD8 Adsorption**

The water samples were adsorbed on XAD8 resin purchased from Rohm and Haas. The procedure used was a modified version of a protocol described by Malcolm (Thurman and Malcolm 1981) for the collection of fulvic and humic acids.

The resin was washed in .1N NaOH for six days with daily change of the wash solution or until the TOC of the wash solution drops below 10. The NaOH washed resin was then washed in diethyl ether (soxhlet extracted) for 24 hours followed by extraction in methanol for 24 hours. The resin was then packed onto a glass column and rinsed with distilled water until the TOC drops below 1 (about 3 gallons of water). The packed column was then alternately rinsed with .1N NaOH and .1N HCl 3 times.

The filtered (.45 micron) pH 2 sample was then passed onto the cleaned XAD8 column. The adsorbed organics were desorbed with three bed volumes of .1 N NaOH. The extract was reacidified to pH 2 and consequently read-sorbed onto a smaller XAD8 column in order to concentrate the solution. It was desorbed with .1N NaOH. No fulvic/humic split is made. The solution was adjusted to an appropriate volume to yield the desired TOC level.

#### 3.6 Ultrafiltration

40 ml of the XAD8 (4 mg TOC) adsorbable extract were fractionated into five nominal molecular weight ranges by four ultrafilters. The ultrafilters have nominal MW cutoffs at 100,000, 30,000, 10,000 and 1,000 and were purchased from Millipore Inc. High purity nitrogen gas at 110 psi was used to force the pH 7 extract through the membranes. Each membrane was rinsed with two 10 ml aliquets of high purity water (distilled Arrowhead water) and the wash was combined with the filtrate for passage through the next smaller membrane size. The residue from the 100,000 MW, the 30,000 MW and the 10,000 MW filters was desorbed by overnight stirring in 40 ml of .1N NaOH. The residue from the 1,000 MW filter was stirred overnight in pH 9 water. The less than 1,000 MW fraction was collected as a 120 ml solution, which is 40 ml of the original solution, plus 80 ml of washes. The solution was not reconcentrated.

#### 3.7 Chlorination of Pure Compounds

Approximately 5 mg TOC of several pure compounds were chlorinated as concentrated 10 ml solutions in water. The TOC was calculated theoretically and was consequently measured gravimetrically. The chlorination procedure is identical to the chlorination of the XAD8 extracts. A chlorine dose giving a 2:1 Cl:C ratio was applied. All chlorinations were done at pH 7 for two hours.

#### 3.8 Addition of Sodium Sulfite to Pure Compounds

Approximately 5 mg of each pure compound was dissolved in 2.5 ml of water. Water insoluble compounds were dissolved in methanol and methanol solutions yielding 5 mg of the compound (usually 20  $\mu$ l) were added to the water. A control (no  $SO_3^-$ ) sample was extracted with 5.0 ml  $CH_2Cl_2$  for compounds eluting at temperatures higher than 75°C or 5.0 ml of pentane for early eluting compounds. The extraction was done in a 10 ml vial.

Sodium sulfite (excess) was added to an identical sample vial and the vial is allowed to stand at room temperature for 15 minutes before extraction. The control and sulfite containing sample were gas chromatographed at the previously described conditions. All samples were analyzed in triplicate.

#### **3.9 TOC and Gravimetric Analysis**

TOC measurements were run in triplicate using an Ionics TOC analyzer (Model 1270) which employed a combustion-infrared method for the analysis of soluble and purgable TOC. Acetic acid was used to prepare standards for each analytical run. Gravimetric analysis was performed using a Mettler Electrobalance.

#### 3.10 Other Procedures

There are several other procedures which were used. These procedures were not used routinely and will be described when the appropriate experiment is discussed. Table 8 is a list of these protocols.

#### Table 8

### Other Procedures

- 1. Elution of XAD8 adsorbable organics by organic solvents.
- 2. Elution of XAD8 adsorbable organics by pH gradients.
- 3. Fractionation of XAD8 extract by enzacryl gel.
- 4. Humic/fulvic split of XAD8 extract.
- 5. Treatment of NVCO by powder activated carbon.
- 6. Treatment of NVCO by ozone.
- 7. Treatment of NVCO by aeration.

#### 3.11 Reagents

All reagents were analytical grade or better. All solvents were distilled before use. The sodium chloride and sodium sulfate are baked at 550°C for at least four hours before use. All aqueous reagents were prepared in distilled Arrowhead brand water. Arrowhead brand drinking water was found to be superior to the laboratory distilled tap water and Sparkletts brand drinking water (contained fewer GC peaks). The Arrowhead brand water was distilled in glass in the laboratory before use. Teflon tape was used in place of stopcock grease at all times.

#### **IV. RESULTS AND DISCUSSION**

# 1. SOLVENT EXTRACTABLE ORGANICS AT SAN DIEGO (BACK-GROUND ORGANICS)

Solvent extractable organics were collected at the San Diego Wastewater Treatment Plant on fifteen different dates. Initially, both acid and base neutral extracts were analyzed (separately, not successively). It was found that the GC output was similar, but not identical, for both extracts. Gravimetric and GC analysis (total FID area) showed that the Base Neutral extract was roughly about 65% of the acid extract. Consequently, only acid extractables were analyzed after the 3/85 sampling date. Some of the data from eight of these sampling dates are presented in this section as background information on the nature and concentration of organics in the secondary effluent, as well as the treatment efficiency of the various unit operations. The other seven sampling dates do not provide information on background organics at the treatment plant.

The treatment scheme at the San Diego plant has been previously described. Table 9 is a summary of the gravimetric data accumulated during 1984-1986 at the San Diego plant.

It is quite apparent from Table 9 that the treatment scheme at San Diego is quite effective in reducing the extractable organic levels from the secondary effluent. The reduction in treatment efficiency from 97 to 93 percent after chlorination indicates that chlorination has broken down organic carbon which prior to chlorination was not solvent extractable. This assertion is validated by gas chromatography of the extracts.

Date	Aquaculture Efficent mg/L	Sand Filter Effluent mg/L	% Reduction	RO Effluent mg/L	% Reduction	Carbon Adsorption Effluent mg/L	% Reduction	Chlorinat. Product mg/L	% Reduction
11/84	4.04	ND		ND		ND		0.22	
ævg	4.48 4.26	nd Nd		nd ND		nd Nd		0.34 0.28	. <b>93</b>
1/85	<b>6.5</b> 1	ND		0.55		ND		0.34	
ævg	5.55 6.03	ND ND		0.58	<del>9</del> 0	ND		0.18 0.26	<b>9</b> 6
3/85	6.10	ND		ND	<u></u>	ND	-	0.46	
ævg	6.62 6.36	nd Nd		nd Nd		ND ND		0.69 0.57	91
4/85	ND	3.18		0.41	ND		ND		
5/85	3.71	ND		ND		ND		ND	
6/85	4.88	4.45	9	0.52	89	0.21	<b>9</b> 6	0.31	94
7/85	5.22	3.88	25	0.27	95	0.14	97	0.34	93
4/86	3.33	ND	<u> </u>	ND		ND		ND	
Total			·						
avg	5.04	3.84	24	0.47	91	0.18	97	0.36	93
key									

### Table 9 Gravimetric Data for Total Acid Extractable Organics

avg = ND =

g = average of duplicate values

ND = not determined

% reduction is based on aquaculture effluent value

The aquaculture effluent from 5/85, 7/85, as well as 4/86, was fractionated by silica gel column chromatography into three fractions of increasing polarity. The first fraction generally contains aliphatic hydrocarbons. The second fraction contains aromatic hydrocarbons, cyclic unsaturated hydrocarbons, as well as alkyl benzene and alkyl phenolic surfactants. Fraction three contains polar compounds such as phenols, acids and alcohols. Some compounds are not elutable from the silica gel column and are thus called nonelutable polars (NEP). Table 10 points out that gravimetrically, the extract is mainly composed of polar compounds, but that gas chromatographically (based on total areas from the FID detector) the non-polar fractions represent a sizeable percentage of the gas chromatographable compounds. This is not surprising since polar compounds are less amenable to gas chromatography.

Table IU	Tal	ble	10	
----------	-----	-----	----	--

General Makeup of Aquaculture Effluent Extract

Date	% grav. frac. 1+2	% GC(FID) frac. 1+2	% grav frac. 3+NEP	% GC(FID) frac. 3+NEP
5/85	25.5	72.0	74.5	28.0
7/85	27.4	79.0	72.6	21.0
4/86	42.3	57.0	57.7	43.0

It is possible to estimate the percentage of the gravimetric extract that is represented by gas chromatographable peaks. Different compounds give a different area response count by the FID detector to the same amount (by mass) injected into the same column under identical chromatographic conditions. An estimate of 5,000 (acids) to 15,000 (hydrocarbons) area counts per nanogram of compound can be used as "ballpark estimates" which should give a range for the concentrations given by the total FID area counts.

Table 11 provides a comparison of the treatment of organics using gravimetric data, total FID areas and total ECD areas. A percentage of the gravimetric value that is represented by the FID areas is also estimated. The treatment of non-gas chromatographable compounds is slightly better than treatment of the smaller gas chromatographable compounds. This fact is also reflected in the percentage of the gravimetric weight that is represented by FID peak areas. This percentage is higher for the carbon adsorption effluent (15-44% in 6/85) than for the aquaculture secondary effluent (8-24% in 6/85).

Table 11 also clearly illustrates the dramatic effects of chlorination. The increase in total FID (decrease in treatment) area indicates the breakdown of larger molecules which prior to chlorination were not amenable to gas chromatography. The increase in total ECD area indicates that many of these breakdown products are halogenated.

The aquaculture effluent extracts from 11/84 and 4/86 were analyzed by GC/MS for positive identification of some of the compounds in the extract. The GC/MS in 11/84 was run by James Montgomery Engineers Laboratory. The results from Montgomery Engineers are of poor quality and will not be discussed. The 4/86 GC/MS was run at UCLA and provided for tentative identification of numerous compounds. The sparse use of MS data is due to the unavailability of a quality Mass Spectrophotometer on a routine basis at the time that the experimental work was done.

Sampling	%Rea Grav	duction imetric	% Re FII	duction Darea	% Re EC	duction D area	% of gr is in	av. that FID
1 0	6/85	7/85	6/85	7/85	6/85	7/85	6/85	7/85
Aquacult.	-	-	-	-	-	-	8-24	4-12
Sand Filt.	9	25	23	24	18	27	7-21	4-12
RO	89	95	82	78	47	79	14-42	12-36
Carbon	96	97	93	96	78	95	15-44	14-42
Chlorinated Effluent	94	93	63	80	25	80	48-145	40-120

### Table 11 Comparison of Reduction Efficiencies

Key:

% Reduction based on aquaculture effluent values

% of grav. that is in FID = % of the gravimetric weight that can be accounted for by FID peak areas.

The GC data collected during and after 7/85 was saved on floppy disks. It was consequently possible to match retention times of the aquaculture effluent GC extracts form 7/85 and 4/86. This was done in order to assess the reduction of the individually identified peaks from 4/86 with the complete treatment plant sampling done in 7/85. It was not possible to do a complete plant monitoring in 4/86 because the RO unit was not operable.

Figure 12 is the GC output for the aquaculture effluent (4/86) showing both ECD and FID detectors. Figure 13 is the reconstructed chromatogram from the GC/MS of the same sample. Table 12 lists the compounds in the extract which were tentatively identified and their approximate concentrations. Table 13 shows how well some of these compounds were treated along the plant's treatment train during the 7/85 sampling.

It is interesting to note that the RO unit is ineffective in removing nonyl-phenol and its related compounds. These compounds are effectively removed after carbon adsorption. Figure 14 is fraction 1 (aliphatics) from the aquaculture effluent. This extract greatly resembles motor oil extracts previously analyzed (Stenstrom, Fam, Silverman 1984). Figure 15 is the chromatogram of fraction 2 of the aquaculture effluent. The nonyl-phenol series of compounds is clearly visible in this chromatogram. Figure 16 is the total RO extract chromatogram. One observes that the surfactant series comprises a large portion of the extract (compare Figures 15 and 16).

Examination of the ECD peaks form the 7/85 sampling date points out that 109 new halogenated compounds were formed after chlorination (this analysis is not easily performed for samples collected prior to 7/85, since the output was not saved on disks). In addition, several compounds which were present in the aquaculture effluent showed significant increases (greater than 500%) after chlorination. This is quite expected since the water entering the treatment plant had previously been chlorinated by the City of San Diego. The halogenated organics are apparently well treated by the aquaculture fields, but reappear after chlorination.

In summary, the aquaculture effluent is mainly comprised of fatty acids (human waste), hydrocarbons (refined oils and biogenic ( $C_{31}$  n-alkane)), surfactants (from household detergents), pthalate compounds (plasticizers), cholesterols (human waste) and low amounts of halogenated compounds (industrial use and chlorination by-products). The RO unit effectively removes most of these compounds except for the detergents. Carbon adsorption provides final polishing for nearly 97% overall treatment of these compounds. The non-gas chromatographable compounds are also well treated as can be seen from the gravimetric data. Chlorination results in the production of an abundance of gas chromatographable halogenated compounds and is the problematic treatment step at the San Diego Treatment plant.

A mixture of 23 compounds of different polarity and MW was passed through the RO unit (4/17/86) to assess its selectivity towards the various organics. This data is presented in tabular form in Appendix 1. As expected the RO unit treats less polar large MW compounds more effectively. Figure 17 illustrates the effect of MW on the treatment of C12, C14, C16 and C18 straight chain fatty acids (from the 7/85 sampling date).

			Approximate	:
Scan No.	Compound Name	Method of	Conc.	% Confidence
	or Structure	ID	µg/L	in ID
243	decane (is)	1.2.3	10.0	>95
251	$C_{11}$ aliphatic	1.2	0.5	70
291	CH <sub>2</sub> ClBr	1,2,3	2.5	>95
447	CH <sub>2</sub> CII	1.2	2.5	>95
461	chloro-benzene	1,2,3	2.3	>95
476	$C_{12}$ aliphatic	1,2	0.4	70
586	$C_0$ alcohol	1.2.	1.8	60
597	3-heptanol 3.6 dimethyl	1.2	0.6	70
614	$C_{0}$ alcohol	1.2	0.6	70
660	tetradecane (is)	1.2.3	9.4	>95
709	1.4 dichlorobenzene	1.2.3	0.5	>95
754	1.3 dichlorobenzene	1.2.3	3.1	>95
897	cyclohexanone 4-(1,1 dimethyl ethyl)	1,2	1.3	80
915	1-hexanone 1-phenyl	1.2	0.6	90
1146	tetradecanal	1.2	1.4	80
1152	benzene (1-pentyl-heptyl)	1.2	1.4	>95
1178	$C_{10}$ aliphatic	1.2	6.5	80
1196	hexanoic acid 3,5,5 trimethyl	1,2	3.6	90
1277	m-creosol (is)	1,2,3	10.8	>95
1312	hexadecanal	1,2	3.7	80
1346	2-chloro benzeneamine	1,2	5.1	90
1409	$C_{8}H_{12}O_{2}Cl_{2}$	2	10.2	90
1481	1-hexadecanol	1.2.3	8.9	95
1562	1-dodecanoic acid	1,2,3	8.2	>95
1616	1-octadecanol	1,2,3	26.5	95
1642	2,3 dichlorobenzeneamine	1,2	4.5	90
1663	branched $C_{14}$ acid	1,2	15.3	95
1682	4-nonylphenol	1,2	5.6	95
1692	1-tetradecanoic acid	1,2,3	28.1	>95
1701	long chain alkyl phenol	1,2	4.2	95
1713	long chain alkly phenol	1,2	4.4	95
1725	1-pentadecanoic acid	1,2	38.9	95
1736	branched $C_{15}$ acid	1,2	28.4	95
1755	branched $C_{15}$ acid	1,2	14.9	95
1814	1-hexadecanoic acid	1,2,3	85.4	>95
1824	branched $C_{16}$ acid	1,2	72.8	95
1870	branched $C_{16}$ or $C_{17}$ acid	1,2	21.9	90
1915	$C_{31}$ n-alkane	1,2,3	35.5	>95
1962	1-octadecanoic acid	1,2,3	97.5	>95
1990	1-nonadecanoic acid	1,2	52.7	95

# Table 12Compounds Identified in the Aquaculture Effluent<br/>During the 4/86 Sampling by GC/MS

Conc. μg/L	% Confidence in ID
43.6	
ND	90
ND	<b>9</b> 0
ND	<b>9</b> 0
ND	90
ND	<b>9</b> 0
ND	<b>9</b> 0
ND	95
ND	95
	43.6 ND ND ND ND ND ND ND ND ND ND ND ND ND

# Table 12Compounds Identified in the Aquaculture EffluentDuring the 4/86 Sampling by GC/MS (Continued)

#### Key:

- manual interpretation of MS data 1.
- 2.
- computerized matching of MS data GC retention time matched with known standards 3.
- not determined because peaks are too broad confidence in ID is a personal judgement ND
- %
- concentrations evaluated based on area response of similar classes of compounds.
- (is) internal standard

	scan	% Trea	tment After	
	No.	RO	Carbon	
Compound	(4/86 Sample)			
1,3 dichlorobenzene	754	99.5	100.0	
tetradecanal	1146	56.0	100.0	
$C_{19}$ hydrocarbon	1178	83.2	100.0	
$C_9$ branched acid	1196	86.0	100.0	
2, propenal 3, phenyl	1247	91.3	100.0	
hexadecanal	1312	58.6	98.4	
2 chloro-benzeneamine	1346	46.6	97.3	
$C_{22}$ hydrocarbon	1354	85.8	100.0	
$C_{8}H_{12}O_{2}Cl_{2}$	1409	88.7	100.0	
1-hexadecanol	1481	73.1	100.0	
1-dodecanoic acid	1562	47.0	81.5	
2,3,dichlorobenzamine	1642	98.1	98.7	
branched $C_{14}$ acid	1663	57.2	89.5	
4-nonyl phenol	1682	39.1	100.0	
long chain alkyl phenol	F2	31.1	100.0	
long chain alkyl phenol	F2	12.4	91.3	
long chain alkyl phenol	F2	7.6	100.0	
long chain alkyl phenol	F2	34.8	93.5	
1-tetradecanoic acid	1692	50.2	95.1	
long chain alkyl phenol	F2	49.2	100.0	
1-pentadecanoic acid	1725	74.6	100.0	
long chain alkyl phenol	F2	38.5	100.0	
long chain alkyl phenol	F2	17.2	92.9	
long chain alkyl phenol	F2	4.0	100.0	
branched $C_{15}$ acid	1755	72.8	100.0	
1-hexadecanoic acid	1814	94.8	100.0	
$C_{31}$ n-alkane	1915	92.2	97.4	
1-octadecanoic acid	1962	94.7	83.0	
pthalate compound	2110	100.0	74.1	
pthalate compound	2146	100.0	100.0	
pthalate compound	2221	52.4	100.0	
pthalate compound	2297	72.2	100.0	
pthalate compound	2324	100.0	100.0	
pthalate compound	2380	100.0	100.0	
pthalate compound	2509	100.0	100.0	

# Table 13 Treatment of Some of the Identified Compoundsin the Aquaculture Effluent during the 7/85 Sampling

Key: F2 - compound not clearly identified in the 4/86 MS output but was present in the 7/85 sample as a fraction 2 compound eluting near nonyl phenol (see Figure 16).

Compounds not listed in this table but listed in Table 12 were not present in the 7/85 sample.



Fig. 12: GC of the aquaculture effluent total extract. GC conditions as specified in analytical procedures. Some MS scans are labeled. See Table 12 and Fig. 13 for complete listing. Axes are labeled for the FID.



Fig. 12 (Continued)



Fig. 12 (Continued)







Fig. 14: GC of fraction 1 of the aquaculture effluent extract. GC conditions as specified in analytical procedures. n-alkanes are labeled according to the number of carbons. Axes are labeled for the FID.



Fig. 14 (Continued)



Fig. 15: GC of fraction 2 of the aquaculture effluent extract. GC conditions as specified in analytical procedures. Axes are labeled for the FID. Compound ID in Table 12.



Fig. 16: GC of RO effluent total extract. GC conditions as specified in analytical procedures. Axes are labeled for the FID. Compound ID in Table 12.





## 2. IDENTIFICATION OF SOME OF THE NVCO BY GC/MS

The initial samplings at the San Diego treatment plant clearly indicated that chlorination was the problematic treatment step (Tables 9 and 11). An abundance of new halogenated organics are detected by GC and GC/MS.

Some of the compounds are identified by name, others are identified by molecular formula, and several other compounds are only identified by molecular weight or number of halogenated atoms in the molecule. Each sizeable ECD peak produced after disinfection, regardless of its level of identification, is given a reference number. This reference number allows discussion in upcoming chapters on the formation of a particular peak (compound), its precursors, and its treatment. Any other compound which is well identified (regardless of its magnitude) is also given a reference number.

Figure 18 is the gas chromatograph of the extract from the chlorinated product water at the San Diego plant (March 1986). The abundance of halogenated (ECD) peaks is overwhelming. The major ECD peaks, as well as other identified compounds are labeled by reference number in Figure 18. Background compounds (present in the aquaculture effluent) are labeled 'B' and are identified in Table 13. Background peaks which are pthalates are labeled 'P'. The early eluting halogenated compounds are labeled 'A#' and the late eluting chlorinated organics are labeled 'D#'.

It was observed that XAD8 (adsorption resin) adsorbable organics from the aquaculture fields effluent yield a very similar pattern of halogenated organics upon laboratory chlorination (this observation will be discussed in greater detail in upcoming chapters). The chlorinated product water from the San Diego plant contains halogenated compounds produced during disinfection as well as background halogenated compounds. Since the XAD8 extract does not contain any background halogenated organics (they are not collected by the adsorption/desorption procedure i.e., they are only desorbable by an organic solvent from the XAD8 resin), but contains the majority of chlorination by-products, it provides a simpler chromatographic system for the identification of the organic compounds produced during disinfection.

Figure 19 is the gas chromatograph of laboratory chlorinated XAD8 extract. The similarity of this chlorinated extract to the chlorinated product water from San Diego (Figure 18) is very clear. The major difference is that the large hump eluting at 45-50 minutes in Figure 18 is not present in Figure 19. Only a few of the compounds producing this hump were identified. These compounds were present in large concentrations on occasion (Figure 18) and on other occasions their concentrations were much less.

Since the ECD is much more sensitive than either an FID or an MS detector, thirty times more XAD8 extract was chlorinated than that shown in Figure 19 in order to produce MS detectable compounds. Figure 20 is the GC of this concentrated extract and Figure 21 is the equivalent reconstructed MS chromatogram. Unfortunately, this concentrated extract contains fatty acids from the aquaculture effluent which slightly complicates the chromatograph (labeled B in Figure 20). Some of the ECD peaks in Figure 20 appear very broad due to the high concentrations used. The axes in Figures 18, 19, and 20 are labeled for the ECD. The FID is offset slightly to the left.

A GC/MS analysis was performed for the chlorinated product water from the San Diego (December 1985) plant. Unfortunately, the abundance of compounds in the extract did not allow for good MS identification. Comparison of the MS output from the San Diego product water and the chlorinated extract would usually reveal that the San Diego effluent MS scans contain extraneous fragments from carryover of neighboring compounds. Although fractionation of the San Diego extract and the consequent MS analysis of the fractions would remedy this problem, due to time, equipment limitations, and satisfaction with the XAD8 MS results the fractionation was not performed. The GC/MS scans for the identified compounds are shown in Appendix 2.

Table 14 lists the identified compounds, method of identification, percent confidence in the identification, approximate concentration of the compound in the San Diego effluent (average value from all collected samples), GC retention time and compound reference number for upcoming discussion. A personal communication with R. Christman and D. Norwood indicated that they had not encountered some of these compounds (1986).

The following generalizations can be made about the produced halogenated organics. First, in agreement with Miller (1983), Coleman (1984), Kringstad (1985), Quimby (1980), Snoeyink (1981) and McCreary (1981) chlorinated aromatic compounds were observed. Christman et al. (1979, 1981) only observed aliphatic halogenated compounds in their work with chlorinated humic and fulvic acids. Second, many of the observed halogenated compounds are unsaturated and contain oxygen atoms. Some unsaturated halogenated compounds are reactive with dechlorinating agents and have consequently escaped detection by several workers in the past. The chapter entitled "Effects of Dechlorinating Agents" details this observation.

Third, many of the compounds contain more than one chlorine atom and consequently produce much more response in the ECD detector (the ECD detector is only sensitive to halogenated compounds) than in the FID detector. Although the FID detector responds to all molecules, it gives the best response to carbon-hydrogen bonds. Since many of the observed halogenated organics are unsaturated (fewer carbon-hydrogen bonds) and are poly-chlorinated, this magnifies the difference between the response of the two detectors.

Fourth, the identified halogenated compounds most closely resemble the structures identified by Coleman, et al. (1984) (Table 4). This is likely due to the fact that Coleman did not add any dechlorinating agents to his samples prior to extraction. Most workers (Christman (1981), Quimby (1980), Miller (1983)) dechlorinate their samples prior to extraction and, as will be discussed in Section 5, sodium sulfite has been found to be reactive with several of the observed compounds. The reaction between the dechlorinating agents and the halogenated compounds precludes their chromatographic identification.

Fifth, the unavailability of a GC/MS on a routine basis precluded more positive identification of the compounds listed in Table 14. It is highly recommended that sample fractionation be performed prior to GC/MS identification in order to minimize carryover. In addition, many of the produced halogenated organics have weak molecular ion intensities which is typical of halogenated aliphatics. Chemical ionization mass spectroscopy would consequently be recommended to assist in more positive identification.
Scan No.	Identification	RT (min.)	Method of ID	% Confidence in ID	ref.	Concentration in chlorinated SD final effluent average (ppb)
255	chloroform	-	1,2,3	>95	E1	ND
279	chloro- bromomethane	-	1,2,3	>95	E2	ND
303	dichloro-propane	-	1,2	90	E3	ND
356	dichloro-cyclohexene	5.52	1,2	60	A1	3.1
383	unknown unsaturated chlorinated compound	6.39	-	-	A2	5.0
-	unknown	6.67	-	-	A3	0.5
429	chloro-iodo methane	7.80	1	>95	A4	0.8
439	2-propanone 1,1 dichloro	8.00	1,2	90	A5	5.7
443	2-propanone 1,1,1 trichloro	8.28	1,2	90	A6	10.0
481	$C_3NCl_3$	9.17	1	60	<b>A</b> 7	0.7
496	1-propene 1,2,3,3 tetrachloro	9.46	1,2	80	<b>A</b> 8	<.5
-	unknown	9.85	-	-	A9	<.5
505	unknown	9.91	-	-	A10	0.4
513	C4H6Cl3N	10.64	1	60	A11	1.0
<b>5</b> 41	$C_5H_8Cl_2$	11.17	1	90	A12	2.9
<b>5</b> 55	MW 152, 2 chlorines $C_4H_2O_2Cl_2$	11.94	1	60	A13	0.3
615	C 5H 3Cl 3O	13.25	1	70	A14	4.6
642	cyclopentanol 1,2 methyl	14.24	1,2	90	A15	1.5

# Table 14 Halogenated Compounds Produced during Disinfection

.

672	C 5H 5Cl 3O	15.25	1	90	A16	<.5
695	pentachloropropene	15.83	1	90	A17	1.5
702	C 5Cl 3H 5O	16.49	1	90	A18	3.3
733	MW 146, 1 chlorine	17.21	1	60	A19	3.1
770	benzaldahyde	17.63	1,2	<b>9</b> 0	A20	1.2
795	unknown	19.36	-	-	A21	4.2
889	1-hexanone,5 methyl,1-phenyl	22.48	1,2	70	A22	3.1
<b>9</b> 09	unknown halogenated aliphatic acid	22.64	-	-	A23	<.5
959	unknown	23.43	-	-	A24	<.5
<b>9</b> 96	unknown halogenated aliphatic. Formed mostly at high pH and low chlorine dose	25.54	-	-	A25	<.5
1297	$C_4H_4Cl_4O$ (may be fragment of larger molecule) molecule	36.23	1	60	D1	ND
1307	$C_4H_2Cl_4O$ (may be fragment of larger molecule)	36.25	1	60	D2	ND
1317	$C_4Cl_4O$ (may be fragment of larger molecule)	36.55	1	80	D3	8.9
1336	2,4, dichloro- 6-methyl phenol	37.43	1,2	90	D4	<.5
1368	$C_8Cl_2OH_{14}$	38.60	1	30	D5	1.9
1378	$C_8H_9Cl_2NO_2$	38.87	1	30	D6	7.6
1399	$C_{10}Cl_2H_{12}NO_2$	39.55	1	30	D7	1.0
1427	2,4,6 trichlo- phenol	40.61	1,2,3	>95	D8	2.8
1459	dichloro-propyl	41.61	1	70	D9	0.6

	phenol						
1492	trichloro be acid	nzoic	42.89	1	60	D10	33.2
1528	MW 232, 3	chlorines	44.12	1	60	D11	0.8
1560	MW 230, 3 chlorines		45.15	1	60	D12	5.1
1589	trichloro-ph ethoxy	enol	46.03	1	80	D13	5.8
-	unknown		47.59	-	-	D14	<.5
Key:							
RT = retenti ND = not de ref = referen in upc Scan No. = MS sc 1 = manua 2 = compu 3 = GC ref % confidence in ID = person concentration = based for FII average at the concer-		ention time in a determined erence number pcoming chap scan number nual interpreta nputer matched retention time sonal judgeme ed on 10,000 a FID area. Con rage for all sam he San Diego p incentration val arded as ±100	for compoun- oters (Figure 21) tion of MS so d interpretation e match with nt area counts/ng ncentration is mples collect plant. uses should bo %.	ure 20) nd for discuss can on of MS sca known stand g s the ted e	sion n ard		

This table only lists compounds produced during disinfection. Background compounds are identified in Table 12.



.

Fig. 18: GC of the San Diego Wastewater Treatment Plant chlorinated final effluent. GC conditions as specified in analytical procedures. Axes are labeled for the ECD. Compound ID in Table 14.



Fig. 18 (Continued)



Fig. 19: GC of chlorinated XAD8 aquaculture extract. Chlorination conditions: 1 mg TOC, 10 mg chlorine, pH 7, contact time 2 hours. GC conditions as previously specified. Axes are labeled for the ECD. Compound ID in Table 14.



Fig. 19 (Continued)



Fig. 20: GC of chlorinated XAD8 aquaculture extract. Chlorination conditions: 30 mg TOC, 30 mg chlorine, pH 7, contact time 2 hours. GC conditions as previously specified. Axes are labeled for the ECD. Compound ID in Table 14.



Fig. 20 (Continued)



Fig. 21 Reconstructed GC/MS of Chlorinated XAD8 Aquaculture Extract

#### **3. PRECURSORS TO THE OBSERVED NVCO**

Several experiments were performed in order to ascertain the nature of the precursors to the observed NVCO. It was assumed that the precursors to the NVCO are present in the aquaculture effluent. This assumption greatly simplified the laboratory work. Working with the aquaculture effluent meant that the precursors would be found in higher concentration than in the prechlorination carbon adsorption effluent. This would consequently reduce the required volume of water from which to collect the precursors.

The identification procedure involved laboratory chlorination of various fractions of organic compounds from the aquaculture effluent and comparison of the resultant chromatographs with the chromatographs of the San Diego chlorinated plant effluent. Production of the halogenated organics found in the plant's final effluent, upon laboratory chlorination of a certain fraction, implies that the precursors are present in that particular fraction.

Several different fractionation schemes were used in order to separate the organics in the aquaculture effluent. The various fractions were subsequently chlorinated in the laboratory and the GC outputs were compared to Figure 18. (chlorinated San Diego effluent). Fractions from other treatment plants were also chlorinated in the laboratory to test whether these precursors are unique to aquaculture secondary treatment. The final experiment involved the laboratory chlorination of pure compounds which could likely be present in the aquaculture effluent. The GC outputs from this pure compound chlorination experiment were also compared to Figure 18. The nine performed experiments are listed in Table 15 and will each be discussed separately in this chapter.

### Table 15

# Experiments to Fractionate the Precursors

Experiment	Description
3.1	Chlorination of XAD8 extract
3.2	Chlorination of $CH_2Cl_2$ total and silica gel fractions
3.3	Solvent extraction vs. XAD8 adsorption for precursors collection
3.4	Chlorination of organic solvent fractions eluted from XAD8 columns
3.5	Chlorination of humic/fulvic fractions
3.6	Chlorination of 2 pH eluates from XAD8 columns
3.7	Chlorination of ultrafilter separated fractions
3.8	Chlorination of fractions from other treatment plants.
3.9	Chlorination of pure compounds

The experiments described in Table 15 have collectively provided a good description of the precursors by solubility, molecular weight, and polarity. The results from the chlorination of pure compounds reinforces these descriptions, as well as suggests the exact nature of the precursors.

## 3.1 Chlorination of XAD8 Extracts from the Aquaculture Effluent

It was initially conjectured that humic and fulvic acids are the major precursors to the observed halogenated organics. Thurman and Malcolm (1981) had shown that XAD8 resins are effective in the concentration of these natural acids. Several other workers had shown that chlorinated XAD8 extracts yield an abundance of halogenated compounds (Miller 1983, Quimby 1980). XAD8 resin was consequently chosen to concentrate these precursor compounds from the aquaculture effluent. It should be carefully noted however, that XAD8 resin is fully capable of adsorbing a host of compounds in the water and that humic and fulvic acids are a only small fraction of the different adsorbed organics (Junk 1974, Shinohara 1981).

The carbon adsorption effluent prior to chlorination at the San Diego treatment plant typically has a TOC of 0.5 to 1.0 mg/L. It was consequently decided that the laboratory chlorination be performed with 1.0 mg TOC of XAD8 extract. Figures 18, 19 and 20 have already shown that chlorination of the XAD8 extracts reproduces most of the halogenated compounds seen at the San Diego plant. Figure 22 shows that the produced quantities (total ECD peak areas) in the plant's chlorinated effluent and the laboratory chlorinated extracts are also very similar. This demonstrates that the choice of 1.0 mg XAD8 extract and 2.5 mg chlorine is a good simulation of actual plant conditions.

The results of this experiment indicate that the precursors are collectible by XAD8 adsorption. This implies that the precursors are acidic compounds (adsorbable in acid solution, but desorbable with alkaline solution) found in the aquaculture effluent.



Fig. 22: Comparison of the total chlorination by-product ECD areas of chlorinated XAD8 aquaculture extract and the San Diego Wastewater Treatment Plant final effluent. Before = before chlorination, After = after chlorination.

# 3.2 Laboratory Chlorination of CH<sub>2</sub>Cl<sub>2</sub> Extracts

Total methylene chloride extractable organics from the aquaculture effluent, as well as the silica gel fractionated extract (see analytical procedures for details) were redissolved in distilled Arrowhead brand water and chlorinated as concentrated fifteen milliliter solutions. 1.5 mg (by weight) of aquaculture extract was used and a chlorine dose of 2.5 mg was applied at pH 7 and a two hour contact period. Figure 23 is a schematic of the experimental procedure.

The resultant chromatographs were compared to Figure 18 (chlorinated San Diego effluent). The chlorinated total extract, as well as the chlorinated third fraction (methanol:methylene chloride elutable) gave very similar chlorination patterns to Figure 18. Fraction 1 (hexane eluate) and fraction 2 (benzene eluate) were basically not affected by the addition of chlorine.

Figure 24 shows that 66% of the increased ECD total area brought about from chlorination of the total extract was due to the compounds present in the third fraction. 30% of the increased ECD area in the total extract could not be accounted for in the three collected fractions. It was consequently assumed that compounds which were non-elutable (labeled NEP in Figure 24) from the silica gel column were responsible for the difference.

The results from this experiment point out that the precursors are polar (third fraction and NEP fraction) compounds. This conclusion concurs with the results of Section 3.1. Much more significant, however, is the observation that the precursors are solvent extractable. This implies that they are only moderately polar, since if they were very polar, they would not be solvent



Fig. 23 Fractionation Scheme of the Chlorinated Methylene Chloride Extracts



Fig. 24: Total ECD areas of the chlorinated silica gel fractions as a percent of the total extract ECD area. Fraction 1 = hexane eluate, fraction 2 = benzene eluate, fraction  $3 = CH_2CL_2$ : MeOH eluate, NEP = non-elutable polars.

extractable. Although this observation is highly qualitative it is also highly significant. Humic and fulvic acids are generally not considered to be solvent extractable. Indirectly, therefore, this experiment implies that the precursors do not fit the classic definitions of humic and fulvic acids.

# 3.3 Solvent Extraction vs. XAD8 Adsorption for Precursors Collection

The experiments discussed in Sections 3.1 and 3.2 indicate that the precursors to the observed NVCO can be collected by either XAD8 resin adsorption or by methylene chloride extraction. A simple experiment was designed in order to verify which method is more efficient for the collection of the alleged precursors.

Two one liter samples of reverse osmosis effluent were chlorinated in the laboratory with 10 mg/L NaOCl at pH 7 for two hours. Another duplicate set of RO effluent samples were chlorinated under the same conditions except that the samples were passed over XAD8 (at pH 2) resin before chlorination. A third set of samples was extracted with  $CH_2Cl_2$  and the methylene chloride was discarded before chlorination. The resultant total ECD areas from each set of samples were then compared.

The XAD8 treated samples showed an average 70% drop in total ECD area, whereas the methylene chloride extracted samples only showed an average 33% drop in total ECD area. This points out that the XAD8 resin is more effective in removing the precursors to the observed gas chromatographable NVCO. This is quite fortunate since XAD8 adsorption is simpler and cheaper to perform than solvent extraction (once the resin has been cleaned). It was consequently decided that XAD8 resin be used for all future precursors collection protocols.

# 3.4 Chlorination of Organic Solvent Eluted Fractions from XAD8 Columns

In an effort to better understand the solubility properties of the precursors the following experiment was performed. Sixteen liters of aquaculture effluent were adsorbed to a cleaned XAD8 column at pH 2. The adsorbed organics were then eluted with a series of increasingly polar solvents. The first fraction was collected with 35 ml of diethyl ether. The second fraction was collected with 35 ml of methylene chloride and a third fraction was collected in the same volume of methanol. The fourth fraction was eluted with an identical volume of .1 N NaOH.

Each fraction was analyzed by GC before and after chlorination with 10 mg/L NaOCl at pH 7 for two hours. As would be expected many of the solvent extractable compounds present in the aquaculture effluent were collected by XAD8 adsorption and appeared in both the ether and methylene chloride fractions. The ether and methylene chloride fractions consequently contained background organics which gave a sizeable ECD response. These compounds are not usually collected in the routinely used XAD8 adsorption procedure because the XAD8 adsorbed organics are normally only collected with .1 N NaOH and these gas chromatographable compounds are not elutable with this alkaline solution.

No effort was made to translate the ECD total areas into concentrations, since the desired results are discernible by comparison of the raw total area values. Table 16 shows the total ECD area before and after chlorination (the ether, methylene chloride and methanol were evaporated and the residues were redissolved in distilled water before chlorination).

Fraction Number	Solvent	Total ECD Area before Chlorine Addition	Total ECD Area after Chlorine Addition	Net Increase in total ECD area due to Chlorine
1	Ether	3.38x10 <sup>7</sup>	3.22x10 <sup>8</sup>	285x10 <sup>6</sup>
2	CH <sub>2</sub> Cl <sub>2</sub>	5.73x10 <sup>7</sup>	1.53x10 <sup>8</sup>	147x10 <sup>6</sup>
3	Methanol	2.54x10 <sup>6</sup>	7.61x10 <sup>7</sup>	73x10 <sup>6</sup>
4	.1 N NaOH	5.83x10 <sup>5</sup>	2.32x10 <sup>6</sup>	$2 \times 10^{6}$

#### Table 16 Organic Solvent Fractionated XAD8 Extract

The precursors to the observed gas chromatographable NVCO are apparently easily elutable with organic solvents (ether, methylene chloride and methanol). This experiment again suggests that these precursors do not fit the classic definitions of humic and fulvic acids since humic compounds are not ether or methylene chloride soluble (fulvic acids are elutable with methanol to a certain extent). Although this experiment points out that the precursors are ether elutable, it is a cleaner separation to collect them with .1N NaOH (the usual XAD8 desorption protocol) since the background chromatographable compounds are not collected with the sodium hydroxide solution.

#### 3.5 Chlorination of Humic/Fulvic Fractions

The procedure used in this work to collect XAD8 adsorbable organics with .1N NaOH is an abbreviated version of a procedure developed by Thurman and Malcolm (1981) to extract humic and fulvic acids. Thurman and Malcolm further separate the extract into a humic and a fulvic fraction by centrifugation at pH 1. The soluble fraction is fulvic acid and the residue is labeled the humic fraction.

This additional separation step (humic/fulvic split) was performed in order to be able to compare results from this work with the findings of others. The humic and fulvic fractions were analyzed by gas chromatography before and after chlorination with 10 mg NaOCl at pH 7 for two hours. The total ECD response was compared with the unfractionated sample (no humic/fulvic split).

Figure 25 illustrates that the fraction labeled fulvic acids is fifteen times more productive than the humic fraction. The fulvic fraction produces 98% of the total ECD area produced by the unfractionated sample (identical GC pattern) whereas the humic fraction only accounts for 6% of the total area of the unfractionated sample. The additional 4% in total area can be attributed to experimental error.

The results of this experiment conclusively demonstrate that humic acid is not the major precursor to the observed NVCO. The precursors are present in the fraction which Malcolm and Thurman, as well as numerous other workers have labeled fulvic acids. It should be stressed that hundreds of compounds can be collected in this fraction. Operationally, this fraction contains acidic compounds which are base soluble. Many workers have chosen to label these compounds fulvic acids for a lack of a better name. It is felt that this label is too broad especially since the precursors of interest have been shown to be organic solvent soluble (Sections 3.2, 3.3, and 3.4) and classically, fulvic acids are only water (low and high pH) soluble.

#### **3.6 Chlorination of Two pH Eluates from XAD8 Columns**

In a 1979 publication, McCarthy et al. demonstrated that two distinct fractions may be eluted from XAD resins if one varies the pH of the eluant. A similar experiment was attempted in an effort to asses the acidity of the precursors.

Aquaculture effluent was adsorbed onto an XAD8 column at pH 2. The first fraction was eluted at pH 6 and a second fraction was collected at pH 13. Each fraction was subsequently chlorinated at pH 7 with 10 mg chlorine for two hours.

Within experimental error, there appeared to be no quantitative or qualitative differences between the two fractions. It appears that the precursors are partially eluted at pH 6 and that their increased solubility at pH 13 allows for more complete desorption. No definitive conclusions may be reached from this experiment.

#### 3.7 Chlorination of Ultrafiltration Fractions

The XAD8 adsorbed organics from the aquaculture effluent were (40 ml from 2000 ml of concentrated extract collected from 360 liters; TOC of 1 mg/10 ml of concentrated extract) separated into five molecular weight ranges by ultrafiltration (see analytical procedures section for more details). Ten milliliters (one mg TOC) of the greater than 100,000 MW, the 100,000 to 30,000 MW, the 30,000 to 10,000 MW and the 10,000 to 1,000 MW fractions were



Fig. 25: Total ECD areas of chlorinated humic/fulvic fractions as a percent of the total extract ECD area.

consequently chlorinated with a dose of 10 mg chlorine at pH 7 for two hours before extraction. 30 ml of the less than 1,000 MW fraction was chlorinated under the same conditions. Thirty milliliters was used because the solution was diluted threefold by the filter washings. GC analysis was performed before and after chlorination for each fraction. All samples were run in duplicate.

Table 17 summarizes the experimental results. Figure 26 is a bar graph showing the total ECD area attributable to chlorination from each fraction. The unchlorinated fractions gave virtually no ECD peaks. It is quite clear that the NVCO precursors are predominantly present in the less than 1,000 MW fraction. No effort was made to translate total ECD areas into concentration because only a relative comparison between the fractions is desired. The sum of the total ECD areas for the five fractions is slightly greater than the area of the unfractionated extract (103%), but lies within experimental error.

#### 3.8 Chlorination of XAD8 Extracts from Other Treatment Plants

XAD8 extracts were collected from two other wastewater treatment plants and chlorinated in the laboratory. This experiment was done in order to investigate whether the observed halogenated organics in the San Diego plant are unique to water hyacinth based secondary treatment.

One of the two chosen plants used activated sludge secondary treatment (Whittier Narrows Wastewater Treatment Plant in Whittier, California), while the other plant, located in Florida, used water hyacinth fields for secondary treatment.

	Total ECD Area No. 1	Total ECD Area No. 2	Average Total ECD Area
Fraction	(x 10 <sup>-7</sup> )	(x 10 <sup>-7</sup> )	x 10 <sup>-7</sup> )
> 100K	0.28	0.22	0.25
100-30 K	0.26	0.14	0.20
30-10 K	0.18	0.21	0.20
10-1 K	0.18	0.16	0.17
< 1 K	3.71	4.59	4.15
Total Extract	4.53	5.19	4.86

## Table 17 Untrafilter Fractionated XAD8 Extract

## Key:

>	=	greater than
<	I	less than
Κ	=	thousand daltons



Fig. 26: Total ECD areas of chlorinated UF fractions from the San Diego Wastewater Treatment Plant XAD8 extract. It = Iess than, gt = greater than, K = 1000 daltons.

Twenty liters of secondary effluent from each plant was adsorbed onto XAD8 columns at pH 2. The .1 N NaOH eluted extract was next fractionated into 5 molecular weight fractions as previously described. The TOC analyzer was not operational during the time that the experiments were performed. The laboratory chlorinations were consequently done using an unknown quantity of extract. An equivalent amount of extract (based on volume adsorbed and volume of eluate) as that used for the San Diego samples was used in the chlorination experiments to minimize the variability. Since no direct comparisons are made between the NVCO formation potential (NVCOFP) of the extracts from the various plants, the quantity of extract used for each plant is irrelevant. The comparisons made between the various plants are qualitative and merely compare the gas chromatographs. Comparisons of the NVCOFP of each molecular weight fraction for a given plant are also valid since the chlorination conditions are constant for a given treatment plant.

Figure 27 is the GC output for the chlorinated Whittier Narrows XAD8 extract. Figure 28 is the similar output from the water hyacinth treatment plant. A comparison of Figure 19 (chlorinated San Diego plant XAD8 extract) to the Whittier Narrows and the Florida water hyacinth treatment plant extracts immediately shows that the halogenated organics observed in San Diego are also common to the latter two wastewater treatment plants. The axes in Figures 27 and 28 are labeled for the ECD. The FID is slightly offset to the left.

Figures 29 and 30 contrast the total ECD areas attributable to chlorination for the five molecular weight fractions from each treatment plant. Once again the less than 1,000 molecular weight fraction accounts for nearly 85% of the NVCOFP of the total unfractionated extract. The sum of the total areas for the five fractions is not 100% of the ECD area for the unfractionated extract, but lies within reasonable experimental error.

In summary, the two wastewater treatment plants show very similar NVCO profiles upon laboratory chlorination to the San Diego plant. This points out that the NVCO precursors are not unique to the San Diego plant nor to water hyacinth based secondary treatment.

#### **3.9** Chlorination of Pure Compounds

Twenty four pure compounds which are likely to be present in the aquaculture effluent were purchased from various chemical distributors and chlorinated in the laboratory. The compounds were chosen so as to represent an assortment of natural organic compounds. Carbohydrates, lipids, amino acids, metabolic acids, as well as plant pigments were chosen. The resultant gas chromatographs after chlorination were compared to the San Diego chlorinated effluent, as well as the chlorinated aquaculture XAD8 extract. Since only retention time matches (not MS comparisons) were used for comparison, the identifications must be regarded as possible but not positive. The chosen list of compounds is by no means exhaustive and is only meant to give ideas about the NVCO formation potential of the chosen classes of compounds.

Although only one mg TOC had been used in the chlorination of the XAD8 extract, it was decided to use larger amounts (usually 5 mg TOC) of the pure compounds in order to increase the detection limits. All chlorinations were done at pH 7 for two hours using approximately 2:1 chlorine:TOC ratios.



Fig. 27: GC of chlorinated XAD8 extract from Whittier Narrows Wastewater Treatment Plant. GC conditions as previously specified. Axes are labeled for the ECD.



Fig. 27 (Continued)



Fig. 28: GC of chlorinated XAD8 extract from the Water Hyacinth Wastewater Treatment Plant. GC conditions as previously specified. Axes are labeled for the ECD. Compound ID in Table 14.



Fig. 28 (Continued)



Fig. 29: Total ECD areas of chlorinated UF fractions from the Whittier Narrows Wastewater Treatment Plant. LT = less than, GT = greater than, K = 1000 daltons.



Fig. 30: Total ECD areas of chlorinated UF fractions from the Water Hyacinth Wastewater Treatment Plant. Ranges for 1000 daltons.

All TOC values were calculated theoretically using gravimetric data. In some cases, five mg TOC was not available so a lesser amount was used. Several chlorine doses were used if the chlorination with the 2:1 Cl:TOC ratio was highly productive.

Table 18 lists the compounds which were chlorinated, the class and amount of the compound which was chlorinated, as well as the applied chlorine dose. The reference numbers (see Table 14 for reference numbers) for the NVCO which were produced during chlorination are also included.

Examination of Table 18 points out that carbohydrates, lipids and fatty acids are not likely to be precursors to the observed NVCO. Amino acids, as well as the fatty acids, produce a few halogenated organics upon chlorination, but do not produce the wide spectrum of compounds seen upon chlorinating the XAD8 aquaculture extract. Humic acid purchased form Aldrich Chemical Company was also chlorinated in the laboratory (data not presented in Table 18). The chlorination of 5 mg of humic acid with 10 mg of free chlorine was productive of compounds A1 and D1. The 5 mg (in 15 ml of water) solution, however, was black in color and showed no color resemblance to the aquaculture XAD8 extract (pale yellow color). A 40 mg (by weight) solution of humic acid, chlorinated with 80 mg of chlorine produces several other compounds but again is black in color. In brief, it requires 40 milligrams of this humic acid to form a total ECD response produced by the chlorination of one mg of aquaculture XAD8 extract.

Figure 31 is the GC of chlorinated Morin, a plant flavonol. Flavones and flavonols are the most widely distributed of all the yellow plant pigments, although the deeper yellow colors of plants are normally due to carotenoids. Figure 31 shows resemblance to the chromatographs of the chlorinated aquaculture XAD8 extracts (Figure 19). The axis labeled in Figure 31 is for the ECD. The FID is slightly offset to the left.

Flavones and flavonols were chosen as model compounds for chlorination for a variety of reasons. Their molecular weight is less than 1000 (typically 220-400). They are soluble in water and organic solvents depending on the extent of hydroxylation. Flavones and flavonols are moderately polar, as well as acidic. These compounds are also widely distributed in the plant kingdom. Lastly, their pale yellow color matches the color of the XAD8 aquaculture extract. In summary, this list of properties closely matches the properties of the precursors in the San Diego XAD8 extract discussed in Sections 3.1-3.8.

The similarity of the chlorination products of the flavones and the aquaculture XAD8 extract, as well as the matching of their respective solubility, MW, color and acidity properties is an appealing match, but admittedly may only be coincidental. Furthermore, it is highly unlikely that these flavone compounds remain unchanged after secondary treatment. It is more plausible that a modified plant pigment may be the reactant with aqueous chlorine.

The data presented thus far in conjunction with the knowledge that reverse osmosis treatment is much more effective in the treatment of large molecules (humic and fulvic acids) strongly suggests that the precursors bear some structural similarity to these plant pigments. Reinhard (1984) had also stated that in tertiary treated waters, the small MW fractions (less than 1000)
are the most important reactants with aqueous chlorine.

Figure 32 shows the molecular structure of flavone and kaempferol. Chlorination of the center puran ring could potentially lead to the formation of compounds D1, D2, D3, and D4. The unsaturated 'A' reference number compounds could result from breakage of either of the unsaturated rings. The chlorophenols could be formed by chlorine addition to either aromatic ring.

In conclusion, the precursors to the observed NVCO are not unequivocally defined. The presented data however, should point out that small, partially organic solvent soluble, non-humic molecules are important chlorination precursors. Plant pigments provide excellent laboratory model chlorination compounds and may quite possibly be the major NVCO precursors.

Compound Name	mg used (TOC)	mg Chlorine Added	Reference No. of NVCO Produced in Trace <sup>3</sup> Amounts	Reference No of NVCO Produced in Large Amounts	Other Halogenated Compounds Produced <sup>1,2</sup>	
		Ca	rbohydrates			
Cellulose	10.2	20.4	NP	NP	Low	
Corn Starch	9.9	19.8	NP	NP	NP	
Fructose	5.9	11.8	NP	NP	NP	
Levan	4.5	9.0	NP	NP	NP	
Pectin	5.8	11.6	NP	NP	NP	
	Amin	o Carbohydrates	s (found in bacteri	al cell walls)		
N-acetyl- muramic acid	2.5	5.0	NP	NP	NP	
N-acetyl- neuramic acid	5.0	10.0	NP	NP	NP	
		Aromat	ic Carbohydrate			
Tannic Acid	6.0	12.0	NP	A10	Low	
		Amino A	cids and Proteins			
Pepsin	5.0	10.0	NP	A14	Low	
Proline	5.0	10.0	NP	A12	Low	
Tryptophan	4.3	8.6	D7	A14	Low	
		Lipids	and Cholesterol			
Cholesterol	6.3	12.6	NP	NP	Low	
Psychosine	2.5	5.0	NP	NP	Low	
Sphingosine	2.5	5.0	NP	A2	Low	

## Table 18 Chlorinated Pure Compounds

## Table 18 Chlorinated Pure Compounds (Continued)

Chisadalactic Hydrotarbon						
Squalene	5.0	10.0	A1,A2	A16	Low	
		F	atty Acids			
Lactic	5.0	10.0	NP	NP	High	
Pyruvic	5.0	10.0	NP	NP	High	
Malic	5.4	10.8	NP	NP	High	
Oleic	5.0	10.0	NP	NP	High	
		Flavone T	ype Plant Pigment	ts		
Catechin	8.8	20.0	A1,A2,A4,A8,A	.9,A10,A11	High	
Flavone	6.5	13.0	A1,A2,A4,A16,A17,A23,A24, D3,D8,D10		High	
Kaempherol	2.5	5.0,10.0,20.0 40.0	A1,A2,A4,A6,A8,A10,A14 A16,A17,A18,A23,A24,D8		High	

5.0,10.0,20.0 A1,A2,A4,A6,A8,A9,A10,A14

A16,A17,A18,A23,A24,D3,D8

High

#### Unsaturated Hydrocarbon

## Key:

Morin

2.5

40.0

1	=	Low indicates that the ECD area of the compounds is less than three times the background ECD noise blank level
2	=	High indicates compounds are greater than three times background levels
3	=	Trace amounts indicate that ECD area for that compound is less than 5% of the ECD response produced by the chlorination of 1 mg XAD8 resin extract
NP	×	not productive



Fig. 31: GC of the breakdown products of chlorinated morin. GC conditions as previously specified. Axes labeled for the ECD. Compound ID in Table 14.



.

Fig. 31 (Continued)



FLAVONE



KAEMPHEROL

Fig. 32 Molecular Structure of Flavone and Kaempherol

## **4. EFFECT OF CHLORINATION PARAMETERS ON THE**

#### **PRODUCTION OF NVCO**

Several chlorination parameters were varied in order to assess their effects on the formation of the observed gas chromatographable NVCO. The effects of pH, chlorine dose, contact time and bromide ion concentration were investigated. pH 7, a chlorine dose of 2.5 mg, a two hour contact period, 1.0 mg TOC and 0.0 mg of bromide ion were chosen as the base conditions. One parameter was varied while the others were maintained constant.

This experiment was performed on three different occasions. The carbon adsorption effluent, as well as XAD8 extract from the aquaculture effluent were chlorinated in 8/85. The XAD8 extract was again chlorinated under these varying conditions in 5/86. All three experiments showed the exact same trends. Unfortunately, the chromatographs from 8/85 contain four large contaminant peaks which, although can easily be subtracted, make the chromatographs more difficult to visualize. The quantitative results after subtraction of the contaminant peaks are very similar to the 5/86 experiment. The GC integrator reports from some of these experiments are included in Appendix 3. Only the data from the 5/86 experiment will be presented in this section however.

#### 4.1 Effect of Chlorine Dose

The chlorine dose added to the XAD8 extract has a noticeable effect on the relative quantities of produced halogenated organics, as well as the total produced gas chromatographable NVCO. Figure 33 shows the GC profiles for three of the applied chlorine doses (pH 7, 2 hour contact time, 0 mg bromide ion). High chlorine doses bring about the breakdown of larger halogenated molecules and one observes a shift in the chromatogram to lighter compounds (smaller retention times).

The GC's shown in Figure 33, as well as others to be shown in Figures 35, 37, 39, 42, 43, and 46 only show the initial portions of the output. This was done in order to present more than one chromatograph on the same page. The latter part of the chromatographs (not shown) only contain a few compounds.

In addition, only a few of the peaks are labeled in these small chromatographs due to size limitations. The figures may be compared to the larger GC's (Figures 18, 19, and 20) as well as Table 14 for complete peak referencing.

The first moment of the chromatogram was evaluated according to Equation 9.

First moment = 
$$\sum (RT)_i x (ECD \ area)_i / (total \ ECD \ area)$$
 (9)

where

 $(RT)_i$  = retention time of compound i  $(ECD \ area)_i$  = ECD area of compound i

The first moment is the centroid of the chromatograph. A low centroid indicates a predominance of smaller compounds, whereas a large first moment

reflects the presence of larger compounds. The first moment of the chromatogram, as well as the total ECD area are plotted in Figure 34. Higher chlorine doses lead to lower chromatograph centroids, but surprisingly do not lead to higher total NVCO areas. The highest production was observed with the addition of only one milligram of chlorine. The formation of each individual peak (compound) at the varying chlorine doses may be monitored from the data provided in Appendix 3. Dilutions for the GC outputs are the same and the areas are directly comparable. The retention times from one run to the next usually match within a 0.04 minute window.

As has been previously mentioned in the literature review section, many workers have noted that THM formation increases with increasing chlorine doses. It has consequently been routinely recommended that chlorine doses be kept low in order to minimize THM formation. Higher amounts of THM's were undoubtedly formed by the higher chlorine doses used in this experiment and yet an unknown amount of non-gas chromatographable TOX was formed. Since neither THM's nor total TOX were monitored in this work, it is not possible to state which chlorine dose leads to the formation of the least halogenated organics.

This experiment demonstrates that an abundance of halogenated organics are formed during chlorination, whose relative amounts can be controlled by the applied chlorine dose. This observation immediately suggests that a chlorine dose should be applied which would lead to the formation of minimum toxic products (possibly a choice between toxic and very toxic). Since the relative size and volatility of the chlorination products can also be controlled by the applied chlorine dose, other decision variables must be addressed. The ultimate decision about chlorine doses may favor the production of components which may be removed from the water with an additional treatment step. If treatment by activated carbon is possible, it may be wiser to use low chlorine doses since heavier components are more easily removed by carbon adsorption. On the other hand, if aeration is to be used as a final polishing step, high chlorine doses could be used to maximize the production of lighter compounds which would be amenable to air stripping.

The above mentioned ideas highlight the need for an investigation which would simultaneously address the questions of toxicity of the various fractions and the dependence of toxicity on chlorination parameters. The work of Coleman (1984) was a step in this direction. Such an investigation would be lengthy, tedious and expensive, but would certainly be worthwhile.

In summary, advocating the use of low chlorine dosages in order to minimize THM formation is an incomplete recommendation. Chlorine dose appears to be a parameter which can be utilized to minimize harmful chlorination by-products and can be tailored to subsequent treatment steps.

## 4.2 Effect of Contact Time

Contact time, like chlorine dose, affects the relative amounts of the produced NVCO. Figure 35 shows the GC outputs of three of the tested contact times (pH 7, 2.5 mg chlorine, 0.0 mg bromide). Figure 36 is a plot of the total ECD areas and the first moments of the chromatographs vs. contact time.

Increased contact time leads to the formation of smaller components (lower first moment) and a slight reduction in the total ECD area. Increased



Fig. 33: GC's (ECD) of chlorinated aquaculture XAD8 extract at various chlorine doses. pH 7, contact time = 2 hours, TOC = 1 mg. GC conditions as previously described. Compare to Figure 19 and Table 14 for compound ID.



Fig. 34: Effect of chlorine dose on the breakdown products of chlorinated XAD8 extract.

contact time allows for further reaction of the free chlorine with the available TOC and the consequent breakdown of the larger molecules.

It is plausible to utilize the effects of contact time to minimize the more toxic components of TOX as well as to allow chlorination to proceed to the point which is most amenable to a further treatment step. These ideas were discussed in Section 4.1.

#### 4.3 Effect of pH

The chlorination of the XAD8 extract was performed at several pH values. pH is an extremely important parameter in determining both the total produced NVCO and the relative amounts of the various compounds. Figure 37 shows the GC's for pH 3, 7, and 11 while Figure 38 shows the quantitative analysis of the chromatograms. Low (3) and high (11) pH result in the production of the heavier components, while the near neutral pH values (5,7,9) show similar profiles. Overall, high pH is the most NVCO productive.

The production of the heavy NVCO, 'D' reference number compounds is most likely an addition step to an unsaturated bond which may proceed by either base or acid catalysis.

#### 4.4 Effect of Bromide

The aquaculture XAD8 extract was chlorinated with varying amounts of bromide ion in solution. The chlorinations were done at pH 7, using 10 mg of chlorine for two hours. The extract solution was spiked with 1, 5, 10, or 20 mg of potassium bromide before chlorination.



Fig. 35: GC's (ECD) of chlorinated aquaculture XAD8 extract at various contact times. pH 7, chlorine dose = 2.5 mg, TOC = 1 mg. GC conditions as previously specified. Compare to Figure 19 and Table 14 for compound ID.





Fig. 37: GC's (ECD) of chlorinated aquaculture XAD8 extract at various pH values. Chlorine dose = 2.5 mg, TOC = 1 mg, contact time = 2 hours. GC conditions as previously specified. Compare to Figure 19 and Table 14 for compound ID.



The bromide ion has a significant effect on the produced halogenated organics. Figure 39 compares the chromatographs of zero and ten milligram bromide ion addition. Figure 40 shows that the total ECD area nearly triples after the addition of one mg bromide, but does not increase with further addition of bromide ion. Some of the chlorinated compounds show a decrease with the addition of bromide ion, at the expense of the formation of new brominated compounds (Figure 39).

#### 4.5 Summary of the Effects of the Chlorination Variables

The gas chromatographable NVCO which were monitoried in these experiments are only a subset of the total organic halogens (TOX) produced during the disinfection of water. The concern for chlorination by-products centers around the health effects of these by-products. These experiments demonstrate that while certain compounds can be reduced by varying the chlorination conditions, the concentrations of other compounds are often increased at their expense. The choice of chlorination conditions should depend on minimizing the most harmful by-products.

Chlorination at low pH, long contact time, high chlorine dose (10 mg/L), and zero mg/L bromide concentration minimizes the formation of this subset of TOX. A recommendation of these chlorination conditions would be inappropriate until the relative toxicity of the various components of TOX is examined.



Fig. 39: GC's (ECD) of chlorinated aquaculture XAD8 extract in the presence of bromide. Top 5 mg bromide added, bottom no bromide addition. Chlorine dose = 10 mg, contact time = 2 hours, TOC = 1 mg, pH 7. GC conditions as previously described.



Fig. 40: Effect of bromide on the breakdown products of chlorinated XAD8 extract. Chlorine dose = 10 mg, contact time = 2 hours, pH 7, 1 mg TOC.

## 5. EFFECTS OF DECHLORINATING AGENTS

It has been commonplace to add a dechlorinating agent such as sodium sulfite to quench the residual chlorine before analyzing the organic compounds in a chlorinated water sample. This is usually done in order to arrest the further reaction of chlorine with the carbon sources in the water. Since dechlorinating agents are not reactive with THM's, this protocol gained wide acceptance with researchers who studied the kinetics of THM formation.

The recent interest in the analysis of other halogenated chlorination by-products proceeded by mimicking the residual chlorine quenching step from the THM analytical protocols. The question regarding the effects of dechlorinating agents on these non-volatile halogenated organics has not been addressed. It has been assumed that dechlorinating agents are not reactive with all of the chlorinated organic by-products.

It was observed that the addition of sodium sulfite or sodium thiosulfate to the chlorinated water samples (from the San Diego Wastewater Treatment Plant) before extraction had a significant effect on the quantity and makeup of the methylene chloride extract.

This observation was first made in an experiment designed to reproduce the halogenated organics observed in the San Diego Wastewater plant in the laboratory. The residual chlorine in the chlorinated San Diego effluent was not regularly quenched before extraction. The carbon adsorption effluent (from San Diego) was chlorinated in the laboratory under a variety of conditions (contact time, pH, and chlorine dose) in order to determine which set of conditions most closely reproduces the chlorination by-products seen in San Diego. The residual chlorine was quenched with sodium sulfite before extraction for the laboratory chlorinated samples. There consistently appeared to be a difference between the laboratory chlorinated samples and the San Diego chlorinated effluent. After several iterations of parameter modifications, it was finally realized that sodium sulfite addition is the reason for the difference between the chromatographed extracts.

Three experiments were designed to assess the effects of sodium sulfite on the produced halogenated organics. First, sodium sulfite was added to several categories of aqueous solutions of pure halogenated compounds. Second, sodium sulfite was added to the chlorinated San Diego final effluent. Lastly, sodium sulfite was added to laboratory chlorinated XAD8 aquaculture extracts before methylene chloride extraction. Some of the XAD8 solutions were spiked with bromide ion before chlorination. Each of these experiments will be discussed separately.

## 5.1 Addition of Sodium Sulfite to Pure Halogenated Compounds

Eight classes of halogenated organics were treated with sodium sulfite before extraction from a prepared aqueous solution. Control samples were extracted under identical conditions minus the sodium sulfite addition step (see analytical procedures section for more details). All samples were analyzed in triplicate. Table 19 lists the classes of compounds used, the compound name and the average percent decrease in the integrator area of the compound caused by the addition of sodium sulfite. The decrease in the area of the compound implies that the compound reacted with the sulfite ion and consequently the area of the original compound (reactant) decreases. The two unsaturated aliphatics (3-chloro-1-butene, and 3-bromopropene) as well as chloro-benzene were the only three compounds which were reactive with sodium sulfite. Although the tested list of compounds is not exhaustive, it is still very informative.

It was predictable that chloro-phenols, and halogenated saturated aliphatics would not be reactive with the sulfite ion since they have been successfully analyzed in the past by numerous workers. The presence of oxygen (aldehydes, phenols, and alcohols) or nitrogen atoms does not lead to reactivity with the sulfite ion. The three reactive molecules are unsaturated. Other unsaturated compounds, however, were unreactive (dichlorobenzenes) which means that the presence of a carbon double bond may be necessary, but is not sufficient to render the compounds reactive with sulfite.

It is hypothesized that the sulfite ion displaces the halogen atom, forming a sulfonic acid (or possibly a di-sulfonic acid). Sulfonic acids are not methylene chloride extractable (too polar) and consequently do not appear in the gas chromatograms after sulfite addition. It is postulated that the reaction is a substitution and not an addition reaction because, brominated compounds are more reactive with sulfite than chlorinated compounds. This is seen with 3-bromopropene and with the brominated compounds produced by the reaction with the XAD8 extracts (Section 5.3). Bromide is a better leaving group than chlorine and is consequently more likely to undergo substitution reactions (Gutsche and Pasto 1975). A leaving group is the moeity in a molecule which is displaced during a reaction. The alkyl bromide ion is a fifty times better leaving group than the alkyl chloride ion. Figure 41 is a schematic of the postulated reaction between 3-bromopropene and sodium sulfite. The fast reaction of the the sulfite ion with unsaturated carbonyl compounds has been reported as early as 1966 (Schroeter 1966). These reactions were reported for applications in the food processing and pharmaceutical industries. The reactions reported in this work are very similar to Schroeter's reports.

#### 5.2 Addition of Sodium Sulfite to the Chlorinated Effluent

Two liters of chlorinated final effluent were extracted without addition of sodium sulfite (Figure 18). Excess (five fold) sodium sulfite was added to a duplicate sample before extraction. The gas chromatograms of the two extracts are shown in Figure 43. The ECD area for peaks eluting before twenty minutes (most of the 'A' reference number peaks) drops by 75% after sulfite addition (from  $1.9 \times 10^7$  to  $4.8 \times 10^6$ ) whereas the area drop for peaks eluting after twenty minutes is only 37% (from  $1.1 \times 10^8$  to  $6.9 \times 10^7$ ). The early eluting peaks which are most affected by sodium sulfite are mostly unsaturated halogenated compounds.

The chromatographs shown in Figures 42 and 43 were chosen so as to illustrate the fact that the early eluting peaks ('A') are the ones most affected by sodium sulfite. On several occasions, probably due to differing chlorination conditions at the treatment plant, most of the compounds in the chlorinated effluent extract were 'A' peaks. Under these latter conditions, sodium sulfite has a more pronounced effect on the total gas chromatographable NVCO. This observation may be of practical utility. If the sulfonated compounds are less of a health hazard than their halogenated counterparts, it may be advantageous to chlorinate under conditions which produce compounds

Compound Name	Compound Class	% Drop Caused by Sulfite		
o-chlorophenol	phenol	0		
2,4,5-trichloro-phenol	phenol	0		
2,4,6-trichloro-phenol	phenol	0		
chloro-cyclohexane	cyclic aliphatic	0		
bromo-cyclohexane	cyclic aliphatic	. 0		
trichloroethane	straight aliphatic	0		
chloroform	straight aliphatic	0		
chloro-ethanol	alcohol	0		
chloro-pyridine	nitrogen containing	0		
bromo-analine	nitrogen containing	0		
2,4-dichlorobenzaldehyde	aldehyde	0		
2,4-dichlorobenzene	aromatic	0		
1,3-dichlorobenzene	aromatic	0		
1,4-bromochlorobenzene	aromatic	0		
chloro-benzene	aromatic	31		
3-chloro-1-butene	unsaturted aliphatic	26		
3-bromo-propene	unsaturated aliphatic	95		

# Table 19 Addition of Sodium Sulfite to Pure Compounds



Fig. 41 Reaction of Sodium Sulfite with 3-Bromopropene

that are reactive with the sulfite ion.

#### 5.3 Addition of Sodium Sulfite to Chlorinated XAD8 Extract

Aquaculture effluent XAD8 extracts were chlorinated and sodium sulfite was added (five fold excess) before methylene chloride extraction. Once again, one observes a large drop in the total ECD area (68%, 10 mg chlorine at pH 7, 4 hours) and an even greater drop for the early eluting peaks (77% for peaks eluting before 20 minutes, 'A' peaks). Table 20 summarizes some of the data.

An XAD8 extract sample spiked with five milligrams of bromide ion was treated with sodium sulfite before extraction. Although the percentage decrease is less than that observed without addition of bromide, the magnitude of the drop was more than twice that without bromide addition (Table 20). This may indicate that brominated compounds are more reactive with the sulfite ion. As was indicated in Section 5.1, the bromide ion is a better leaving group than the chloride ion and may be more likely to undergo this substitution reaction.

#### 5.4 Summary of the Effects of Sodium Sulfite

Sodium sulfite is reactive with many of the observed halogenated organics seen in the San Diego chlorinated final effluent. Sodium sulfite should only be added in the laboratory before extraction if the compounds of interest are not reactive with the dechlorinating agent (THM's). This observation is critical for proper and accurate quantitation of the chlorination byproducts. In addition, this observation may have practical significance if the



Fig. 42: GC's showing the effect of sodium sulfite on the chlorinated San Diego Wastewater Treatment Plant effluent. Top: excess sulfite added; bottom: no sulfite addition. Compare to Figure 19 and Table 14 for compound ID. GC conditions as previously specified. Axes labeled for ECD.

sulfonated compounds are found to be less hazardous than their halogenated counterparts.



Fig. 43: GC's showing the effect of sodium sulfite on the chlorinated aquaculture XAD8 extract. Top: excess sulfite added; bottom: no sulfite addition. Compare to Figure 19 and Table 14 for compound ID. GC conditions as previously specified. Axes labeled for ECD.

Conditions	Total ECD Area		Area Before 20 minutes		Area After 20 minutes	
(all for 4 h Cl and 10 mg C <sub>12</sub> )	minus sulfite	plus sulfite	minus sulfite	plus sulfite	minus sulfite	plus sulfite
	x 10 <sup>7</sup>	<b>x</b> 10 <sup>7</sup>	x 10 <sup>7</sup>	x 10 <sup>7</sup>	x 10 <sup>7</sup>	x 10 <sup>7</sup>
рН 3	6.0	1.7	4.5	1.1	1.5	0.6
pH 7	6.5	2.1	5.6	1.3	. 1.0	0.9
pH 11	6.9	1.8	4.1	0.9	2.7	0.9
5 mg Br, ph 7	22.0	12.0	18.0	9.2	4.0	3.4

## Table 20 Effects of Sodium Sulfite on Chlorinated XAD8 Extract

## 6. TREATMENT OF THE OBSERVED HALOGENATED ORGANICS

Several treatment schemes were screened for their ability to minimize the formation of the observed halogenated organics. First, the application of powdered activated carbon (results would be comparable for granular activated carbon) before and after chlorination was evaluated. Second, disinfection with chloramines instead of free chlorine was tested. Third, aeration of chlorinated water samples in order to minimize the formation of the observed NVCO was attempted. Fourth, ozonation before and after chlorination was evaluated. Last, partial dechlorination and a two stage chlorination scheme which would involve chlorination, dechlorination and a subsequent chlorination were evaluated for treatment of the NVCO. Each of these treatment schemes will be described and discussed separately.

## 6.1 Treatment with Powdered Activated Carbon

One liter volumes of activated carbon effluent from the San Diego Wastewater Treatment plant (pre-chlorination water) was chlorinated in the laboratory with ten milligrams of chlorine at pH 7 for two hours. The water samples were treated with varying doses of powdered activated carbon (PAC) either before or after chlorination. The PAC used was Westvaco Nuchar SA-15 which had been rinsed three times with distilled methylene chloride before baking at 105<sup>o</sup>C for 24 hours. The weighed amount of PAC was added to the water sample in a one liter flask and was stirred for one hour. The filtered water sample was consequently extracted and analyzed by GC as previously described. Six of the eight samples were analyzed in duplicate.

Carbon treatment before chlorination investigates the ability of activated carbon to adsorb the NVCO precursors. Carbon treatment after chlorination addresses the ability of activated carbon to adsorb the formed halogenated organics.

1000 and 4000 mg doses of PAC were added before chlorination and 4000, 1000, 250, and 100 mg doses were added after chlorination. An untreated sample (San Diego carbon adsorption effluent) was also analyzed as well as a laboratory chlorinated sample which was untreated with PAC.

Figure 44 illustrates that PAC, added after chlorination, is very effective in reducing the total observed NVCO to the same level as before chlorination. The total NVCO ECD areas plotted in Figure 44 were evaluated as the area after chlorination minus the ECD area of the untreated carbon adsorption effluent (blank sample from San Diego).

Carbon treatment before chlorination does not seem to be effective in removing the NVCO precursors. This is the situation at the San Diego wastewater treatment plant, since the water is treated with activated carbon before chlorination, but still produces high halogenated organics concentrations.

6.2 Chloramines

Disinfection using chloramines has been successfully used by several workers to minimize THM and TOX formation and has been discussed in previous sections. An experiment was performed to quantify the utility of chloramines in reducing the observed halogenated organics.



Fig. 44: Treatment of NVCO by PAC. Chlorine dose = 10 mg/L, pH 7, contact time = 2 hours represented by 0 point. Left is PAC treatment after chlorination. Right is PAC treatment before chlorination.

XAD8 extractable organics from the aquaculture fields were chlorinated with ten milligrams of chlorine for two hours at pH 3, 7 and 11. Ammonia  $(NH_4Cl)$  was added using a 70 mg/ml  $N-NH_4$  stock solution. Three doses of ammonia were added before chlorine addition at each pH. The ammonia doses used were 14, 35 and 70 milligrams and each lies at a different point along the breakpoint curve. At high pH the dominant chlorine species is monochloramine and at low pH the dominant species is dichloramine. Six of the twelve samples were run in duplicate and the given values in Figure 45 are the calculated averages. The Supelcowax column (GC) was in poor condition at the time of the analysis and consequently a Carbowax 20M column was used in its place. The injector temperature was 215°C, and the detector maintained a 250°C temperature (since an effluent splitter was used, the detector temperature could exceed the column limit). The GC oven was programmed from 65 to 205°C at four degrees per minute after an initial four minute hold. Peak areas from this experiment are therefore not comparable with other previously described work, but in themselves allow for comparisons between disinfection with free and combined chlorine.

Figure 45 shows the total ECD area vs. the chlorine: $NH_4^+$  ratio for the chlorinated 1 mg TOC. Figure 45 also shows the location of each point along the breakpoint curve. The use of combined residuals reduces the observed NVCO levels by 32-62%. The chromatograms of the free and combined residuals extracts are very similar with a few exceptions. Basically, chloramines result in lower levels of most compounds and produce low amounts of a few new (unidentified) peaks.



Fig. 45: Reduction of NVCO levels by the use of chloramines. Chlorine dose = 10 mg, TOC = 1 mg, contact time = 2 hours.
#### 6.3 Aeration

Chlorinated water samples were aerated with high purity air in order to determine whether aeration is a viable treatment scheme for the observed halogenated organics. Eight hundred milliliters of distilled water was spiked with one milligram TOC of aquaculture XAD8 extract. The samples, each placed in a one liter beaker were chlorinated for two hours with 2.0, 10.0, and 50.0 milligram doses of chlorine at pH 7. The oxygen transfer coefficient  $K_LA$  was also measured ( $K_LA = 0.43$ ) and the data are provided in Appendix 4. The samples were aerated for three hours using a stone bubble diffuser with the diffuser placed in the center of the beaker, one inch from the bottom. Samples were also chlorinated for the total 5 hours without aeration as well as for two hours without aeration. The Carbowax 20M column was used in this experiment using the GC conditions described in Section 6.2.

The experiment was designed to show that heavy chlorine doses (50 milligrams) could be used to produce lighter compounds which could then be removed by aeration. The results of the experiment were disappointing in that aeration was not effective in removing even the lightest compounds ('A' reference numbers). The results were also difficult to interpret because aeration stripped the residual chlorine so the aerated samples were neither comparable to the two hour chlorinated samples nor the five hour chlorinated samples (without aeration). For example, the total ECD area for two hours of chlorination was  $6.4 \times 10^7$  (2 milligrams dose) and  $2.71 \times 10^7$  after five hours. With aeration the total area was  $3.68 \times 10^7$ . It is reasoned that aeration stripped the available chlorine at a point somewhere between two and five hours and consequently arrested further reaction (0 residual chlorine was measured after

aeration). Table 21 shows the total ECD areas for the nine tested conditions. Six of the nine points were run in duplicate.

Although the data is difficult to interpret, it is still evident that aeration is not effective in reducing the levels of the observed compounds. Aeration as a treatment method was consequently not pursued after this initial experiment.

Chlorine Dose	Total ECD Area 2 hours C <sub>12</sub>	Total ECD Area 5 hours C <sub>12</sub>	Total ECD Area Aerated
Milligrams	x 10 <sup>7</sup>	x 10 <sup>7</sup>	x 10 <sup>7</sup>
2.0	6.4	2.7	3.7
10.0	5.6	4.5	3.7
50.0	3.5	4.0	3.4

#### Table 21 Treatment of NVCO by Aeration

#### 6.4 Ozonation

Ozonation was screened for its ability to reduce the levels of the observed halogenated organics. In one experiment, the aquaculture XAD8 extract was ozonated before chlorination in order to render the precursors unreactive to subsequent chlorination. In a latter experiment, ozone was used to destroy the formed halogenated organics after chlorination. Neither experiment showed ozone to be a promising method to reduce the observed chlorination by-products. Ozonated samples without chlorination showed very little methylene chloride extractable organics.

One milligram of XAD8 aquaculture extract was diluted to twenty five milliliters. The sample was chlorinated at pH 7 for two hours with ten milligrams of chlorine. Ozone was applied by passing oxygen gas through a UV sterilizer. The formed ozone was bubbled into the XAD8 extract solution using a six inch pipet. The ozone residual was measured at 0.75 - 1.0 mg/L (orthotolidine method, Standard Methods 1985) and this residual was maintained throughout the ozonation period. The flask containing the XAD8 extract was stirred during the ozonation and was capped with parafilm in order to minimize evaporative losses. The samples were ozonated for one, two and four hours before chlorination. In the experiment designed to evaluate ozonation after chlorination the samples were ozonated for two hours. In both experiments, nitrogen gas was applied to the samples (in place of ozone) so as to insure that the observed differences are due to the reactive ozone species and not simply due to aeration. The final sample which was analyzed was ozonated for four hours without chlorination. All samples were analyzed in duplicate.

Ozonation after chlorination showed no significant improvement. One observes a 42% drop in total ECD area with ozone treatment and 43% drop with nitrogen treatment, implying that the decrease is attributable to evaporative losses. The gas chromatographs of the untreated and ozonated samples also look qualitatively identical.

The samples which were ozonated prior to chlorination showed different chromatographic patterns form the un-ozonated samples. Figure 46 compares the GC's for the un-ozonated sample and a sample which was ozonated for four hours prior to chlorination. One observes a sharp drop in the heavy, 'D', compounds and an increase in the unresolved 'hump' associated with the lighter 'A' compounds. The total ECD area drops by 37% for the four hour ozonated sample. Ozone has a powerful bleaching effect on the XAD8 extracts (color changes from yellow to milky-clear) and one observes identical chromatographs for the one, two and four hour pre-ozonated samples. Nitrogen gas sparging prior to chlorination shows no qualitative or quantitative difference (8% increase in total ECD area) with the untreated sample (chlorinated, but not sparged).

The sample which was ozonated for four hours without chlorination shows very little gas chromatographable compounds (FID and ECD). This only means that the breakdown products were not analyzable by the used analytical procedures. Evaluation of ozone as a disinfectant was beyond the scope of this research work.

The use of ozone in water treatment is a complex and broad field. These crude experiments were only meant to screen the possible utility of ozone for the reduction of the observed NVCO. Ozone was found to alter the precursors so as to change the chlorination breakdown products. The significance and utility of this observation can only be judged if the breakdown products after ozonation were found to be less harmful than without ozonation.

#### 6.5 Dechlorination

The discovery that sodium sulfite is reactive with some of the observed halogenated organics (discussed in Chapter 5) was initially very exciting as it appeared to be a solution to their elimination. A two stage chlorination





Fig. 46: GC's of the effect of pre-ozonation on NVCO formation. GC conditions as described in Section 6.4. Axes labeled for ECD.

procedure was envisioned, whereby the first chlorination would produce the halogenated by-products and dechlorination would eliminate some of these NVCO. The second chlorination should not produce any chlorination products since the precursors would have been eliminated. This scheme, however, has shown very little success. Apparently, the NVCO are reduced by sodium sulfite and rendered unchromatographable, but a subsequent chlorination oxidizes them to their previous chromatographable state. Figure 47 is a schematic of proposed reactions.

This procedure has been attempted nearly fifty times with very little success. The carbon adsorption effluent from the San Diego Wastewater Treatment Plant, as well as the aquaculture XAD8 extract were the chlorinated samples. The initial chlorination (the precursor consumption step) was attempted at pH 3, 7 and 11. High chlorine doses (10, 20, 40 and 100 mg/L) were used as well as long contact times (4-24 hours). The high chlorine doses and long contact times were intended to maximize the reaction of the precursors with chlorine. The second chlorination was always done for two hours at pH 7 using a 10 mg/L chlorine dose. The chromatograph of this twice chlorinated extract is then compared to a sample which was chlorinated for two hours at pH 7 using a 10 mg/L chlorine dose. The sodium sulfite addition step was done at various pH values since the  $SO_3^-$  ion has different redox potentials at the various pH's. In summary, no set of conditions was found which yields any significant treatment. Figure 48 serves as an illustrative example of the limited success shown by this method. The sample used to generate Figure 48 was chlorinated for 4 hours at pH 11, dechlorinated at pH 11 with excess sulfite (five fold excess), then chlorinated again at pH 7 with 10 milligrams of chlorine for two hours. The figure shows the sizeable total ECD area drop after dechlorination and its subsequent reappearance after the second chlorination.

Dechlorination has been shown to be a viable treatment for reducing the levels of the produced NVCO (Sections 5.2 and 5.3). Since it is necessary to maintain a chlorine residual in discharged waters, the effect of partial dechlorination on the observed halogenated organics was investigated. One liter of carbon adsorption effluent from the San Diego Wastewater Treatment plant was chlorinated using a 10 mg/L dose at pH 7 for two hours. The extractable organics were analyzed after partial and full dechlorination. Partial dechlorination (4 mg/L total available chlorine) results in a 65% decrease in the total ECD area and total dechlorination results in a 90% decrease in total ECD area. Partial dechlorination is consequently a desirable unit operation which is capable of significant reduction in the observed halogenated organics levels.



Fig. 47 Schematic of the Proposed 2-Stage Chlorination Scheme



Fig. 48 Treatment of NVCO Levels by 2-Stage Chlorination

### **V. SUMMARY, CONCLUSIONS AND RECOMMENDATIONS**

This research work has focussed on the gas chromatographable nonvolatile halogenated organics produced during the disinfection of water. Analysis, formation and treatment of these compounds were investigated. An improved analytical technique for the analysis of these compounds was developed which indicated that dechlorination prior to sample analysis is undesirable. The major precursors to the observed halogenated compounds are characterized. Third, some of the formed NVCO are identified. Fourth, chlorination parameters were varied to assess their importance for NVCO formation. Last, several treatment alternatives were screened for their abilities to reduce NVCO levels. The results from each of these five goals are listed below.

1. It was observed that many of the produced compounds are reactive with dechlorinating agents (sodium sulfite and sodium thiosulfate) and that they had escaped detection by workers who dechlorinated their samples prior to extraction. It is postulated that the sulfite ion undergoes a substitution reaction with halogen atoms. The most reactive group of compounds towards the sulfite ion was found to be the unsaturated, halogenated aliphatics. The sulfite ion was shown to be reactive with aqueous solutions of pure unsaturated halogenated compounds.

If knowledge of the exact reaction time between chlorine and the TOC in the water samples is not required, then use of dechlorinating agents is unnecessary. Researchers who require exact knowledge of reaction times in their analytical laboratory experiments may remove residual chlorine by rotoevaporation (Kringstad 1985) or perform the extraction in a time period which is small compared to the studied reaction times. Dechlorinating agents should only be added if the compounds of interest are known to not be reactive with the sulfite ion.

2. The major precursors to the observed halogenated compounds were found to be slightly organic solvent (methylene chloride) soluble and to have molecular weights less than 1000 daltons. The precursors were found to be collectible in the fraction that many workers call aquatic fulvic acid (Thurman and Malcolm 1983). The fact that these compounds are organic solvent soluble however, makes it difficult to continue to call them fulvic acids simply because they are yellow and are collectible by an adsorption method designed to collect humic and fulvic acids. It is hoped that deviation from traditional nomenclature will stimulate research to better classify aquatic fulvic acids. Humic acid was shown to definitely not be the major precursor to the observed compounds.

Table 22 lists the characteristics of the precursors and cites the section in the Results and Discussion chapter in which the experiment is discussed.

Flavones and flavenols provide good laboratory models of the precursors since they give similar chlorination patterns upon chlorination to the observed NVCO at the San Diego plant. The tested flavone compounds also possess similar MW and solubility properties to the

#### Table 22 Precursors Characteristics

	Observation	Reason	Section in Results and Discussion
1.	Precursors are acidic	XAD8 adsorbable in acid	3.1
2.	Precursors are polar	column chromatography polar fraction	3.2
3.	Precursors can't be too polar; organic solvent soluble.	they are $CH_2Cl_2$ extractable and desorbable by ether from XAD8 columns	3.2,3.3,3.4
4.	Precursors have MW less than 1000 daltons	ultrafiltration of XAD8 extract	3.7
5.	Precursors are common to water	present in tested water samples	3.8
6.	Precursors may be colored	all NVCO productive fractions were pale yellow to bright yellow	3.1,3.3-3.9
7.	Flavenols and flavones provide good precursor models	similar properties similar GC pattern	3.1-3.9

precursors. It is unlikely, however, that the tested flavones are the exact precursors. The precursors are more likely to be modified plant pigments due to secondary treatment and other biological and chemical alteration which the molecules may undergo.

- 3. The unavailability of a mass spectrophotometer on a routine basis made positive identification of the observed halogenated compounds a difficult task. In general, three categories of compounds were observed. Unsaturated, heavily chlorinated compounds which were reactive with sodium sulfite were identified. Chlorinated furan structures, as well as chlorinated phenolics, were also observed. The chlorinated furans were slightly reactive with sodium sulfite but the chlorophenols were unaffected by dechlorination.
- 4. It was observed that pH, chlorine dose, contact time, as well as bromide ion concentration greatly affect the relative distribution, as well as the total amounts of the chlorination by-products. A general recommendation of chlorination conditions is intentionally not presented; however, minimization of the observed NVCO occurred at low pH, long contact time and medium chlorine doses.

The NVCO which were monitored in this study are only a fraction of the total TOX formed upon chlorination. A recommendation of general chlorination conditions is dependent on the minimization of the most harmful components of TOX. A study which would address the formation of all the components of TOX and their relative toxicity would be needed to properly recommend chlorination conditions. Studies in the past which have recommended low chlorine dose in order to minimize THM formation would maximize the formation of some of the compounds observed in this study.

In addition to minimizing the harmful chlorination by-products, pH, chlorine dose and contact time can potentially be used to form components of TOX which are amenable to a subsequent treatment step. Conditions which maximize THM formation and minimize NPTOX formation can be used if aeration is used as a final polishing step. Conditions which lead to the formation of heavier components should be used if carbon adsorption is used as a final treatment step.

5. Several treatment schemes were screened for their ability to minimize the formation of the observed halogenated compounds. Carbon adsorption after chlorination was found to be the most effective treatment scheme. Chlorination using chloramines as well as partial dechlorination were also found to be effective treatment alternatives. Aeration was not found to be an effective treatment scheme since even the lightest components of the formed NVCO were not easily purged. Ozone treatment prior to chlorination changes the relative amounts of the formed halogenated organics. The importance of this latter observation depends on the relative toxicity of the various components.

The San Diego wastewater treatment plant effectively removes 97% of the extractable organics from the secondary effluent after carbon adsorption. The problematic treatment step at the plant is chlorination. Chlorination prior to carbon adsorption would be recommended. This chlorination step would be consumptive of the organic precursors and the carbon adsorption process is capable of removing a sizeable fraction of the formed TOX. Carbon adsorption will also dechlorinate the water which would necessitate a second chlorination after carbon treatment. This second chlorination should not be as TOX productive as the initial chlorination since much of the precursors would have been consumed in the initial chlorination. Partial dechlorination shall be performed after this second chlorination step.

#### **VI. REFERENCES**

- 1. Andelman, J.B., Shapiro, M.A., and Ruppel, T.C., Purdue University Eng. Bull. Ext. Ser. 118:220(1965).
- 2. ASTM Committee, Proposed Method of Test for Organic Halides in Water by Carbon Adsorption-Microcoulometric Detection, Joyce, R.J., Task Group Chairman, ASTM Committee D-19; 1981.
- 3. Baker, R.A., and Malo, B.A., "Water Quality Characterization Trace Organics," J. Sanit. Eng. Div., ASCE, 93:(6) (1967).
- 4. Bean, R.M., Mann, D.C., and Neitzel, D.A., "Organohalogens in Chlorinated Cooling Waters Discharged from Nuclear Power Stations," *Water Chlorination Environmental Impact and Health Effects*, Jolley, R.L. ed., 4:383 (1983).
- 5. Becher, G., Carlberg, G.E., Gjessing, E.T., Hongslo, J.K., and Monarca, S., "High-Performance Size Exclusion Chromatography of Chlorinated Natural Humic Water and Mutagenicity Studies Using the Microscale Fluctuation Assay," *EST*, 19:422 (1985).
- 6. Bellar, T.A., and Litchenberg, J.J., "Determining Volatile Organics at Microgram-per-Liter Levels by Gas Chromatography, JAWWA, 739 (1974).
- Boyce, S.D., Barefoot, A.C., Britton, D.R., and Hornig, J.F., "Formation of Trihalomethanes from the Halogenation of 1,3-Dihydroxybenzenes in Dilute Aqueous Solution: Synthesis of 2-\*Resorcinol and its Reaction with Chlorine and Bromine, Water Chlorination Environmental Impact and Health Effects, Jolley, R.L., ed. Vol. 4, p. 253, Ann Arbor Science (1983).
- 8. Boyce, S.D., Hornig, J.F., "Formation of Chloroform from the Chlorination of Diketones and Polyhydroxybenzenes in Dilute Aqueous Solution," *Water Chlorination Environmental Impact and Health Effects*, Jolley, R.L., ed. Vol. 3, p. 131, Ann Arbor Science (1979).
- 9. Briley, K.F., Williams, R.F., Longley, K.E., and Sorber, C.A., "Trihalomethane Production from Algal Precursors," *Water Chlorination Environmental Impact and Health Effects*, Jolley, R.L., ed. Vol. 3, p. 117, Ann Arbor Science (1979).
- 10. Bull, R.J., "Health Effects of Drinking Water Disinfectants and Disinfectant By-Products," EST, 16:552A (1982).
- 11. Burnham, A.K., Calder, G.V., Fritz, J.S., Junk, G.A., Svec, H.J. and Willis, R., "Identification and Estimation of Neutral Organic Contaminants in Potable Water," *Anal. Chem.*, 44:139 (1972).
- 12. Butterfield, C.T., Wattie, E., Megregian, S. and Chambers, C.W.,

"Influence of pH and Temperature on the Survival of Coliforms and Enteric Pathogens when Exposed to Free Chlorine," Public Health Reports, 58(51):1837 (1943).

- 13. Callaway, J.Y., Gabbita, K.V., and Vilker, V.L., "Reduction of Low Molecular Weight Halocarbons in the Vapor Phase above Concentrated Humic Acid Solutions," *EST*, 18:890 (1984).
- 14. Christman, R.F., Johnson, J.D., et al., "Chlorination of Aquatic Humic Substances," National Technical Information Service, PB161952 (1981).
- 15. Christman, R.F., and Gjessing, E.T., ed., Aquatic and Terrestrial Humic Materials, Ann Arbor Science, (1983).
- 16. Christman, R.F., Norwood, D., Personal Communication (1986).
- 17. Chow, B.M., Roberts, and P.V., "Halogenated Byproduct Formation by *ClO*<sub>2</sub> and *Cl*<sub>2</sub>," *J. Envr. Engr. Div.*, ASCE, 107:609 (1981).
- 18. Coleman, W.E., Melton, R.G., Kopfler, F.C., Barone, K.A., Aurand, T.A., and Jellison, M.G., "Identification of Organic Compounds in Mutagenic Extract of a Surface Drinking Water by a Computerized Gas Chromatography/Mass Spectrometry System (GC/MS/COM), EST 14:576 (1980).
- 19. Coleman, W.E., Munch, J.W., Kaylor, W.H., Strelcher, R.P., Ringhand, H.P., Meler, J.R., "Gas Chromatography/Mass Spectroscopy Analysis of Mutagenic Extracts of Aqueous Chlorinated Humic Acid. A Comparison of the Byproducts to Drinking Water Contaminants. *EST*, 18:674 (1984).
- 20. Collins, H.F., Selleck, R.E., and White, G.C., "Problems in Obtaining Adequate Sewage Disinfection," J. Sanitary Engineering Div., ASCE, 97:549 (1979).
- 21. Cotruva, J.A., "THM's in Drinking Water," EST. 15:268 (1981).
- 22. Cummings, R.B., Jolley, R.L., Lee, N.E., Lewis, L.R., and Thompson, J.E., "Mutagenicity of Nonvolatile Organics in Undisinfected and Disinfected Wastewater Effluents," *Water Chlorination Environmental Impact and Health Effects*, Jolley, R.L. ed., Vol. 4, p. 1279 (1983)
- 23. De Leer, E.W.B., "The Identification of Highly Chlorinated Ethers and Diethers in River Sediment near an Epichlorohydrin Plant, Water Research, 19:1411 (1985).
- 24. Digiano, F.A., Uden, P.C., Saracen, W.C., and Coker, E.L., "Characterization and Treatability of the By-Products of Naturally Occurring Humic Substances," *National Technical Information Service*, PB83-208868 (1983).

- 25. Dragunev, S.S., Murzakov, B.G., Soviet Soil Science (English translation), p. 253 (1969).
- 26. Dubois, M., Gilles, K.A., Hamilton, J.K., Rebers, P.A., and Smith, F., "Colorimetric Method for Determination of Sugars and Related Substances, *Analytical Chemistry*, 28:350 (1956).
- 27. Fleischacker, S.J., and Randtke, S.J., "Formation of Organic Chlorine in Public Water Supplies," JAWWA, 3, 132 (1983).
- 28. Gabbita, K.V., Callaway, J.Y. and Vilker, V.L., "Detection and Quantitation of Trace Levels of Low Molecular Weight Halocarbons (LMHs) Associated with Commercial Sodium Humate," *Toxicol. and Env. Chem.*, 9:247 (1985).
- 29. Gabbita, K.V., "Presence of 1,2-dibromo-3-chloropropane (DBCP) Residues in Sodium Humate and its Possible Significance, "*Toxicol. and Env. Chem.*, 11:203 (1986).
- 30. Gilliam, A.H., Riley, J.P., "Microsacale Functional Group Analysis of Marine and Sedimentary Humic Substances," Analytica Chimica Acta., 141:287 (1982).
- 31. Gjessing, E.T., ed., *Physical and Chemical Characteristics of Aquatic Humus*, Ann Arbor Science, 1976.
- 32. Glaze, W.H., and Henderson, J.E., "Formation of Organochlorine Compounds from the Chlorination of a Municipal Secondary Effluent, *JWPCF*, 47:2511 (1975).
- 33. Glaze, W.H., Peyton, G.R., and Rawley, R., "Total Organic Halogen as Water Quality Parameter: Adsorption/Microcoulometric Method," *EST.*, 11:685 (1977).
- 34. Glaze, W.H., Peyton, G.R., Saleh, F.Y., Huang, F.Y., "Analysis of Disinfection By-Products in Water and Wastewater," Inter. J. Environ. Anal. Chem., 7:143 (1979).
- 35. Glaze, W.H., Rawley, R., Burleson, J.L., Mapel, D., and Scott, D.R., "Further Optimization of the Pentane Liquid-Liquid Extraction Method for the Analysis of Trace Organic Compounds in Water," Advances in the Identification and Analysis of Organic Pollutants in Water, Keith, L.H., ed. p. 267 (1981).
- 36. Gutsche, D.C., and Pasto, D.J., Fundamentals of Organic Chemistry, Prentice Hall, 1975.
- 37. Henderson, J.E., Peyton, G.R., and Glaze, W.H., "A Convenient Liquid-Liquid Extraction Method for the Determination of Halomethanes in Water at the Parts-per-Billion Level," Advances in the Identification and Analysis of Organic Pollutants in Water. Keith,

L.H., ed. p. 105 (1976).

- 38. Hoehn, R.C., Barnes, D.B., Thompson, B.C., Randall, C.W., Grizzard, T.J., and Shaffer, P.T.B., "Algae as Sources of Trihalomethane Precursors, Annual Conference of AWWA, San Francisco, CA 1979.
- 39. Hollod, G.J., and Wilde, E.W., "Trihalomethanes in Chlorinated Cooling Waters of Nuclear Reactors," *Bull. Environ. Toxicol.* 28:404 (1982).
- 40. Ingols, R.S., et al., "Bactericidal Studies of Chlorine," Indus. Engr. Chem., 45:966 (1953).
- 41. Jenkel, M.R., and Roberts, P.V., "Total Organic Halogen as a Parameter for the Characterization of Reclaimed Waters: Measurement, Occurrence, Formation and Removal," *EST*, 14:970 (1980).
- 42. Johnson, J.D., and Jensen, J.N., "THM and TOX Formation: Routes, Rates, and Precursors," JAWWA, 4:157 (1986).
- 43. Johnson, D.E., Randtke, S.J., "Removing Non-Volatile Organic Chlorine and its Precursors by Coagulation and Softening," JAWWA, 249 (1983).
- 44. Jolley, R.L., Jones, G., Pitt, W.W., and Thompson, J.E., "Chlorination of Organics in Cooling Waters and Process Effluents," *Water Chlorination Environmental Impact and Health Effects*, Vol. 1, p. 105 (1978).
- 45. Junk, G.A, Richard, J.J., Grieser, M.D., Witiak, D., Witiak, J.L., Arguello, M.D., Vick, R., Svec, H.J., Fritz, J.S., and Calder, G.V., "Use of Macroreticular Resins in the Analysis of Water for Trace Organic Contaminants," J. of Chromatography, 99:745 (1974).
- 46. Kaiser, K.L.E., and Oliver, B.G., "Determination of Volatile Halogenated Hydrocarbons in Water by Gas Chromatography," *Analytical Chemistry*, 48:2207 (1976).
- 47. Kissinger, L.D., and Fritz, J.S., "Analytical Notes Analysis of Drinking Water for Haloforms," JAWWA, 435 (1976).
- 48. Kokoropoulos, P. and Manos, G.P., "Kinetics as Design Criteria for Post Chlorination," J. Env. Engr. Div., ASCE, 99:73-83 (1973).
- 49. Kringstad, K.P., Sousa, D.F., and Stromberg, L.M., "Studies on the Chlorination of Chlorligins and Humic Acid," *EST*, 19:427 (1985).
- 50. Liao, W., Christman, R.F., Johnson, D.J., and Millington, D.S., "Structural Characterization of Aquatic Humic Material," *EST*, 16:403 (1982).
- 51. Lin, S., Liukkonen, R.J., Thom, R.E., Bastlan, J.G., Lukasewycz, M.T.,

and Carlson, R.M., "Increased Chloroform Production from Model Components of Aquatic Humas and Mixtures of Chlorine Dioxide/Chlorine," *EST*, 18:932 (1984).

- 52. Malcolm, R.L., Wershaw, R.L., Thurman, E.M., Aiken, G.R., Pinckney, D.J., and Kaakinen, J., "Reconnaissance Samplings and Characterizations of Aquatic Humic Substances at the Yuma Desalting Test Facility, Arizona," USGS, (1981).
- 53. McCarthy, P., Peterson, M.J., Malcolm, R.L., Thurman, E.M., "Separation of Humic Substances by pH Gradient Desorption from a Hydrophobic Resin," *Anal. Chem.*, 51:2041 (1979).
- 54. McCreary, J.J., and Snoeyink, V.L., "Characterization and Activated Carbon Adsorption of Several Humic Substances," *Water Research*, 14:151 (1980).
- 55. McCreary, J.J., and Snoeyink, V.L., "Reaction of Free Chlorine with Humic Substances before and after Adsorption on Activated Carbon, EST, 15:193 (1981).
- 56. Mieure, J.P., "A Rapid and Sensitive Method for Determining Volatile Organohalides in Water," JAWWA, 60 (1977).
- 57. Miller, J.W., and Uden, P.C., "Characterization of Nonvolatile Aqueous Chlorination Products of Humic Substances," *EST*, 17:150 (1983).
- 58. Minear, R.A., and Bird, J.C., "Trihalomethanes: Impact of Bromide Ion Concentration on Yield, Species Distribution, Rate of Formation and Influence of other Variables," *Water Chlorination Environmental Impact and Health Effects*, Vol. 3, p. 151, (1979).
- 59. Morris, J.C., "Kinetic Reactions between Aqueous Chlorine and Nitrogen Compounds," Fourth Rudolph's Research Conference, Rutgers University, 1965.
- 60. Morris, J.C., "The Chemistry of Aqueous Chlorine in Relation to Water Chlorination," Water Chlorination Environmental Impact and Health Effects, Vol. 1, p. 21, (1978).
- 61. Morris, J.C., Baum, ??, "Precursors and Mechanisms of Haloform Formation in Chlorination of Water Supplies, *Water Chlorination Environmental Impact and Health Effects*, Vol. 2, p. 29, (1978).
- 62. Nicholson, A.A., Meresz, O., and Lemyk, B., "Determination of Free and Potential Haloforms in Drinking Water," *Anal. Chem.*, 49:814 (1977).
- 63. Norman, T.S., Harms, L.L., and Looyenga, R.W., "The Use of Chloramines to Prevent Trihalomethane Formation," JAWWA, 176 (1980).

- 64. Norwood, D.L., Johnson, D.J., and Christman, R.F., "Reactions of Chlorine with Selected Aromatic Models of Aquatic Humic Material, *EST*, 14:187 (1980).
- 65. Norwood, D.L., Johnson, J.D., Christman, R.F., and Millington, D.S., "Chlorination Products from Aquatic Humic Material at Neutral pH," Water Chlorination Environmental Impact and Health Effects, Vol. 4, p. 383, (1983).
- 66. Odegaard, H., Koottatep, S., "Removal of Humic Substances from Natural Waters by Reverse Osmosis," *Water Research*, 16:613 (1982).
- 67. Oliver, B.G., "Effect of Temperature, pH and Bromide Concentration on the Trihalomethane Reaction of Chlorine with Aquatic Humic Material," *Water Chlorination Environmental and Health Effects*, Jolley, R.L. ed., Vol. 3, p. 141, Ann Arbor Science (1979).
- 68. Oliver, B.G., and Lawrence, J., "Haloforms in Drinking Water: A Study of Precursors and Precursor Removal," JAWWA, 161 (1979).
- 69. Oliver, B.G., and Visser, S.A., "Chloroform Production from the Chlorination of Aquatic Humic Material: The Effect of Molecular Weight, Environment and Season," *Water Research*, 14:1137 (1980).
- 70. Onodera, S., Yamada, K., Yamaji, Y., and Ishikura, S., "Formation of Polychlorinated Phenoxyphenols during the Reaction of Phenol with Hypochlorite in Dilute Aqueous Solution, J. of Chromatography, 288:91 (1984).
- 71. Peters, C.J., Young, R.J., and Perry, R., "Factors Influencing the Formation of Haloforms in the Chlorination of Humic Materials," *EST*, 14:1391 (1980).
- 72. Quimby, B.D., Delaney, M.F., Uden, P.C., and Barnes, R.M., "Determination of the Aqueous Chlorination Products of Humic Substances by Gas Chromatography with Microwave Emission Detection," *Anal. Chem.*, 52:259 (1980).
- 73. Reckhow, D.A., and Singer, P.C., "The Removal of Organic Halide Precursors by Pre-ozonation and Alum Coagulation," *JAWWA*, 4, 151, (1984).
- 74. Reinhard, M., "Molecular Weight Distribution of Dissolved Organic Halogen in Advanced Treated Waters," *EST*, 18:410 (1984).
- 75. Richard, J.R. and Junk, G.A., "Liquid Extraction for the Rapid Determination of Halomethanes in Water," JAWWA, 62 (1977).
- 76. Robbins, S.L., Cotran, R.S., *Pathological Basis of Disease*, Saunders Publishing (1984).

- 77. Robinson, T., The Organic Constituents of Higher Plants, 4th ed., Cordus Press, Amherst, MA (1980).
- 78. Rook, J.J., "Formation of Haloforms During Chlorination of Natural Waters," J. Water Treatment Exam., 23:234 (1974).
- 79. Rook, J.J., "Haloforms in Drinking Water," JAWWA, 168 (1976).
- 80. Rook, J.J., "Possible Pathways for the Formation of Chlorinated Degradation Products during Chlorination Humic Acids and Resorcinol," *Water Chlorination Environmental Impact and Health Effects*, Jolly, R.L., ed. Vol. 3, p. 85, Ann Arbor Science (1979).
- 81. Saleh, F.Y., and Mokti, M., "Fulvic Acid and Chlorinated Fulvic Acid in Water and Sediment: HPLC Fractionation and Spectroscopic Characterization, *Water Chlorination Environmental Impact and Health Effects*, Jolley, R.L., ed., Vol. 3, p. 201, (1983).
- 82. Saunier, B.M., and Selleck, R.E., "The Kinetics of Breakpoint Chlorination in Continuous Flow Systems," JAWWA 3:164, (1979).
- 83. Schroeter, L.C., Sulfur Dioxide; Applications in Foods, Beverages, and Pharmaceuticals, Pergamon Press, 1966.
- 84. Selleck, R.E., Saunier, B.M., and Collins, H.F., "Kinetics of Bacterial Deactivation with Chlorine," J. Environ. Engr. Div., ASCE, 104:1197 (1978).
- 85. Sepp, E., "Optimization of Chlorine Disinfection Efficiency," J. Environ. Engr. Div., ASCE, 107:139 (1981).
- 86. Shinohara, R., Kido, A., Etu, S., Hori, T., Koga, M., and Akiyama, T., "Identification and Determination of Trace Organic Substances in Tap Water by Computerized Gas Chromatography - Mass Spectrometry and Mass Fragmentography, *Water Research*, 15:535 (1981).
- 87. Snoeyink, V.L., Clark, R.R., McCreary, J.J., and McHie, W.F., "Organic Compounds Produced by the Aqueous Free-Chlorine-Activated Carbon Reaction," EST, 15:188 (1981).
- 88. Standard Methods, Standard Methods for the Examination of Water and Wastewater, Am. Public Health Assoc. (1980).
- 89. Stanbro, W.D., and Smith, W.D., "Kinetics and Mechanism of the Decomposition of N-Chloroalanine in Aqueous Solution," *EST*, 13:446 (1979).
- 90. Stenstrom, M.K., Fam, S., and Silverman, G.S., "Use of a Modified Oil and Grease Analytical Method to Assess the Quality of Urban Runoff," Oil and Freshwater Conference, Edmonton, Canada, 1984.

- 91. Stevens, A.A., Slocum, C.J., Seeger, D.R., and Robeck, G.G., "Chlorination of Organics in Drinking Water," JAWWA, 615 (1976).
- 92. Thomas, Q.V., Stork, J.R., and Lammert, S.L., "The Chromatographic and GC/MS Analysis of Organic Priority Pollutants in Water, J. of Chromatography, 18:583 (1980).
- 93. Thurman, E.M., Malcolm, R.L., "Preparative Isolation of Aquatic Humic Substances," *EST*, 15:463 (1981).
- 94. Urano, K., Wada, H., and Takemasa, T., "Empirical Rate Equation for Trihalomethane Formation with Chlorination of Humic Substances in Water," *Water Research*, 12:1797 (1983).
- 95. U.S. Environmental Protection Agency, Federal Register, 44:68670 (1979).
- 96. U.S. Environmental Protection Agency, Method 450.1 Interim Envn. Monitoring and Support Lab, Physical and Chemical Methods Br., Cincinnati, Ohio (November 1980).
- 97. Wachter, J.K., and Andelman, J.B., "Organohalide Formation on Chlorination of Algal Extracellular Products," *EST*, 18:811 (1984).
- 98. White, G.C., "Current Chlorination and Dechlorination Practices in the Treatment of Potable Water, Wastewater and Cooling Water," *Water Chlorination Environmental Impact and Health Effects*, Jolley, R.L., ed., p. 1 (1978). (Vol. 2)
- 99. White, G.C., *The Handbook of Chlorination*, Van Nostrand Reinhold, 2nd edition, New York (1986).
- 100. Wong, G.T.F., Oatts, T.J., "Dissolved Organic Matter and the Dissipation of Chlorine in Estuarine Water and Seawater," *Water Research*, 18:501(1984).

## **Appendix 1**

In order to better select the most desirable membranes for the proposed expansion of the San Diego Aquaculture treatment system, a "cocktail" composed of various compounds was prepared. These compounds were selected to represent several classes of chemicals. Each class was selected with several similar compounds with different substitutions.

Several iterations of the cocktail formulation were made. Finally the list of compounds shown in Table A1 was selected. These were all soluble enough to be conveniently introduced in the RO feedwater. The compounds were also selected to be identifiable by the previously described GC procedure. The concentration was adjusted to provide approximately 100  $\mu$ g/l in the RO feedwater, so the product water will remain above minimum detection levels.

The cocktail containing the selected compounds was solubilized in 5 gallons of methanol. The methanol was then diluted to 100 gallons with warm tap water. The tap water was then injected into the RO feedwater pump suction line at 5.0 GPM for 18 minutes. This flow represented approximately 10% of the RO feedwater flow. Brine and product water samples were collected after 25 minutes of operation. This sampling time was determined by using a salt tracer, which showed that 25 minutes was sufficient to allow the cocktail to reach the RO brine water. A cocktail for selenate and selenite was also used. This cocktail consisted of a 100 gallon solution of each compound. Each tank was injected as described previously. Initial selenate or selenite concentration in the feed water containing the cocktail was  $300 \mu g/l$ .

At the time of the survey, the RO plant was arranged into three stages of 14, 7 and 3 membranes (pyramid fashion). The last three membranes were changed from the CA membranes traditionally used to the three test low pressure membranes by adding a pressure reducing value. By collecting the brine and product water from each type of membrane, four evaluations were made.

Table A1 shows the results of the survey. In general, all four membranes provided excellent rejection. The ketones were not rejected by the cellulose acetate membranes, and as a result, no analysis of the low pressure membranes could be made. An interference to the aniline analysis occurred, and the data shown in Table A1 for aniline are spurious.

	Cellulose	Membrane Type		
Compound	Acetate	Film Tech	Fluid Systems	Desalination
2	8 4 4	NT	ND	ND
2-octanone	-0.44		ND	ND
2-nonanone	12.34		100	05 10
tetradecane	100.	98.20	100.	95.10
tetradecene	100.	97.33	100.	95.08
hexadecane	100.	97.89	100.	92.16
hexadecene	100.	98.23	100.	95.03
aniline	-149.71	ND	ND	ND
decanol	93.34	100.	100.	100.
octadecane	100.	98.64	100.	95.93
chlorophenol	58.20	98.43	97.12	<b>97.3</b> 7
octadecene	100.	98.53	100.	95.58
phenol	27.20	97.46	96.64	95.46
eicosane	100.	98.59	100.	98.02
2 5-dimethylphenol	51.65	ND	ND	ND
m-cresol	29.82	96.24	96.54	92.16
hevadecanone	100	98.43	99.88	96.28
propyl phenol	88.60	96.75	98.17	92.15
2.2 dimethylphenol	65 57	94.88	93 17	88.98
2,5 unically phonol	87.20	98.05	99 19	94 95
2 4 6 trichlorophanol	00.08	08 11	99.97	98.06
2,4,6 inchorophenor	77.70 07.55	00.17	100	97 11
nexadecanol	97.55	99.12	00.87	88.45
2,4,5 trichlorophenol	99.93	90.47	99.07 100	07.46
octadecanol	97.77	98.92	100.	77.40 07 70
selenate	97.48	99.18	99.30	91.12
selenite	97.62	97.95	95.42	90.31

# Table A1. Contaminant Mass Rejected by Membrane Type<sup>-1</sup>

Key: ND not detected, due to interferences or too low concentration in the feedwater to the third stage.

1 Table values calculated as follows:

$$Rejection = 100 \left[ 1. - \frac{Q_p C_p}{Q_f C_f} \right]$$

where

 $Q_f =$  Feed flow rate  $Q_p =$  Product flow rate  $C_f =$  Feed concentration  $C_p =$  Product concentration

# Appendix 2

Computer reconstructed electron impact mass spectra (MS) of some of the halogenated compounds listed in Table 14 are shown in the following pages.












































## **APPENDIX 3**

Some of the Hewlett Packard integrator output from one of the experiments designed to assess the effects of chlorine dose, contact time and pH on the formation of the observed halogenated compounds is provided in this appendix. 1 mg TOC (XAD8 aquaculture extract) was chlorinated at varying chlorine doses, contact times and pH values.

The base conditions of 2.5 mg chlorine, pH 7, and two hour contact time are shown below (Table A3). The identified peaks are labeled by reference numbers in this chromatograph (see Table 14). The formation of these compounds may be followed in subsequent chromatographs by retention time matching (RT). The retention times usually match within a 0.04 minute window. The subsequent chromatographs include checkpoints to aid the interested reader in matching the retention times. The checkpoints indicate the difference (RT) at that point in the chromatograph from the base conditions. The retention time difference for peaks between checkpoints from the base conditions (Table A3) can be evaluated by interpolation.

These files were not edited so as to allow for calculation of total areas within desired retention time regions. For example, it is possible to group the areas of compounds eluting before a given retention time or of 'A#' compounds or in any other desired fashion. The area rejection was set at 10,000 counts. All chromatographs were run at identical dilutions and the area counts are directly comparable. Table A2 lists the chlorination conditions of the chromatographs shown in this appendix.

Table Number	pН	Chlorine dose (mg)	Time (hours)	Bromide (mg)	TOC (mg)
A3	7.0	2.5	2.0	0.0	1.0
A4	7.0	5.0	2.0	0.0	1.0
A5	7.0	10.0	2.0	0.0	1.0
A6	7.0	20.0	2.0	0.0	1.0
A7	7.0	40.0	2.0	0.0	1.0
A8	7.0	1.0	2.0	0.0	1.0
A9	7.0	0.5	2.0	0.0	1.0
A10	7.0	2.5	0.25	0.0	1.0
A11	7.0	2.5	0.5	0.0	1.0
A12	7.0	2.5	1.0	0.0	1.0
A13	7.0	2.5	4.0	0.0	1.0
A14	7.0	2.5	8.0	0.0	1.0
A15	7.0	2.5	24.0	0.0	1.0
A16	3.0	2.5	2.0	0.0	1.0
A17	5.0	2.5	2.0	0.0	1.0
A18	9.0	2.5	2.0	0.0	1.0
A19	11.0	2.5	2.0	0.0	1.0
A20	7.0	10.0	2.0	5.0	1.0

Table A2 List of Chlorination Conditions and Table Numbers

0.11	0.173	ž.	100920	36.07		0.012	0.072	N	10241	CO. 47
0.02	0.035		21443	15 QS		0.054	0.126	įŦ	100/1	23.81
0.01	0.108	1	12040	33.73		0.026	0.082	Ē	22503	23.70
0.01	0.109	Ę	12980	35.51		0.017	0.095	Ŧ	14676	23.57
0.060	0.101	3	53063	35.30	A24	0.012	0.128	PH	10601	23.48
0.025	0.076	P	22381	34.92	A23	0.057	0.087	Ą	50717	22.64
0.037	0.082	Ş	32263	34.45		0.023	0.108	Ŧ	20657	22.09
0.100	0.141	\$	88092	34.30		0.031	0.154	ž 3	27450	21.78
0.03	0.074	2 4	23445	JJ. 46		0.027	0.083	Į	24074	20.99
0.090	0.095	5 3	. 84036	55.UV		0.024	0.117	PP	21352	19.67
0.042	0.105	1	37464	32.90	· A21	0.048	0.074	Ę	42634	19.38
0.080	0.140	Ş	70876	32.63		0.016	0.123	2	13955	19,13
0.021	0.089	Ş	18458	32.30		0.029	0.151	Ş	25342	18.15
0.035	0.134	\$	31312	32,20	A19	0.091	0.103	\$:	80018	17.95
0.021	0.105	٤:	20227	32.01		2.04/	0,141	2 8	78151 0004001	17 49
0.020	0.082	23	20457	11. PQ		0.910	0.212		0966.09	16.09
0.04	0.U99	53	17517	26.1C	A17	2.527	0.143	12	2233400	15.71
0.10	0.103	1		ay 15	A16	0.663	0.256	Ş	586110	15.33
0.014	0.102	5	12504	21.15		0.395	0.158	5	349180	15.22
0.018	0.111	Į	16042	30.87		0.088	0.044	۵ ۲	77692	15.06
0.075	0.143	1	66318	30.61		0.504	0.221	Ş	445210	14.88
0.010	0.120	Ş	14316	30.29		0.521	0.205	¥	460620	14.62
0.01	0.075	Ş	11005	30.18		0.089	0.082	Ş	78979	14.48
0.037	0.113	Ş	32946	29.97		0.090	0.106	¥	79262	14,40
0.022	0.104	Ş	19662	29.87		0.064	0.098	\$	56096	14.21
0.017	0.098	Ş	15152	29.75		0.024	0.078	23	20653	14.09
0.025	0.106	\$:	22100	29.57	A14	3.912	0.119		3457300	13.37
0.050	0.207	\$:	49602	29.13		0.012		83	700L7 CLCC0	12.30
	0 160	53	10101	28.33		0.031	0.12/	2 2	11694	14.00
0.0/	0.131	53	60400	17.07	A13	0.063	0.163	1	55 371	11.95
0.034	0.098	12	29939	20.07	A12	0.455	0.169	Ş	402370	11.09
0.060	0.118	5	53072	27.91		1.417	0.135	¥	1252300	10.86
0.015	0.084	Ş	12904	27.78	A11	0.580	0.111	Ş	512090	10.69
0.015	0.061	Ş	13523	27.56	A10	0.342	0.172	\$!	302310	10.18
0.016	0.069	\$	13768	27.49	A9,0	0.112	0.155		90780	
0.04	0.137	53	42170	27.02		35.982	0.219	52	3.1797E+07	7.86
0.013	0.107	12	11784	26.78		0.012	0.086	þþ	10631	7.61
0.031	0.135	Ş	27069	26.50		0.315	0.207	Ą	278390	7.21
0.029	0.112	Ş	25479	26.37	2	2.308	0.154	ž i	2039300	6.63
0.01	0.119	\$ :	27283	26.26	A)	1 264		20	1117100	
0.000	0.102	53	67571	26.05	Reference Number	AVEN.	ANV/HI	TALL	ANLA	2
0.130		53	00101	23.00	) 1					AREAT
0.380	0.134	5	3350/0	10.07						1D: 000
0.126	0.141	1	111340	25.19		LE NAME:	, WORKT I		10: C	WORKF ILE
0.054	0.123	2	47344	24.72		20:15:38	PR/29/86	2	82.	RUN # 7
0.014	0.087	2	12008	24.48						
0.055	0.143	Ş	48377	24.27		onditions	ination c	chlor	8034	
0.047	0.087	Ş	41245	24.16						
							Table A3	_4		

	0.024	0.035	0.014	0.038	0.068	0.041	0.027																																											
	0.106	0.095	0.037	0.103	0.129	0.053	0,040																																											
i	2	02 W	77 D W	45 D VV	93 BV	32 W	66 D W	67E+07	00E+00																																									
	C I Z		125	939	780	365	237	EA= 8.83	OR= 1.00																																									
	21.64	52.23	87.66	16.29	95.99	96.03	96.12	TOTAL AR	HUL FACT																																									
40.0	0.011	0.055	0.070	0.084	0 012	0 033	0.021	0 036	20.00			0.041		0.066	0.061	0.114	0.016	0.061	0.016	0.017	0.124	0.127	0.026	0.020	0.028	0.019	0.029	0. 145	0.072	0.029		0.055	0.081	0.075	0.015		0.056	0.032	0.020	0.035	0.134	0.067	0.043	0.080	0.034	0.026	0.058	0.025	0.015	0.015
0.123	0.104	0.119	0.132	0.132	0.090	0,101	0.138	0.152	0 073	0.179	0.115	0.162	0,167	0.137	0.174	0.160	0.109	0.179	0.136	0.144	0.187	0.164	0.216	0.168	0.144	0.147	0.151		0.254		0.078	0.067	0.093	0.104	0.10	0.106	0.102	0.184	0.121	0.129	0.119	0.054	0. 282	0.149	0.055	0.048	0.128	0.110	0.054	0.133
\$	3	3	3	2	3	3	2	3	3	3	2	3	3	3	3	3	3	4	3	3	3	3	3	\$	3	\$ !	51	<b>t</b> 3	\$ 3	: 3	:3	3	3	3	23	:3	2	2	3	3	2	\$	\$	2	3	3	≥ i	Z i	3	:3
29738	28750	48336	62105	74513	10632	19407	62300	31795	13150	31474	24621	36416	51681	58185	53883	100670	14396	54020	16961	15253	109560	112250	22512	17332	26938	10901	80002	050021	01720	53678	16934	48557	71217	66125 D	13214 41280	42550 D	49801	26311	17457	31137	118280	58729	38124	70826	29703	23297 D	51611 D	21122	25661	13403
50.36	50.53	50.78	50.93	51.54	51.79	51.99	52.53	52.76	\$3.00	53.17	\$3.79	54.26	\$5.57	56.29	56.51	56.78	57.32	57.72	58.80	59.99	60.29	61.03	62.30	63. 29	04 . 20 46 01	10.CD		67.13	67.94	68.06	68.14	68.20	68.27	68.36 40 30	69, 50 69, 52	69.55	70.42	73.43	73.99	74.56	77.38	64.77	79.58	83.12	63.16 55 5:	83.21	83. 26 86 13	21.00	07.10 AA AA	89.70
2 5	3	5		2	1			1	5	90	1	01				2	2	2	2				010						110			210			610					114	1									
0.227	077 · A	1.015	0.040	0.304	0.181	0.040	0.126	0.107	0.064	1.179	0.344	0.458	0.474	0.073	0.109	0.129	017.0	660.0				51 C	101.0	0.059	0.035	0.100	0.023	0.077	0.168	0.367	0.027	0.054	170.0	0.039	0.076	0.030	0.015	0.142	C 00.00	0.000		0.40	0.100	110.0	0 128	0.014	0.115	0.093	0.057	0.076
0.138	0.1.4	0.092	0.091	0.139	0.125	0.129	0.118	0.142	0.169	0.099	0.200	0.180	0.161	0.081	0,120	0.146	0.149	0.109	0.100	111.0			0.171		0.101	0.112	0,101	0.093	0.156	0.110	0.101	0.100	0.107	671 O	0.152	0.115	0.087	0.213	0. 141	0.052	100.0	250.0	0, 123	0.035	0.110	0.2.0	0.166	0.175	0,143	0.176
ē:	Ē	Ē	Ŧ	ž	Ē	Ž	Ş	Ŧ	룿	ł	3	3	3	3	3	\$ i	\$ į	2 3	3	\$ 3	\$ }	\$ 3	3	3	3	3	5	2	3	3	3	3 !	3 !	\$ 3	:3	3	3	3	\$ !	\$ 3	\$	3	\$ 1	\$ }	\$ 3	\$ 3	\$ 3	5	: 2	3
200330	201390	896660	42306	268870	159790	35389	111580	94485	56219	1042200	304190	405050	418600	64641	96067	114230	192220	90697	12/4000	15016	105501	46461	00111	01/76	1150F	00200	91991	68401	148110	324470	23476	47977	18900	09055	66889	26700	13461	125580	75214	55872	15937	37648	092622	751790	050011	056211	12250		20403	67105
14	. 73	7.01	7.25	7.40	7.63	8.06	8.23	8.44	6.89	9.11	9.34	9.85	0.07	0.33	0.39	0.58	0.81	2	97.14	1.75	42.25	42°24	42.84	46.74			07.04 71.06	£4.23	44.47	44.75	44.96	45.21	45.59	45.98 44	46.33	46.51	46.69	46.91	47.22	47.44	47.59	47.65	47.79	48.12		48.75	60.03	47.02	19 67	50.07

T al	ь1.	•	44
	•••	-	_

					17.58	10989	BV	0.080	0.013
5 1	ng Chlorine	dos	3 <b>e</b>		17.72	47349	VV	0.096	0.056
					17.87	20249	vv	0.065	0.024
					17.97	114940	٧V	0.099	0.136
RUN # 783.	•	A1	PR/29/86 ,	22:01:39	16.17	46803	W	0.214	0.055
WORKFILE II	D: C		, WORKFIL	E NAME:	18.73	42731	VP	0.129	0.050
1D: 000					19.17	55122	PV	0.130	0.065
AREAS					19.21	22096 1	VV C	0.054	0.026
RT	AREA TY	PE	AR/HT	AREAS	19.39	119580	vv	0.098	0.141
checkpoint	: next peak	18	A1; RT is	off because	19.68	113110	W	0.182	0.113
peak is bro	bed.				20.20	21461	vv	0.150	0.025
5.55	3290700	BV	0.145	3.880	21.00	17037	vv	0.085	0.020
5.81	126620	vv	0.093	0.149	21.19	14790	VP	0.090	0.017
5.97	58658	VB	0.094	0.069	21.56	13102	vv	0.112	0.016
6.65	3666300	BV	0.174	4.323	21.82	36065	vv	0.168	0.043
7.07	315880	VV	0.177	0.372	22.10	71980	vv	0.136	0.085
7.27	366760	VP	0.182	0.432	22.49	28953	W	0.104	0.034
7.67	64857	PV	0.089	0.077	22.65	63568	vv	0.112	0.075
7.94 2.	0632E+07	vv	0.187	24.327	22.62	16533	VV	0.176	0.020
8.11 1.	6152E+07	vv	0.186	19.044	23.70	19778	BV	0.077	0.023
8.36	9807500	VB	0.220	11.564	23.82	36501	VV	0.129	0.043
9.26	17521	BP	0.087	0.021	24.06	17436	vv	0.073	0.021
9.53	14883	٧P	0.094	0.018	24.17	39690	vv	0.086	0.047
9.87	188600	PV	0.158	0.222	24.38	26583	٧V	0.097	0.031
10.21	490980	W	0.171	0.579	24.73	51616	٧P	0.140	0.061
10.41	289250	vv	0.165	0.341	25.20	68215	PV	0.136	0.080
10.72	916350	vv	0.114	1.080	checkpoint:	next per	k is	A25; sub	tract 0.01 minute
10.88	761590	vv	0.128	0.898	25.42	77738	.VV	0.133	0.092
11.13	395360	vv	0.150	0.466	25.62	76970	vv	0.119	0.091
11.37	162140	VP	0.124	0.191	26.06	53703	VP	0.091	0.063
11.98	103310	VP	0.199	0.122	27.01	36791	W	0.120	0.043
12.32	17876	PP	0.106	0.021	27.23	27858	vv	0.174	0.033
12.61	83931	PV	0.167	0.099	27.62	23178	VP	0.140	0.027
12.76	12692	vv	0.065	0.015	27.93	74043	PV	0.106	0.087
12.95	77467	PV	0.086	0.091	28.09	23859	٧V	0.096	0.028
13.16	14728	W	0.077	0.017	28.22	59953	vv	0.139	0.071
checkpoint	: next peal	t 15	Al4 subt	ract 0.02 minutes	28.44	38208	vv	0.104	0.045
13.39	3966600	VB	0.115	4.677	28.89	24998	BV	0.091	0.030
13.87	45216	BV	0.152	0.053	29.14	47077	VV.	0.152	0.056
14.08	1408Z	vv	0.052	0.017	29.58	12469	VP	0.083	0.015
14.12	13577	vv	0.039	0.016	29.66	24442	PV	0.111	0.029
14.23	9/211	vv	0.141	0.115	29.98	23796	VP	0.078	0.028
14.36	58977	vv	0.0//	0.070	30.62	48196	PH	0.096	0.057
14.62	664250		0.231	0.783	30.88	24774	HOH	0.145	0.029
14.85	587750	vv	0.214	0.693	31.11	25651	ю	0.134	0.030
15.02	228030 D	vv	0.099	0.269	31.28	165230	HV	0.106	0.195
15.24	062640	VV	0.13/	1.01/	31.43	63619	VV	0.112	0.075
15.35	847720	VV.	0.175	1.000	31.61	14877	VV	0.081	0.018
checkpoint	:: next peal	K 11	AI/; SUD	Tract U.UZ minutes	31.77	36327	VV	0.103	0.043
15.73	1721100	vv	0.195	2.029	31.89	21115	vv	0.079	0.025
16.11	1113700	VP	0.187	1.313	32.04	23668	VV	0.121	0.028
16.76	19291	PV	0.059	0.023	32.21	21722	VV	0.084	0.026
16.94	Z594700	VB	0.117	3.059	32.32	36368	vv	0.101	0.043
					32.64	73580	٧V	0.183	0.087

				0.026	0.104	2	22125	74.59			-		
				0.028	0.110	Ş	23696	71.49	0.036	0.080	Ş	30265	46.35
				0.053	0.079	Ş	45114	70.66	0.033	0.098	Ş	27859	46.00
				0.045	0.068	Ş	38330	70.61	0.025	0.134	2	21176	45.86
				0.160	0.222	Ş	136060	70.49	0.041	0.112	Ş	36494	45.22
				0.046	0.182	Ş	38805	69.57	0.036	0.138	Ş	30706	44.98
				0.059	0.252	Ş	50402	68.67	0.115	0.153	Ş	97354	64.75
				0.028	0.132	Ş	23763	68.30	0.134	0.137	Ş	113340	44.46
				0.035	0.184	Ş	29484	67.16	0.017	0.114	٧Þ	14532	43,99
				0.014	0.101	¥	12040	67.07	0.045	0.138	Ş	38242	43.78
				0.075	0.169	5	63818	65.60	0.094	0.114	Ş	79639	43.52
				0.032	0.201	ł	27016	63.40	0.089	0.100	Ş	75607	43.39
				0.029	0.164	Ş	24880	62.79	0.297	0.138	Ş	252160	43.03
				0.037	0.222	¥	31426	61.83	10.04	d10; add	* 1	t: next pe	checkpo in:
				0.099	0.182	Ş	83785	61.04	0.068	0.105	Ş	57948	42.82
				0.022	0.105	Ş	18691	60.80	0.014	0.097	٧P	12019	42.24
				0.232	0.237	Ş	196340	60.30	0.202	0.167	Ş	171280	41.78
				0.152	0.266	Ş	128590	59.27	1.936	0.149	Ş	1642100	41.45
				0.026	0.104	Ş	22321	58.80	0.095	0.112	\$	80620	41.21
				0.019	0.091	Ş	16487	58.67	0.034	0.058	Ş	28739	41.10
				0.080	0.166	Ş	67908	57.72	0.148	0.172	Ş	125870	40.83
				0.084	0.169	z	71555	56.79	0.083	0.127	Ş	70533	40.57
				0.114	0.144	٤	96742	56.30	0.105	0.118	Ş	91698	40,40
				0.113	0.207	Ş	95402	55.57	0.383	0.235	Ş	325020	40.06
				0.015	0.111	Ş	12690	54.60	0.303	0.187	Ş	257090	39.94
				0.029	0.131	Ş	24364	54.29	0.156	0.102	٤	132050	39.36
				0.020	0.118	2	17094	53.82	0.678	0.089	P	574750	39.12
				0.028	0.109	Ş	23642	\$3.39	0.013	0,098	VP	11224	38.88
				0.114	0.207	Ş	97000	53.14	0.014	0.087	Ş	12011	38.68
				0.058	0.106	Ş	48798	52.78	0.061	0.143	¥	51502	38.44
				0.196	0.213	Ş	166030	52.55	0.063	0.089	Ş	\$3664	38.25
				0.129	0.167	Ş	109690	52.26	0.020	0.100	Ş	16526	38.07
				0.112	0.164	Ş	95205	51.98	0.038	0.148	Ş	32350	37.87
				0.077	0.110	Ş	65030	51.66	0.092	0.117	Ş	77643	37.64
				0,183	0.204	Ş	155010	51.54	0.360	0.130	Ş	305670	37.41
				0.022	0.056	Ş	18805	51.34	1.925	0.089	Ş	1632400	37.01
				0.041	0.094	\$	34445	51.12	HARCE.			t: next pe	checkpoin
				0.106	0.167	5	90167	50.93	0.148	0.078	5	125390	36.75
				0.014	0.074	٤:	15071	50.79	0,14,	0.014	٤:	73864	36.73
						5		20.17	0.0/0	0.094	53	01040	36.95
				0.071	951.0	2	95465	50.09	0.036	0.065		12206	30.10
				0.045	0.128	2	38522	49.64	0.075	0.122	1	63517	36.09
				0.185	0.183	2	156950	49.03	0.022	0.075	Ş	18442	35.95
	Ş	A= 8.4812E+	TOTAL ARE	0.050	0.143	۶	£ 1993	48.74	0.022	0.090	Ş	18514	35.84
0.530	, M	355830 1	87.08	0.103	0.122	٧P	87268	48.36	0.020	0.103	Ş	16542	35.73
0.183	Ş	24535	85.24	0.050	0.143	Ş	42723	48.03	0.022	0.148	Ş	18472	35.50
0.132	2	14135	85.19	0.108	0.142	Ş	91139	47.80	0.036	0.101	Ş	30657	35.31
670.0	\$	13774	83.24	0.060	0.095	Ş	50421	67.64	0.033	0.093	Ş	27779	34.93
0 104	\$	26080	83.20	0.031	0.059	Ş	26288	47.54	0.065	0.078	Ş	54733	34.81
0.122	\$	28000	83.09	0.044	0.095	Ş	37395	47.48	0.118	0.178	Ş	100310	34.26
0.468	Z	331840	79.71	0.074	0.115	Ş	63012	47.21	0.027	0.090	PV	23098	33.47
0.091	\$:	48674	77.43	0.016	0.082	Ş	13880	46.84	0.019	0.077	٧P	16086	33.29
0.093	Ş	45926	77.37	0.025	0.105	Ş	21160	46.69	0.222	0,096	Ş	187950	33.10
									0.070	0.112	Ş	59109	32.92

0.057 0.057 0.033 0.031 0.031 0.016 0.017 0.029

## Table A5

## 10 mg Chlorine dose

RUN # 7	78,	AP	R/29/86 ,	13:04:45
WORKFILE	; 1D: C		, WORKFII	E NAME:
1D: 000				
AREAS				
RT	AREA '	түре	AR/HT	AREAL
5.49	1400800	BP	0.141	1.700
5.76	102740	PV	0.086	0.125
5.93	284030	٧P	0.160	0.345
checkpoi	int: next pe	ak is	A2; add (	.03 minutes
6.60	5161200	PV	0.189	6.264
7.00	404650	vv	0.162	0.491
7.19	464480	VP	0.190	0.564
7.60	158980	PV	0.092	0.193
7.83	1.9016E+07	vv	0.193	23.077
8.04	1.3754E+07	vv	0.177	16.692
8.29	1.1580E+07	VB	0.234	14.054
9.21	18242	BP	0.088	0.022
9.43	20326	PP	0.127	0.025
9.80	243720	PV	0.159	0.296
10.14	407290	VV	0.170	0.494
10 17	183340	vv	0.159	0.223
10 65	751570	vv	0.110	0.912
10 82	1638900	VV	0.127	1.989
11 04	351840	vv	0.152	0.427
11 30	157670	VP	0.133	0.191
11 72	11420	vv	0.086	0.014
11 90	67603	vv	0 113	0.076
17 73	12450	VP	0 107	0.019
17 57	49677	PV.	0 119	0.060
17 77	28453	vv	0 119	0.035
12.72	20433	vv	0 102	0.083
12.00	16068	vv	0.089	0.045
13.00	10708		A14 add	
13 33	10C. BUXC P	VR. IS	0 177	4 975
13.32	4030000	80	0.127	0.029
15.79	42713	vv	0.127	0.027
14.15	92313	100	0.130	0.031
14.42	/3/73	100	0.125	0.090
14.30	000.000	10/	0.1/8	0.443
14.61	535000		0.200	0.047
15.10	9/0830		0.122	1.100
15.27	765990		0.150	0.930
15.65	842150	~~	0.149	1.022
15.80	389370	VV	0.145	0.4/3
16.02	622750	vv	0.171	0.756
checkpo	int: next pe	bak is	A18; add	0.05 minutes
16.87	3844200	PB	0,131	4.665
17.64	19518	PV	0.083	0.024
17.78	14567	vv	0.064	0.018
17.89	66424	VP	0.080	0.081
18.63	12580	vv	0.089	0.015

19.06	46462	PV	0.121	0.054
19.31	99212	vv	0.108	0.030
19.59	139620	vv	0 184	0.120
20.14	17006	Ŵ	0 079	0.021
20.91	17433	vv	0 089	0.021
21.51	11203	PV	0 114	0.021
21.73	41496	vv	0.110	0.014
22.02	106120	va	0.130	0.050
22.41	18328		0.070	0.129
22.57	30211	10	0.077	0.022
23.01	13574	VD	0.070	0.037
23 30	72108	04	0.080	0.016
23 62	18984	1110	0.150	0.027
23 74	23487	101 101	0.090	0.023
23.00	12057		0.110	0.029
25.70	12032		0.0/8	0.016
24.03	10010	7.7	0.11/	0.080
24.31	19822	NN NN	0.084	0.024
24.41	14031	77	0.064	0.018
29.03	50929	72	0.150	0.062
23.12	/1942	PN	0.140	0.087
CRECKPOINT:	next pe	8K 18	AZS; add	0.07 minutes
23.34	10/360	701	0.147	0.130
23.33	99432		0.134	0.121
23.01	103//	PLM All M	0.084	0.020
43.70 24 31	126300	NN	0.114	0.153
20.71	23981	MM	0.129	0.029
20.00	18106	904	0.065	0.022
20.73	03526	1111	0.146	0.077
27.19	2/518	NON	0.091	0.033
27.40	83094	HM	0.235	0.103
27.04	152920	MIN	0.136	0.186
28.00	4/030	MH	0.102	0.058
20.10	75325	NN	0.178	0.116
20.33	47880	HH	0.116	0.061
20.48	43525	HIN	0.131	0.053
26.61	38990	MH	0.102	0.047
28.91	26008	ЮН	0.080	0.032
29.08	8030Z	MON	0.222	0.098
29.77	46956	KOK	0.129	0.057
29.89	35304	RCH	0.107	0.043
30.34	73211	HV	0.109	0.089
30.80	17246	vv	0.115	0.021
30.89	12304	vv	0.086	0.015
31.00	19523	vv	0.103	0.024
31.18	150180	Ŵ	0.118	0.182
31.34	66433	W	0.126	0.081
31.52	15075	vv	0.078	0.018
31.67	55879	٧V	0.123	0.068
31.81	26584	vv	0.085	0.032
31.93	40829	vv	0.144	0.050
32.14	23112	٧V	0.099	0.028
32.23	36049	vv	0.098	0.044
32.61	63611	vv	0.177	0.077
32.83	58892	vv	0.125	0.072

400.0	0.000	0,043	0.037	0.035	0.035	0.017	0.216	0.013	0.01	0.019	0.068	0.057	0.025	0.015																																			
		0.118	0.070	0.065	0. 143	0.060	0.457	0.189	0.089	0.053	0.115	0.079	0,040	0.177																																			
3	: 3	: 3	:3	3	3	3	2	3	3	3	2	3	3	3	0	8																																	
			980	0 5561	121	1795	0110	9658	5577	5566	4609	6675	0 9710	2822	2402E+	+30000																																	
;	57				7		171	Ξ	-	-	ñ	4	Ñ	-	-																																		
!	22	ç ş	8 ×		1	1	63	2	3			5	19		TAL AR	FACT																																	
1					4				2						Ē	2																																	
790 0	0.022	0.036	0.081	0.057	0.070	0.069	0.042	0.304	0.150	0.091	0.088	0.041	0.018	0.093	0.017	0.056	0.098	0.039	0.072					0.049	0.025	0.053	0.107	0.019	0.089	0.020	0.111		0.020	0.015	0.015	0.024			0.051	0.039	0.038	0.014	0.019	0.041	0.067	6 G	C 16	090.0	,,,,,
																																								Ť			Ť		-				
80.0	0.074	0.083	0.149	0.120	0.158	0.172	0.132	0.159	0.115	0.184	0.197	0.143	0.091	0.176	0.059	0.126	0.211	0.103	0. 129				0.128	0.140	0.129	0.180	0.220	0.108	0.176	0.117	0.149		0.170	0.130	0.107	0.140	101.0		0.104	0.071	0.077	0.034	0.047	0.104	0.172	0.120 0.120	0.157	0, 129	
3	3	3	3	3	3	3	\$	\$	Z	5	5	\$	\$	\$	3	3	3	A .	<b>-</b> i	2 3	: 3	: 3	: 3	5	3	3	\$	3	4	\$	Z i	\$ 3	: 2	3	Z	•	23	:3	:3	3	3	3	3	5	2	2 3	23	: 2	
050	817	681	424	864	611	612	422	820	0/61	786	243	1579	.857	683	1698	. 70	964	603	0/2			1	275	000	1280	14.22	.953	1221	683	133	5	200	029	950	656	082			845	768	022	Q [ 79	176	Q 866	3	89	202	863	,,,,
5	-	2	š	¥	5	ž	2	<b>3</b> 2	21	2		8	7	ž	-		2	F 1						9	20	4		5	2				2	Ξ	Ξ	Z	3		1	5	5	=	5	8	5	75	158	5	
H.	52	10.	. 50	69	5	2	59	46	21	6	. 24	· 52	<b>9</b>	82	6	5	<b>9</b>	2:	Ţ	5	: =		2	45	. 14	.37	63	2	5	02	= :	66	=	94	5	6	2		5	1	44	50	24	5	2:	2	58		
14	14	13	13	47	1	8	7	9		5	20	5	8	2	2	5	23	2:	2:	25	13	1	3	ŝ	56	26	\$	5	5	5		3	62	62	3		61	5	5	5	6)	61	6	5	5	2 2	: =	2	
5			:	32	5	42	11	2	53	<u>.</u>	21	62	22	5	•	5	69	nutes	5:	23	53		2	2	37	¢3	79	8	17	<b>;</b>	22	•		80	16	2	2;		2 2		53	6	27	5	<u>8</u> :	2 1	:5	2 8	4
6 0	0.0	0.0	0.0	0.0	0.1	0.0	0.0	0	0.0	0	0.0	0.0	0.0	0.1	0.0	0.1	0.7	18 18 19						0.0	0.0	0.3	0.1	0	0.2	0	00			0.1	0.0	0.0				0.0	0	0.0	0	0.0	00		50	) = ) 0	
60	18	96	88	19	62	22	86	8	86	20	81	16	<b>9</b> 9	68	8	66	2	o ppe	E	65			5	62	92	96	23	96	2	6	88	5 5	65	10	:	5	2 2	86	91	89	83	5	47	5	21		23	; =	
0.0	0	0.0	0	0.0	0	5	0		0.0	0	0.0	0.0	•	0	5	0	5	6	0	5				0	0.0	0.0	0	0.0	0	0	0 0	5 6	50	0	0.0	0	5 6			0	0.1	0	0.1	5	0	> c > c	,	50	
3	\$	2	3	3	3	3	\$	\$	\$1	3	3	3	3	3	3	3	3		\$ į	3	: 3	3	3	3	3	2	3	3	3	3	\$ 9		3	3	٩Y	5	\$ 3	: 3	3	3	2	3	3	3	2	\$ 3	: 3	: 3	: [
211490	27459	14696	11056	26578	03541	34,353	58361	24644	18685	15476	16949	50946	16337	118070	65092	160760	221600	next pe	0008/6	041116	120620		42860	29522	30780	287410	147690	82188	178560	52218	20224	97956	598000	88847	12984	67681		15875	874.33	30877	106460	13408	22334	35593	24357	19779	44037	84171	
																		int:	1							. ,							-					-											
5	2	6	28	8	5	5	2	2	22	9	Ş	14	3	:	2	3	\$.		2 :	2 2	: :	1	5	5	8	5	2	2		F :	5:	2 =	1		2	3	2 2		3	:	8	2	2	2	5 ?	2 2	: 2	2	. :

	Table A	6				18.16	10937	PP	0.101	0.020
		•				18.76	17644	VP	0.123	0.032
	20 mm chlori	ne do				19.38	29477	VV .	0.078	0.053
•			46			19.47	16318	VV	0.085	0.030
RIN # 71	84	AD	D/30/86	10.36.08		19.66	90131	VV .	0.200	0.163
MORKETLE	1D· C	ALC 1	UNPVET:	10.30.00		19.99	22856	vv	0.100	0.041
	10. 0		, WORKFI			21.26	12582	VP	0.094	0.023
APFAT						21.57	10549	VV	0.106	0.019
87	APEA T	VDF	AD /NT	ADEAT		21.80	26526	VV	0.141	0.048
checknois		155 6 1 6 1	AN/AL	ARCA&		22.09	163490	vv	0.094	0.296
5 51	762690	89	0 144	1 781	windres.	22.46	25331	vv	0.116	0.046
5.78	84239	PV	0.083	0 153		22.63	27319	vv	0.117	0.050
5 95	139930	VP	0 179	0 616		23.38	21448	BP	0.117	0.039
6 61	29 30600	PV	0 170	5 306		23.88	28413	vv	0.211	0.052
7.03	285 190	vv	0 162	0 517		24.04	12877	VV	0.078	0.023
7.22	401830	VP	0 188	0.728		24.15	36484	vv	0.089	0.066
7.62	166590	PV	0.097	0 102		24.48	11707	vv	0.095	0.021
7.88	1 1286E+02	Ŵ	0 195	20 4 14		24.71	58423	VP	0.153	0.106
8.08	9329100	vv	0 167	16 892		25.19	55826	PV	0.145	0.101
A. 33	9046700	VB	0 220	16 380		25.41	81617	vv	0.145	0.148
9.27	19209	RV	0 128	0 071		25.60	70167	W	0.113	0.127
9.47	26083	VP	0.135	0.047		26.05	110370	W	0.105	0.200
9.83	199780	PV	0 169	0.362		26.42	13765	WV .	0.105	0.025
10.17	125180	vv	0.147	0.227		27.00	25941	vv	0.128	0.047
10.38	71565	vv	0.125	0.130		27.91	58219	PV	0.094	0.105
10.69	471920	vv	0 117	0.855		28.25	17936	BV	0.100	0.033
10.85	416380	vv	0 121	0.754		29.16	45883	vv	0.180	0.083
11.09	176310	vv	0.149	0 119		29.86	33736	PV	0.119	0.061
11.35	91752	VP	0.125	0.166		30.20	18935	vv	0.155	0.034
11.94	69284	VP	0.178	0.126		30.62	46953	PV	0.105	0.085
12.28	25243	PP	0.099	0.046		31.25	45294	PV	0.108	0.082
12.49	59492	PP	0.117	0.108		31.42	33187	VV	0.168	0.060
12.77	43361	PV	0.098	0.079		31.75	32134	vv	0.104	0.058
12.93	31105	VP	0.058	0.056		31.68	12277	vv	0.079	0.022
13.12	11998	PV	0.080	0.022		32.01	40067	W	0.123	0.073
checkpois	nt: the next	peak	1s A14:	subtract	0.01 minute	32.31	54871	vv	0.190	0.099
13.38	2144600	VB .	0.116	3.883		32.69	40020	vv	0.167	0.073
13.83	24784	BP	0.150	0.045		32.91	38747	VV.	0.122	0.070
14.24	30493	PV	0.148	0.055		33.09	44488	VV.	0.121	0.081
14.46	66708	vv	0.146	0.121		33.27	21548	VP	0.075	0.039
14.61	268590	vv	0.176	0.486		34.12	28324	FV	0.098	0.051
14.82	259690	vv	0.177	0.470		34.30	523/6	VV.	0.184	0.095
15.01	66004	vv	0.062	0.120		34.43	1//6/	VV.	0.089	0.032
15.22	1117400	vv	0.114	2.023		35.29	10338	PV	0.120	0.030
15.32	706400	vv	0.126	1.279		33.48	10327	VV.	0.125	0.019
15.71	\$97000	vv	0.131	1.061		35.72	10161	VV.	0.0/1	0.018
15.86	249370	vv	0.125	0.452		33.81	822/1	VV.	0.099	0.149
16.08	210740	VP	0.128	0.382		36.07	52532	VP	0.139	0.095
checkpoir	nt: the next	peak	is A18;	add 0.01	winute	36.37	14133	PV	0.075	U.026
16.92	5625700	PB	0.200	10.186		30.48	111860	VV VD	U.080	0.203
17.57	16660	BV	0.064	0.030		36.72	110730	VP .	0.113	U.201
17.68	16653	vv	0.084	0.030		cneckpoint:	the next	peak	18 D3; #dd	U.01 minute
17.85	29600	vv	0.073	0.054		37.00	1001000	r 8	0.105	2.900
17.94	23896	VP	0.075	0.043		37.40	101240	BV.	U.11Z	U.184

57.69	56.76	56.51	55.57	54.26	53.75	53.38	53.12	52.51	52.23	51.73	51.64	51.54	50,90	50.31	50,07	49.64	69.36	10 01	48 12	1	47.62	47.35	47.19	46.56	46.35	46.14	46.05	45.24	44.74	44.43	43.74	43.50	43.01	42.87	42.76	42.56	41.77	41.10	41.08	40,81	40.56	40.39	40.14	39.85	39.33	39.10		38.66
5004.3 PV	38306 VV	17358 VV	37277 PP	42971 W	115000 VV	67140 VV	102810 VV	199760 VV	AA 60697	50294 VV	11441 W	V8 08109	25296 VV	31101 W	AA 56907	55704 PV	44 95691	AA 70000	AA 16100	28263 VV	78636 W	18431 W	40023 PV	12022 W	30255 W	24370 W	27926 VV	20547 W	24353 VV	61591 VV	43178 W	AN C1706	VA 265255	29834 VV	36518 W	26009 VV	210207 VV		13668 W	AA 69150	14230 W	25229 W	29224 VV	55613 BV	49454 VV	127150 PV		AA 6(1)L
0.188	0.156	0.118	0.210	0.211	0.200	0.175	0.182	0.293	0.139	0.138	0.037	0.146	0.135	0.158	0.157	0.070			0.158	0.127	0.183	0.092	0.102	0.096	0.150	0.129	0.090	0.141	0.146	0.174	0.144		0.155	0.101	0.120	0.097		0.119	0.092	0.122	0.081	0.094	0.155	0.169	0.090	0.094	0.000	
0	0	0	0	0	0	0	0	0	0	-	•	•	0	0	0	<b>-</b>	- e	, e	• •		0	0	0	•	•	0		0	0	<u>•</u>	0	e e	• •	0	0	0	<b>-</b> -	• e		. <b>0</b>	0	0	0	<u>.</u>	<u>,</u>	0	e	•

HUL FACTOR	92.19	91.94	86.87	86.76	85.16	83.09	80.78	80.68	80.59	79.50	77.38	71.95	71.77	70.42	69.51	68.26	67.07	65.55	61.03	00.20
1.0000E+00	19782 W	10157 W	37201 W	164.88 VV	10888 PV	29365 BV	25064 W	22208 W	35799 VV	41915 W	50070 PV	17900 W	13210 W	42752 VP	14282 VV	14352 PV	AA 50%	30761 W	20589 BP	11 20105
	0.155	0.126	0.238	0.125	0.165	0.237	0.122	0.101	0.187	0.399	0.220	0.121	0.121	0.305	0.164	0.209	0.224	0.192	0.155	
	0.030	0.010	0.067	0.000	0.020	0.053	0.045	0.040	0.065	0.112	0.091	0.032	0.024	0.077	0.026	0.026	0.035	0.056	0.037	

	Table A	7			
					17.
	40 mg chlo	rine	dose		17
			120104	16. 37. 19	18
RUN # 787		APR	UOP/00	10:37:12	18
WORKFILE I	D: C		, WURKPI	LE NATE:	19
10:000					19
AREAL	AREA TO	795		AREAL	19
K I	449780	87	0 148	0.861	19
3.33	123200	PV	0.086	0.159	19
5.82	875890	VP	0.228	1.062	20
	· the next	neek	is A2:	subtract 0.03 minutes	20
4 66	3491800	PV	0.176	4.488	20
7 07	369730	VV	0.167	0.475	21
7.25	465820	VP	0.175	0.599	21
7.66	232150	PV	0.095	0.298	21
7.89	7276700	vv	0.097	9.354	21
7.92	8714600 D	vv	0.119	11.202	22
8.09	9736400	vv	0.178	12.515	22
8.36	9950400	VB	0.219	12.790	22
9.26	19888	BP	0.108	0.026	22
9.53	29757	PV	0.122	0.038	23
9.87	280020	PV	0.166	0.360	23
10.21	84714	vv	0.153	0.109	23
10.41	93411	vv	0.132	0.120	24
10.72	639910	vv	0.112	0.625	24
10.87	418490	vv	0.111	0.336	26
11.12	1/3990	VV 1/D	0.137	0.309	24
11.37	240340	WP DNJ	0.117	0.076	25
11.85	116360	V10	0 187	0.150	25
11.90	25128	PV	0 100	0.032	25
12.27	37122	vv	0.119	0.048	25
12.33	200520	vv	0.158	0.258	26
12.75	167560	vv	0.131	0.215	26
checknoin	t: the next	t Deal	t is Al4	6; subtract 0.01 minute	26
13.38	2878100	vv	0.150	3.700	27
13.72	214970	vv	0.139	0.276	27
13.82	67398	vv	0.047	0.087	27
14.05	75590	vv	0.060	0.097	27
14.25	241080	vv	0.164	0.310	27
14.33	71893	vv	0.049	0.092	27
14.47	253230	vv	0.132	0.326	2/
14.62	619470	vv	0.192	0.796	20
14.84	1025500	vv	0.277	1.318	20
15.22	1750700	vv	0.119	2.250	20
15.33	1903200	VV.	0.155	2.440	20
15.72	761790	VV.	0.173	0.9/9	20
15.86	681640	VV	0.162	U.6/D	20
16.11	902530	٧P	0.258	, itou	29
checkpoi	nt: the nex	t pea	IK 18 ÅI	6 144	29
16.92	7113500	10	0.143	0.014	20
17.57	10869	BP	U. US4	V.VI*	

	18494	ther	0.081	A A3F
17.71	17020	PV	0.081	0.025
17.85	121360	vv	0.079	0.156
17.94	49449	vv	0.067	0.064
18.15	16932	PV	0.099	0.022
18.74	44929	VP	0.176	0.058
19.14	26574	vv	0.106	0.034
19.28	55957	VV	0.092	0.072
19.38	70576	vv	0.085	0.091
19.48	41940	vv	0.090	0.054
19.67	264330	VV	0.229	0.314
20.00	80829	vv	0.137	0.104
20 29	110120	vv	0.146	0.142
20 97	33989	vv	0.142	0.044
21 18	18 186	VV	0 075	0 024
21 25	17155	VP	0 107	0 042
21 56	16215	-	0.098	0.018
21.50	63301	PU	0.091	0.081
22.01	400330	va	0.087	0 515
22.00	21120	24	0.087	0.017
22.47	27720	MID	0.072	0.017
22.03	2/01/	80	0.097	0.033
22.71	24003		0.003	0.031
23.09	11/85	77	0.074	0.015
23.36	39020	TT NR	0.120	0.030
23.90	28/43		0.147	0.076
24.15	59420	PUN .	0.084	0.076
24.26	21497		0.086	0.028
24.48	10302	21.11	0.072	0.013
24.59	13251	MM	0.0/2	0.01/
24.71	65401	HP	0.161	0.084
25.19	83492	PM	0.147	0.107
25.42	155140	PCH	0.133	0.199
25.60	112010	ЖМ	0.11/	. 0.144
25.77	16685	NCH	0.069	0.022
26.05	185310	HH	0.134	0.238
26.42	70662	MM	0.194	0.091
26.78	104130	NON	0.104	0.134
27.00	82979	HON	0.143	0.107
27.22	29414	ю	0.076	0.038
27.28	43675	ю	0.100	0.056
27.40	44281	ЮM	0.101	0.057
27.56	73265	ЮH	0.143	0.094
27.73	79494	NH	0.113	0.102
27.91	224330	ЮH	0.121	0.288
28.12	81466	HH	0.122	0.105
28.23	105990	HCH	0.125	0.136
28.37	80295	HV	0.136	0.103
28.56	24476	vv	0.096	0.032
28.68	23350	VV	0.106	0.030
28.87	27603	vv	0.123	0.036
29.16	107250	vv	0.130	0.138
29.41	30861	vv	0.139	0.040
29.85	61020	vv	0.104	0.078
29.96	24882	vv	0.078	0.032
30.15	11946	vv	0.101	0.015
		••		

0 033	0.024	0 076	0.056	0.070	0.049	0.051	0.026	0.014	0.076	0.101																																								
0.305	0.269	0, 102	0.063	0.184	0.135	0.317	0.116	0.055	0.162	0. 188																																								
5	3	2	3	2	\$	5	3	3	\$	5	5 5	2																																						
20614	18886	59140	43812	54314	37940	39655	19868	10732	56931	75700																																								
73.98	76.42	77.30	77.36	83.06	83. 18	85.15	95. IZ	95. 17 22 22	06.06	73.96 Tital ABEA.	MIT. FACTOR																																							
0.046	0.077	0.051	0.369	0.077	0.118	0.025	0.033	0.050	0.034	0.059	0.036	0.06/	0.027	0.021	0.062	0.059	0.081	0.051	0.287	0.029	0.201	0.099	0.025	0.054	0.052	0.041	0.146	0.106	0.092	0.071	0.035	0.022	40.0	0.043	0.017	0.058	0.020	0.066	0.173	0.087	0.038	0.018	0.094	0.017	0.075	0.033	0.013	0.026	0.019	0.019 0.016
0.100	0.117	0.081	0.137	0.103	0.124	0.095	0.107	0.136	0.118	0.117	0.128	0.004	0, 122	0.088	0.094	0.125	0.155	0.136	0.131	0.092	0.101	0. 19Z	0.064	0.136	0.124	0.089	0. 192	0.159	0.153	0.135	0.111	0.129	0.160	0.124	0.070	0.172	0.129	0.166	0.263	0.159	0.168	0.159	0.161	0.118	0.200	0.099	0.146	0.109	0.068	0.056
3	3	3	3	3	3	⋧	3	3	3	<b>3</b> i	5 3	23	3	3	2	3	3	2	3	\$ i	2 i	2	3	\$	3	3	3	3	3	5	2 !	5	: 5	2	2	3	5	44	3	3	2	2	2	2	4	2	2	3	\$ 3	\$ \$
35842	60148	39972	287030	59567	91625	19624	25462	38776	26482	45576	28203	22158	21059	16500	48247	46111	63209	39856	223360	222378	155990	1050	19669	41910	40104	10916	113600	82781	20017	55232	26901	16940	16458	33142	13420	45197	15405	51291	134570	67869	29250	13587	21167	13429	58436	25981	10293	20049	14953	14819
42.55	42.75	42.88	42.99	43.37	43.48	43.77	43.84	07.74	44.66	10° 11	47. 14 41. 14	10 ST	46.15	46.34	47.19	47.40	47.62	48.72	49.02	00.04	49.63	10.00	50.22	50.28	50.91	51.52	51.73	52.22	52.51	53.12	53.38	22.72		55.57	56.48	56.76	57.29	57.68	60, 27	61.01	62.56	64.17	65.56	68.21	69.51	70.36	71.15	71.36	71.64	71.44
0.023	0.338	0.041	0.035	0.116	9.134	0.018	0.212	0.039	0.242	0.043	0.003	0.117	0.099	0.157	0.052	0.027	0.068	0.115	0.034	0.025	0.038	0.021	0.037	0.031	0.234	0.192	0.086	0.191	0.324	dd 0.02 sinutes	3.074	0.059	101.0	0.053	0.026	0.016	0.058	0.249	0.149	0.180	0.043	0.015	0.051	0.040	0.036	0.034	0.089	2.167	0.221	0.015
0.111	0.100	0.094	0.098	0.121	0.144	0.050	0.110	0.076	0.112	0.090	0.089	0 190	0.130	0.105	0.074	0.098	0.096	0.181	0.095	0.111	0.115	COI . D	0.129	0.073	0.090	0.149	0.113	0.100	0.123	: is D3; e	060.0	0.000	0.127	0.092	060.0	0.123	0.079	0.109	0.111	0.149	0.099	0.087	0.099	0.104	0.112	0.098	0.107	0.153	0.175	0.120
3	3	3	3	3	3	3	3	3	3	3	\$ 3	: 3	3	3	47	3	3	3	3	\$ i	3 i	Z	3	3	3	3	3	3	3	a di	3	3	: 3	3	3	3	2	3	3	3	3	3	3	\$	٩ ۲	2	3	3	5	\$3
17843	262730	31871	27101	96668	103890	13696	164970	29920	167930	19160	11111	91176	77345	122250	40482	20888	52934	89506	26732	14/61	29512	16230	28736	23974	181710	149560	66824	148850	251950	: the next	0021662	46022	07/C17	10014	19849	13689	45256	193420	115520	139840	33244	11958	39611	30826	27940	26434	69192	1685600	1/2000	11385
30.29	30.63	30.87	30.97	31.25	31.39	31.60	31.69	31.67	31.99	32.23	05.20	32.40	32.90	33.09	33.27	33.67	34.11	34.24	34.44	34.60	34.91 25 20	35.20	35.49	35.71	35.82	36.06	36.37	36.47	36.71	checkpoint	36.99	37.23		38.08	38.23	38.34	38.65	39.10	39.32	39.63	40.14	40.28	40.39	40.55	40.80	41.05	41.19	41.38	41.74	42.21

	1401	W NO			26.89	14646	vv	0.032	0.015
	1 ee chior	ine d	~~~		26.92	21289	VV	0.043	0.021
	i wg chior	104 0	()B-E		27.18	56080	٧V	0.102	0.056
	778		DD / 18 / 84	14.57.20	27.44	26385	VV	0.075	0.026
NOBALLI	· · · · · ·	-	UNDET	19.32.37 18 NAME:	27.50	18861	VV	0.048	0.019
10.000	C 10. C		, WORKP I	LE INNUE.	28.37	23064	PV	0.078	0.023
ADE AN					29.89	40904	VP	0.119	0.041
ARCAS	AREA	TYPE		ADEAT	30.22	10339	VP	0.095	0.010
R I	ALLA	1100	AR/RI	RALAS	30.53	19138	VV	0.094	0.019
Cneckpo	1087200	19 10 BV		1 081	30.71	17926	VP	0.120	0.018
6.00	108/200	101	0.155	1.003	31.20	114330	٧V	0.106	0.114
0.71	2424/U	***	0.213	0.242	31.35	32126	VV	0.090	0.032
1.03	3.0/40270/	SFD	0.351	30.330	31.68	11101	W	0.077	0.011
10.12	197450	184	0.133	0.023	31.94	13491	VV	0.108	0.013
10.00	172430	8 V 1717	0.104	0.172	32.12	43639	VV	0.166	0.044
11.04	732370	V V 1/10-	0.117	0.747	32.54	81625	VV	0.140	0.081
11.00	233300	V P 1010	0.103	0.234	32.83	26354	VV	0.101	0.026
11.03	103/7	VB	0.150	0.017	33.01	48741	W	0.104	0.049
12.03	31/14	NP DV	0.157	0.032	33.26	17019	VV	0.094	0.017
12.00	12033	100	0.162	0.012	34.19	22336	VV	0.120	0.022
12.07	73279		C. 103	0.073	34.63	16647	VV	0.165	0.017
13 32	DIC: SWAC PC	VU	A 127		34.85	35882	VV	0.136	0.036
13.32	330540		0.147	0.220	35.23	82862	VV	0.147	0.083
14.02	£30340 \$4024	VV	0.107	0.230	35.86	39449	VV	0.119	0.039
14.02	34024	100	0.004	0.034	36.07	26348	VV	0.098	0.026
14.14	190090	171	0.170	0.107	36.30	22740	VV	0.088	0.023
14.30	314330	107	0.225	0.313	36.41	33575	VV	0.097	0.034
14.03	203570		0.191	0.203	36.65	54569	VV	0.084	0.054
15.32	204090	174	0.225	0.203	checkpoint	next peak	L 18	D3: add	0.08 minutes
12.00	439100	VV VB	0.150	0.437	36.93	999280	Ŵ	0.095	0.996
10.00	171700	• • <b>• •</b> •	U.177	V.171	37.17	42800	VV	0.102	0.043
Checkpo	Int: Next pe	PAK 13	A10; 800	V.US MINULUS	37.33	94348	VV	0.141	0.094
10.00	1400400	<b>FB</b>	0.112	1.401	37.55	97369	VV	0.137	0.097
17.07	14303	rv un	0.101	0.015	37.82	29398	VV	0.102	0.029
10.07	13712	100	0.124	0.010	37.94	92752	Ŵ	0.127	0.092
10.42	74281	F V 170	0.091	0.011	36.15	37179	VV	0.134	0.037
17.31	/0201		0.089	0.0/6	38.36	111270	VV	0.169	0.111
20.92	205/4		0.000	0.015	36.67	28769	VV	0.117	0.029
21.71	27344	DV VV	0.173	0.027	39.03	1534100	VV	0.101	1.528
22.31	19/60	10 V	0.159	0.020	39.77	381870	Ŵ	0.126	0.380
23.03	1/432	192	0.104	0.017	39.99	140170	VV	0.160	0.140
23.04	230//		0.072	0.020	40.23	30230	VV	0.067	0.030
23.70	82802		0.221	0.082	40.65	77798	vv	0.163	0.078
24.09	39133		0.089	0.039	40.75	69738	vv	0.173	0.089
24.03	53412	VP	0.112	0.053	41.00	64139	vv	0.150	0.064
25.09	612350	PV	0.107	0.610	41.26 1.	8362E+07	SHP	0.176	18.292
25.32	2080600	VV	0.138	5.001	42.69	35094	TPV	200.0	0 035
25.81	104220	U VV	0.079	0.104	42 79	50307	TVV	0 109	0.050
26.16	118390	VV	0.146	0.118	42 97	271270	TVP	0 114	0 220
26.31	69894	vv	0.104	0.070	41 26	24494	TPV	0.074	0.024
26.40	60895	vv	0.104	0.061	43 40	210910	100	0 174	0.014
26.64	48039	vv	0.098	0.048	43.40	177760	117	0.134	0.210
26.72	24323	DVV	0.050	0.024	43.07	141140	TVP	0.079	0.142
26.82	47109	VV	0.108	0.047	-J. 70	04770	140	0.09/	0.005

660440 BV 0.159

0.658

Table A8

;	2	2	÷	23	2		5		159	573	213	60	170	166	229	217	112	227	135	020																				•											
			0.0		5 0	5 6			0	0	0	0	o	ò	0	0	ò	o	ö	ö																															
1	<b>4</b> i	\$	3	3	\$ 3	:3	3	:3	2	2	3	2	4	2	3	3	2	3	3	3	804	<b>0</b>																													
	26962	42161	17285	13523	15675	10000		1358	56535	268280	38700	39315	00788	36225	56192	19620	123650	46709	39815	16036	1.00385	1.0000E																													
	65.38	66.70	67.18	67.24	67.29	61.39		60 JU	20.18	16.27	55 74	76.99	77.07	62.70	82.79	86.53	88.47	94.70	95.42	65.59	TUTAL AREA-	MUL FACTOR=																													
010 0			0 121	0,040	0.014	0.023	0.033	0.035	0.020	0.026	0.026	0.038	0.051	960.0	0.644	0.066	0.117	0.046	0.144	0.066	0.120	0.085	0.035	C20.0	0.014	0.056		0.172		0.083	0.062	0.148	0.281	0.060	0.144	0.166	0.056	0.046	0.024	060.0	0.016	0.040	0.055	0.044	0.030	0.011	0.021	0.058	0.030	0.011	0.012
0.117			0.122	0.111	0.125	0.091	0. 103	0.143	0.093	0.103	0.088	0.110	0. 135	0.123	0.322	0.129	0.155	0.097	0.169	0.115	0.230	0.149	0.059			111.0		0 185	0,161	0.161	0.124	0.165	0.267	0.114	0.176	0.223	0.165	11.0	0.130	0.199	0.094	0.169	0.175	0.147	0.149	0.096	0.174	0.155	0.196	0.134	Col .V
3	3	3	: 3	3	3	3	3	3	3	\$	3	3	3	\$ ;	\$ ;	\$ 3	\$	5	\$	\$	<b>\$</b> [	\$ i	23	: 3	2 3	\$ 3	: 3	: 3	3	3	3	3	3	3	3	2	2 3	: 3		3	⋧	3	3	3	2	≥	₹	4	\$	\$ 8	2
10201	45575	105200	122920	40427	13756	22824	33195	35064	19617	20217	26341	37728	21062	07/94		CC100	090/11	86/64	144460	66472	066611	/1/20	07666	70111	94761	CO/CC	15544	122860	98476	83552	62373	148590	282150	60450	144970	166460	61008	45669	24288	90717	18144	39905	\$5605	44320	29685	11125	20542	58438	29836	11978	0/411
44.77	10.44	45.13	45.23	45.50	45.72	45.90	46.05	46.28	46.50	70.04	40./4	50 . 03	60.74	17.14			40.24		40.04	48.82 10.01	49.04 10 50	05.74	10.44	00 67	40 06	50.27	50.45	50.58	50.82	50.98	51.25	51.43	51.64	51.96	52.14	52.63	51 IS	53.68	54.42	55.46	\$5.77	55.87	56.15	56.37	57.57	58.00	58.82	60.85	61.61	07.10 61.95	

	Table	A9			31.18	324180	vv	0.100	0.411
					31.33	58990	D VV	0.109	0.075
0	.5 mm chlo	rine	dose		31.67	13441	vv	0.108	0.017
-					31.96	15509	VV	0.129	0.020
RUN # 781		AF	R/29/86 .	18:26:29	32.10	38642	vv	0.167	0.049
WORKFILE I	Ď: C		WORKFIL	E NAME:	32.40	16825	vv	0.100	0.021
1D: 000			•		32.53	72507	- VV	0.148	0.092
AREAT					33.03	12052	vv	0.138	0.015
RT	AREA T	YPE	AR/HT	AREA%	33.25	14359	vv	0.095	0.018
checkpoint	: RT nearl	v ide	mtics1		33.38	10277	VP	0.085	0.013
6.60	792070	BV	0.164	1.005	34.64	10788	VV	0.145	0.014
6.90	157660	vv	0.114	0.200	34.83	23582	VB	0.089	0.030
7.03	318150 £	VB	0.247	0.404	35.24	19818	BP	0.159	0.025
7.85 4.	6985E+07	BV	0.319	59.610	35.85	20133	vv	0.091	0.026
10.13	92980	vv	0.232	0.118	35.98	23751	VP	0.133	0.030
10.35	59203	vv	0.170	0.075	36.33	13751	PV	0.081	0.018
10.66	141580	W	0.115	0.180	36.39	17031	VP	0.088	0.022
10.82	1126400	vv	0.128	1.429	30.69	73739	PV	0.125	0.094
11.05	206900	W	0.174	0.263	checkpoint	: next pe	ak is	D3; edd	0.10 minutes
11.84	35062	vv	0.131	0.045	30.91	380320	VV	0.105	0.483
12.88	16627	PV	0.099	0.021	37.10	1///1	vv	0.081	0.023
checkpoint	:: next pea	nk is	A14; add	0.04 minutes	37.34	44131	vv	0.136	0.056
13.33	389070	PV	0.116	0.494	37.34	33954	VV	0.112	0.043
13.59	53243	٧V	0.141	0.068	37.94	62//6	VV	0.109	0.080
14.14	28554	vv	0.154	0.036	30.07	03043	vv	0.116	0.083
14.40	15318	vv	0.162	0.019	36.30	531/3	~~~	0.120	0.068
14.56	67224	vv	0.173	0.085	39.03	1/902	VP	0.101	0.023
14.82	56562	vv	0.216	0.072	39.61	010890	<b>r</b> 8	0.089	1.029
15.34	15243	٧P	0.169	0.019	39 76	12090	PV .	0.064	0.015
checkpoint	t: next pe	ek is	A17; add	0.06 minutes	39.00	203010		0.100	0.334
15.65	3543100	PB	0.097	4.495	40 71	22264		0.107	0.074
16.88	642820	BB	0.114	0.816	41 30	7967300	DB	0.137	0.029
17.68	15083	87	0.111	0.019	42 79	714850	10	V. 148	10.108
18.06	13162	VP	0.124	0.017	47.93	175 120	UU UU	0.124	0.2/3
19.31	25120	BB	0.085	0.032	43.29	30344	~~~	0.110	0.159
20.48	18547	PB	0.150	0.024	43.43	89801	w	0.100	0.039
21.71	24268	<b>BV</b>	0.166	0.031	43.69	113770	vv	0.132	0.114
22.50	13764	BV.	0.158	0.018	43.90	36609	vv	0.103	0.144
23.02	13800	BV.	0.103	0.018	44.34	388410	BV.	0 170	0.047
23.62	16635	BV	0.084	0.021	44.89	28006	vv	0.1/3	0.473
23.74	33895	VV	0.129	0.043	45.22	1564 10	vu	0.187	0.030
24.09	28864	VV.	0.080	0.03/	45.50	20154	VP	0 107	0.177
24.64	33636	PV .	0.09/	0.043	45.72	15074	PV	0.102	0.020
25.08	470600	. PV	0.095	U. 39/	45.90	12758	vv	0 103	0.017
checkpoin	t: next pe	ak is	AZ5		46.05	17177	VP	0 117	0.010
25.31	4430100	V	0.12/	5.620	46.47	23927	Ŵ	0 126	0.022
26.93	10001	VV.	0.078	0.013	46.74	48997	Ŵ	0 218	0.030
27.21	43540	VV.	U. 146	0.033	46.96	12766	Ŵ	0 102	0.002
27.47	20215	VV.	0.102	0.026	47.10	15509	vv	0.102	0.010
27.56	15381	VV.	0.076	0.020	47.56	571300	vv	0 359	0.020
28.36	42285	VV	0.093	0.054	47.91	35772 1	n vv	0.091	0.723
29.86	33622	VP	0.117	0.043	48.03	65121	vv	0 114	0.043
30.24	20865	VV	0.098	0.027	48.20	17681	vv	0.114	0.003
30.50	23847	VV.	0.111	0.030		1,003	••	A. 112	U. U22

<b>N</b> 7	
Ē	
2 3	
N	
C	
_	

054	075	066	039	14	124					ŝ	5		52	025	191	167	215																																
Ö	Ö	o	ò	Ö	<b>o</b> ' (	<b>.</b> .	<b>.</b> .	- e	; c	5 0		<i>.</i>	s e	6	0	0	o																																
\$	2	3	3	2	2	2 1	2 3	3	3	53	\$ 3	3	: 3	: ≩	5	2	3	è	ş																														
44169	21370	22575	13909	103380	11226	10220				0067	8/767			26152	181680	15138	25826	7.8821E	1.0000E4																														
82.79	64.70	84.76	84.80	88.44	89.25	90.49	92.55	40.44 40		70. PC	10.44	07 20		95.56	95.59	96.32	98.50	TOTAL AREA-	MUL FACTOR=																														
					29	80	02	61	3	1	28	72	5	40	1	62	17	22			26		5	67	21	53	17	2	33			69				70	76	37	5	36	~		. 2			: A	11	59	
					0	0.0	2.0	0.0	0. 0	0.0	0.1	0	0.0	Ŏ	0	0						0	0	0.0	0.5	0.3	0.0	0			50	00		0	0	0.2	0.7		0			50	) = ; =		0	0	0.0	0.0	
<u>.</u>	2	2	22	2	; =	6	62	28	2	8	65	*	82	2		22	:::			2 2	9	3	3	8	90	3	76	8:	8	23	•	5 2	<u>6</u> 9	5	6	6	9	8	6	1	2:	<b>2</b> 7	9 <b>9</b>	. 2	2	5	16	63	,
5	5	5				0.0	0.1	5	0.1		<u>°</u>	0.2	<u>.</u>		0						5		0.2	0.1	0.3	0.2	0.	5	5		5	0			0	0.2	0.2	0.0	0	- 0	5	> c > c	; c	0		5	0.1	0.0	
23	3	: 3	2	2	3	3	₹	3	3	3	3	3	3	3	\$1	Z į	\$ j	\$ 3	: 3	2	2	2	3	\$	3	3	3	3	\$	3 5	5	23	23	2	3	M	2	8	3	5	23	2 3	: 3	: 5	2	: ≩	۶	3	
2 4	9 2	t s	. 5		1	4	5	2		=	2	0	=	= :	2 :	2		2 :	2 5	2		5	4	=	0	0	5		2 :	<u>e</u> 9	2 9	2 2	2 4	2 2	0	2	R	2	4	2 9	2 2	<u>0 %</u>	2 3	2	2		•	2	1
		1560	9761	1452	2260	2986	9708	4173	346	3230	1008	13535	5761	2021	10801	1412		967 <b>4</b>	2040	L'AL	203	2633	2613	5305	41065	27801	1329	911	213	924		21200		3790	15227	18936	61200	105370	103	2851	571	1109	8126	12329	214	2646	5621	4664	
6	* ×	5.5	2 2		28	44	ç	18	96	25	5	6	5	5		53		23		12	52	12	88	60	<b>4</b> 6	ŝ	5	6	52	<u>8</u> 2		<u>s</u> :		3	28	18	11	6	21	2	3 2	6 Z	25	22	27	: =	79	72	
į,					2	2	ġ	2	ġ	Ξ	Ξ	Ξ	ni -	2			į,	ė y		1	-			0	è	o.	÷	2		ri -	i.	0.4	2			ė	è	~	é,	è :			-	1			N	d.	,

Table AlO		23.97	13134	<b>W</b> (	0.072	0.016
		24.09	33326	VV I	0.091	0.041
0.25 hour contact time		74 64	57403	VP I	D. 121	0.070
		25.09	198060	PV I	0.328	0.242
RUN # 777, APR/29/86	. 11: 12: 33	25 34	712030	w i	195	0 871
WORKFILE ID: C	LE NAME:	25.96	51547	w i	0 136	0.063
ID: 000		24.38	55478	vv	0 774	0.068
AREAS		20.20	14054		0.274	0.018
RT AREA TYPE AR/HT	ABEAT	20.70	14730	r v 170	0.133	0.010
CHECKPOINT: THE NEXT PEAK IS AT-	SUBTRACT O O1 MINETER	27.20	10221	17 80	0.000	0.013
5.51 877120 BB 0.090	1 047	27.33	33704	BF	0.107	0.041
6 58 3907800 BV 0 142	4 1007	27.84	12007	5.11	0.080	0.019
6.91 668980 VV 0.234	4.780	28.14	24937		0.112	0.031
7 19 345350 VV 0.234	0.010	28.37	23/61	NON	0.096	0.029
7 61 10627 109 0.071	0.423	28.48	16110	MP	0.110	0.020
7 85 7 60135407 DV 0 100	0.013	29.05	11006	PN	0.086	0.014
R 04 2 17745407 NR 0 244	32.923	29.89	22205	vv	0.094	0.027
	20.036	30.52	31165	PV	0.110	0.038
	0.491	31.18	107570	vv	0.111	0.132
10.15 215650 VV U.157	0.264	31.35	59972	vv	0.111	0.073
10.34 110520 VV 0.136	0.135	31.68	16713	vv	0.091	0.021
10.05 420660 VV 0.097	0.515	31.61	13148	VV .	0.090	0.016
10.83 3145300 VV 0.123	3.848	31.93	21746	VV .	0.120	0.027
11.04 468980 VV 0.158	0.598	32.14	48558	vv	0.218	0.059
11.77 14779 PV 0.127	0.016	32.54	76401	vv	0.169	0.094
11.91 30722 VV 0.127	0.038	32.83	29394	vv	0.105	0.036
12.01 30675 VV 0.108	0.038	33.01	49843	VV .	0.111	0.061
12.55 72814 PV 0.186	0.089	33.38	12290	PV	0.088	0.015
12.75 26925 VV 0.131	0.033	33.83	11494	VP	0.163	0.014
12.88 86419 VV 0.124	0.106	34.17	26156	PV	0.170	0.032
13.08 26963 VV 0.082	0.033	34.60	14568	VV	0.213	0.018
checkpoint: the next peak is A14;	add 0.06 minutes	34.84	22999	VV	0.078	0.028
13.31 2862200 VV 0.122	3.501	35.22	40204	PV	0.122	0.049
14.14 39374 VV 0.171	0.048	35.99	54702	VP	0.199	0.067
14.55 207470 BV 0.168	0.254	36.30	58981	PV	0.090	0.072
14.83 199390 VV 0.245	0.244	36.39	77809	VV .	0.099	0.095
15.16 167270 VV 0.133	0.205	36.64	136540	vv	0.140	0.167
15.27 221500 VV 0.180	0.271	checkpoint:	the next	peak	is D3; add	0.08 minutes
15.65 1613100 VV 0.128	1.973	36.93	1161900	vv .	0.099	1.421
16.03 424760 VP 0.193	0.520	37.17	49430	vv	0.091	0.061
checkpoint: the next peak is A18;	add 0.06 minutes	37.32	133780	VV .	0.134	0.164
16.87 2454000 PB 0.118	3.002	37.55	70630	VV	0.111	0.086
17.64 26218 VV 0.084	0.032	37 79	18916	vv	0.148	0.023
17.88 80078 VV 0.092	0.098	38 15	25629	PV	0.084	0.031
18.64 13222 BP 0.090	0.016	38 36	79735	vv	0.130	0.098
19.05 59549 PV 0.214	0.073	39.03	965730	PV	0.090	1.181
19.31 68516 VV 0.106	0 084	39 74	124950	w	0.099	0 153
19.60 28358 VV 0.183	0 035	30 76	411880	vv	0 124	0 504
19.93 11958 VV 0.095	0.015	39.70	212310	vv	0 142	0.284
20.17 17544 VP 0 135	0 022	J7.70 40 94	47430	vv	0.095	0.058
20.91 12307 VP 0 087	0.015	40.24	4/430	4 V VU	0.075	0.074
21.72 28294 VV n 181	0.015	40.30	80713	**	0.101	0.074
22.04 23123 UV 0.129	0.033	40.47	80/30	**	0.193	0.077
22.57 54451 WU 0.041	0.047	40.73	401820	**	0.122	0.297
23.74 55403 82 0.007	U.UD/	41.00	3169/	**	0.132	0.037
43.14 JJ07J BV U.212	U. U66	41.31	1482800	AA	U. 137	1.910

		0.085	0.199	69230 VV	56.40
		0.058	0.172	47351 W	55.46 56.16
		0.024	0.172	19545 W	55.10
		0.048	0.210	AA 69565	54.74
		0.067	0.153	54501 W	54.15
		0.060	0.146	48825 W	53.94
		0.139	0.238	113590 W	53.67
		0.254	0.229	207460 W	52.62
1.0000E+0	MUL FACTOR=	0.107	0.125	87450 W	52.13
A 1747E40	TOTAL AREA=	0.124	0.132	101660 W	51.85
000001	08 54	0.227	0.216	185240 W	51.68
		0.234	0.200	191460 VN	51.43
76776		0.144	0.145	117670 W	50.83
	94.03	0.201	0.183	164230 W	50.68
01471	94. dQ	0.104	0.128	85225 W	50.45
17674		0.150	0.190	122910 W	50.27
14407	94. 70	0.177	0.203	144400 VI	49.97
17702	10.46	0.050	0.096	40683 W	49.76
34786	93.39	0.142	0.192	115940 W	49.50
17053	89.26	0.095	0.170	77452 D W	49.06
36546 1	88. <b>3</b> 8	0.155	0.197	126670 W	48.92
24417 1	84.86	0.125	0.265	102130 W	48.64
36757 1	84.78	0 145	0.110	11A460 V	40.05
40067 V	82.78	0.046	0.103	97676 V	48 NT
66060	82.71	0.126	0.143	102640 V	47.71
14530	78 17	0.149	/ 0.176	121660 VN	47.60
217660 8	77.11	0.027	0.041	21632 M	57.44
10336	76.16	0.102	0.163	A3210 V	47.40
14065 V	74.63		0.103	LE 1111	47 10
19157 V	74.50	0.018	0.0/9	M #0541	40. / 0
26453 P	73.75	0.022	0.099	17559 W	40.01
30169 P	73.19	0.039	0.142	31712 W	46.26
	71 08	0.019	0.099	15312 VI	46.10
14712 V	70.65	0.015	0.087	12405 BN	45.88
118/60 P	70.19	0.019	0.098	15548 W	45.28
36435 V	69.28	0.076	0.143	62003 V	
24042	69.04	0.001	0 112	256A1 V	44 AA
57041 V	66.93		0.10	245670 M	44.66
146120 V	65.40		0.165	163700 1	44 33
30976 V	64.98	0.024	0.120	1911 PL 191	41.00
47300 V	63.99	0.071	0.155		
10688 8	63.08	0.052	0.126	42342 W	43, 42
103940 V	60.86	0.045	0.125	36347 W	43.29
118960 N	60.11	0.141	0.145	115320 W	42.91
12814 V	58.63	0.068	0.125	55288 VI	42.80
28497 1	57.57	0.042	0.087	34020 PM	42.70
19891	57 F2	0.016	0.110	13120 M	42.14
76112	27 73	<b>U</b> . 133	0.101	TTO DECORT	-1.00

0.021 0.015 0.086 0.064 0.164 0.164	0.066 0.057 0.037 0.037 0.037 0.037 0.037 0.037 0.017 0.017 0.017 0.017 0.045 0.045 0.045 0.045 0.045 0.045 0.021 0.045 0.021 0.045 0.056	0.092 0.016 0.016 0.116 0.127 0.127 0.127 0.127 0.127 0.013 0.013 0.019 0.070 0.029 0.029 0.069 0.145

	Table	A11				31 77	66766				
						25.77	68833		0.103		0.065
	0.5 hour con	tect	time			24.13	30023		0.089		0.060
						24.24	3///3	101	0.099		0.039
RUN #	775.	AP	R/28/86	.18:35:19		24.00	109500	212	0.122		0.112
WORKFIL	E ID: C		WORKE	TTE NAME		23.13	114/40	MM	0.159		0.118
ID: 000						25.38	103350	HH	0.138		0.106
AREAL						25.50	49820	MM	0.131		0.051
RT	AREA T	YPE	AR/HT	ARFAY		25.74	132300	KH	0.088		0.136
checkpo	int: the next	Desk	in A1-	subtract 0	Of minutes	26.00	39801	HDN	0.130		0.041
5.52	2977900	88	0 138	1 057	. Ve Bindles	26.21	20898	HOH	0.124		0.022
6.60	7608100	RV	0 177	7 810		26.46	12136	HP	0.097		0.013
6.90	938900 D	vv	0 187	0.010		26.97	28610	ЮН	0.121		0.029
7.19	148940	Ŵ	0.056	0.704		27.14	69691	юн	0.126		0.072
7.61	18033	VP	0.050	0.133		27.57	52697	ЮH	0.145		0.054
7.87	2.5632E+07	PV	0.000	26 311		27.87	90922	MM	0.112		0.093
8.06	1 53675407	w	0.175	15 760		28.03	29185	HDH	0.103		0.030
8.29	7656200	va	0 217	7 850		28.17	55191	ЮH	0.147		0.057
9 81	229380	DV.	0.141	7.037		28.39	58082	юн	0.120		0.060
10 17	337870	vv	0 14	0.236		28.82	32006	HCH	0.158		0.033
10.68	633310	DW.	0.100	0.347		29.09	30009	HH	0.113		0.031
10 84	8467100	va	0.000	0.445		29.52	31268	HH	0.134		0.032
11 95	26692	DU DU	0.143	0.071		29.70	20999	MH	0.116		0.022
12.05	47755	VV	0.102	0.027		29.81	18279	HV	0.085		0.019
12 54	114150	84V	0.112	0.049		29.93	42568	W	0.121		0.044
12.94	57/47	rv DD	0.1/4	0.11/		30.12	15053	vv	0.102		0.016
checkpo	int: the seat	rr	U. U88	0.054		30.57	90333	vv	0.117		0.093
11 35	3167000	peak	13 814		linutes	30.84	19901	VV	0.128		0.020
14 08	11407	r B VIV	0.123	3.231		31.07	16455	W	0.102		0.017
14.05	20088	<b>VV</b>	0.004	0.012		31.21	884800	vv	0.125		0.908
14.18	11156	VV VV	0.031	0.021		31.71	37506	VV	0.109		0.039
14 59	A48470	WW I	0.0//	0.034		31.85	24952	VV	0.092		0.026
14 87	415210		0.247	0.460		31.96	25749	vv	0.101		0.026
15 20	112060		0.212	0.428		32.14	40810	VV	0.145		0.042
15 30	12000	vv	0.148	0.320		32.26	17442	vv	0.075		0.018
15.68	208/.000	<b>VV</b>	0.214	0.467		32.58	80629	W	0.139		0.083
16.06	2704700		0.132	3.064		32.85	34 390	vv	0.098		0.035
checkoo			0.100	0.760		33.04	190150	vv	0.087		0.195
16 90	7778000	peak .	15 410;	, add 0.03 a	linutes	33.23	10672	vv	0.077		0.011
17 47	14122	V B	0.129	Z.338		33.40	16644	VV	0.090		0.017
17.07	14122		0.092	0.015		34.23	38726	W	0.153		0.040
17.92	78028	~~	0.090	0.101		34.54	13070	<b>VV</b> "	0.123		0.013
10.10	13030	VP	0.11/	0.014		34.86	31204	VP	0.091		0.032
10.00	34018	VP	0.1/1	0.035		35.25	60149	PV	0.122		0.062
19.09	47010	PV	0.144	0.048		35.76	10174	vv	0.083		0.010
17.33	02920	VP	0.092	0.065		35.89	23954	vv	0.106		0.025
19.05	42018	PV	0.109	0.043		36.09	53514	vv	0.167		0 055
19.90	18276	vv	0.092	0.019		36.32	56769	VV	0.074		0.058
20.20	24588	VP	0.136	0.025		36.41	176240	vv	0.103		0 181
20.97	47351	PB	0.090	0.049		36.67	169710	vv	0.124		0.174
21.51	43142	BH	0.076	0.044		checkpoint	the next	Deak	ta D3-	add	0.06 minutes
21.76	37060	ЯP	0.136	0.038		36.95	1039300	vv	0.085		1 067
22.60	47705	HP	0.080	0.049		37.20	56333	vv	0 092		0.058
23.41	24755	PH	0.212	0.025		37.35	172020	vv	0.072		0.030
23.66	24110	HH	0.089	0.025		37.58	132820	w	0 101		0.177
						37.30	134040	* *	v. 101	1	v.130

229

0.056	100 0 00 00 00 00 00 00 00 00 00 00 00 0	0 0.015	0.033	0.053	3 0.019	0 0.012	6 0.082	4 0.089	0 0.017	9 0.066	0.022	7 0.082	6 0.017	2 0.019	6 0.011	6 0.019	5 0.067	1 0.075	1 0.017					3 0.029	0.015	2 0.038	6 0.065	2 0.010	3 0.016 0 0.243	010 0 010	4 0.014	8 0.071	8 0.016	3 0.065	0.054		6 0.079	7 0.132	1 0.038	0.044	3 0.172						
0.16		8.0		0.16	0.0	0.08	0.21	0.15	90.0 0	0.15	0.12	0.22	0.15	0.11	0.05	0.08	0.17	0.1	0.22		2.0			0.11	0.15	0.11	0.23	0.10	0.12	0.12	0.14	0.39	0.24	0.17	67 D	0.141	0.18	0.20	0.05	0.05	0.16						
33	\$ ;	\$ !	\$	\$ 1	\$	\$	3	3	3	\$	3	3	3	3	3	3	3	3	2	\$ 3	\$ 3	3	: 5	3	2	3	47	<b>2</b> į	\$ 2	3	2	3	3	3		2	3	3	3	3	4 G	Ì	2				
54903		6/641	32336	09110	15675	118/3	19349	86685	16123	63761	21530	79876	16535	18001	10790	16326	84791	13066	16512	11049		19111	4/166	28136	14438	36866	82423	1001	015215	29417	13600	69175	15846	63259	4/07C	24125	77218	128180	17575	43145	10/000 9 74215	1.00005					
53.06		24.00	10.40		24.42	22.10	55.47	50.19	56.37	56.65	57.18	57.57	58.15	58.54	58.62	58.66	60.12	19.00	21.20		20. eo		65.40	66.92	69.07	69.30	70.22		21.17	77.42	79.26	79.59	61.40	62.83 64 78	86.97	88.43	93.33	94.71	94.76	94.89	TITTAL APEA	MIL FACTOR					
0.064	0.100	1.202	0.267	0.2/3	0.274	0.041	0.062	0.064	0.432	0.021	3.117	0.115	0.228	0.048	0.067	0.118	0.028	0.062	0.154	0.31	0.075		0.026	0.028	0.057	0.038	0.043	0.019	0.052 0 744	0.023	0.169	0.107	0.032	0.018	00.0 410 0	0,047	0.011	0.028	0.093	0.046	0.016		0.091	0.014	0.121	0.103	
060.0	u. 134	0.095	0.164	0.165	0.148	0.080	0. 105	0.127	0.094	0.077	0.162	0.203	0.130	0.135	0.126	0.119	0.114	0.115	0.139	711.0	0.101		0.104	0.115	0.124	0.132	0.099	0.108	0.129	0.067	0.109	0.118	0.121	0.063	0.10	0.120	0.055	0.087	0.164	0.114	0.111	- 101 C	0, 151	0.058	0.213	0.171	
33	\$ i	2	\$ i	\$	3	\$	3	3	\$	4	2	2	3	3	3	3	4	3	31	\$ }	\$ 3	5	2	3	3	3	\$	3	\$ 3	3	3	3	3	2 1	\$ 3	: 3	3	3	3	2	3 2	23	:3	3	3	₹	ģ
62777	00/001	1229100	259980	202000	266980	69609	60001	62700	421060	20563	3036200	111720	222010	46939	65041	114970	27564	60552	179590	000600	1/90/2	C041/	46456	27054	55618	36722	41642	18425	7480C	22174	164890	104.320	30855	17009	34045	45424	10797	27049	90168	44603	17365	0767C	88825	14012	117800	100620	110110
8	5	5	8	2	10	52	5	.51	2	1	8	. 75	.97	11	. 47		76.	2	9	8	2:	ġ s		6	=	. 26	.45	1.	7 6	1	50	. 28	5	9		1	8	1.41	. 51	10.1	. 28		5	69	89	. 16	37 0

	Table 4				24.20	24498	VV .	0.115	0.046
	Iable a	112			24.66	66542	8 <b>P</b>	0.114	0.126
			1-4		25.10	118690	PV	0.147	0.225
1.	U nour cont	act t	. 186		checkpoint:	the next	peak	is A25;	add 0.06 minutes
BIBI 4 334		AD	120/06	00.18.33	25.35	310520	vv	0.148	0.588
	,	Arr	UODVT1	U9:20:33	25.71	310020	vv	0.091	0.587
WORKFILL I	D: C		, worker i i	AC MARKS:	25.97	48309	vv	0.141	0.092
10: 000					26.95	23884	٧V	0.167	0.045
AKLAS		- 24	A 10 / 10**	ABTAT	27.14	13079	vv	0.091	0.025
R1	ARGA 11	DD DD	AK/11	3 503	27.32	15770	vv	0.095	0.030
<b>3.48</b>	1040000	88 88	U. 137	3.302 	27.54	48874	vv	0.174	0.093
Checkpoint	3777700	Peer	10 42; 4	1 1 1 C	27.84	74229	vv	0.126	0.141
0.00 . 4 #4	413810	TV VV	0.134	0.784	27.99	22425	vv	0.103	0.043
0.00	413810	w	0.213	0.104	28.15	53188	vv	0.158	0.101
7.10	74000	vv	0.092	0.0/6	28.36	31356	vv	0.117	0.059
7.30	4727200	w	0.072	12 741	28.51	60049	vv	0.185	0.114
7.00	8105400	<b>V</b> V	0.174	15 157	28.81	44245	VV.	0.199	0.084
8.00	50103000	V.	0.170	11 021	29.06	20962	VV	0.097	0.040
0.27	9019000	VB	0.156	0 156	29.49	20181	vv	0.124	0.038
7.40	02000	PV DV	0.156	0.107	29.66	20605	vv	0.122	0.039
9.79	30147	vv	0.150	0.102	29.78	20443	vv	0.098	0.039
10.13	86196	vv	0 130	0.160	29.89	47449	vv	0.131	0.090
10.34	417830	WW	0.137	0.100	30.51	19834	VV	0.125	0.038
10.05	3038000	vv	0.103	7 460	31.19	127790	vv	0.115	0.242
11.02	3730700	vv	0.112	0.045	31.35	64964	vv	0.130	0.123
11.07	23762	vv	0.112	0.055	31.68	24012	vv	0.116	0.046
12.02	20003	DV.	0.152	0.151	31.82	17083	vv	0.092	0.032
12.47	48708	100	0.093	0.151	31.94	17238	vv	0.106	0.033
11.00	to the next	naak	4. A14.	add 0 04 minutes	32.14	39502	vv	0.201	0.075
11 12	2303900	Paak	0 117	A 364	32.56	27980	vv	0.090	0.053
14.15	76716	w	0 166	0 145	32.84	25782	vv	0.109	0.049
14.15	\$12040	vv	0.291	0.970	33.01	84413	VV	0.096	0.160
14.30	278630	w	0 189	0.528	33.38	19243	vv	0.095	0.037
15 17	274990	vv	0 144	0 521	34.17	43016	PP	0.190	0.082
15 28	366270	vv	0 204	0 694	34.72	99953	PV	0.078	0.189
15.66	2243200	vv	0.128	A 250	34.84	18592	vv	0.079	0.035
16.03	586790	vv	0 191	1 110	35.23	32394	VV	0.121	0.061
checkpoint	to the new!	net	in A18-	add 0 05 minutes	36.00	23547	VV	0.093	0.045
16 88	4097000	vv	0 224	7 760	36.30	41866	PV	0.088	0.079
17 63	96971	vv	0 130	0.184	36.41	78132	VV	0.085	0.146
17 78	28963	vv	0 066	0.055	36.64	93412	VP	0.128	0.177
17 89	104120	vv	0 116	0 197	checkpoint	: the nex	t pea	k is D3;	add 0.05 minutes
18 06	30470	VP	0.147	0.058	36.93	1067600	21 <b>0</b>	0.100	2.022
18 58	49111	VP	0 140	0 093	37.32	74786	82	0.110	U. 142
10.30	40588	1P	0 083	0.077	37.55	38005	PP	0.080	0.0/2
19.51	17365	vv	0.241	0.033	38.15	23410	VV.	0.086	0.044
20.95	70329	VR	0.076	0.133	38.36	29704	VV	0.106	0.030
21 49	74107	PV	0.078	0.140	39.03	661700	PV	0.093	1.253
21 73	21000	vv	0 193	0 040	39.25	90018	VV	0.095	0.1/1
22.75	11721	vv	0 094	0 022	39.77	294200	vv	0.126	0.557
22.03	£1667	Ŵ	0.075	0.079	39.98	89656	vv	0.167	0.170
23 74	23639	vv	0 112	0.045	40.31	95656	VV.	0.194	0.181
23.98	10931	vv	0 071	0.021	40.48	49473	vv	0.129	0.094
24 09	12052	vv	0.081	0.061	40.75	76172	vv	0.235	0.144
47.0/	36436	••	v. vo.	A. AAT					

				102.0	0.085	0.055	0.063	0.094	0.032	0.048	0.058	0.049	0.024	0.047	0.037	0.247	0.176	0.035	0.026	0.097	0.060	0.061	0.239	0.025	0.059	0.029	0.078	0.041	0.082																				
		0 176	0 147	0.174	0.233	0.000	0.104	0.146	0.134	0.104	0.111	0.083	0.119	0.185	0.229	0.136	0.106	0.201	0.126	0.152	0.078	0.233	0.439	0.073	0.112	0.095	0.093	0.048	0.085																				
3	: 3	2	5	2	3	3	3	3	3	3	3	3	2	8	\$	2	3	2	3	2	3	2	2	3	3	3	3	3	3	6	Ş																		
	019101	20220	12064	107200	C1677	28942	86766	49853	16996	25110	30598	25832	12713	24738	19739	130430	92953 [	18295	13668	51334	31860	32392	126410	13128	30689	15288	16614	21818	43205 [	# 5.2800E4	= 1.0000E4																		
60 A1		61.66	64.97	65.39	66.94	69.28	70.17	70.22	72.15	72.36	72.46	72.57	73.76	73.90	76.21	77.10	77.14	78.33	79.16	82.75	82.82	88.38	93.32	94.65	94.78	95.33	95.47	95.52	95.60	TOTAL AREA	HUL FACTOR																		
0.053	1.154	0.132	0.116	0.020	0.148	0.111	0.396	0.201	0.023	0.059	0.046	0.066	0.057	0.044	0.253	0.067	0.044	0.076	0.058	0.173	0.022	140.0	0.0/0	<	0.043	0.160	0.067	0.103	0.140	6/0.0	0.097	960 0	0.041	0,025	0.046	0.043	0.169	0.030	0.070	0,066	0.039	0.162	100.0	010	511.0	0.118	0.063	0.027	0.024
0.114	0.159	0.113	0.152	0.128	0.184	0.203	0.241	0.146	0.116	0.092	0.074	0.126	0.123	0.131	0.130	0.097	0.094	0.152	0.134	160.0	0.095	0.121	0.131		0.050	0.113	0.135	0.055		0.140	0.130	0.101	0.115	0.086	0.129	0.116	0.145	0.105	0.098	0.148	0.184	0.165		0 0 0 0	0.116	0.147	0.142	0.114	0.124 0.181
3	3	3	3	3	2	3	3	3	3	\$	3	3	3	<b>3</b> i	<b>\$</b> i	R i	\$ !	3	\$	\$ j	<b>;</b>	2 !	\$ 3	2	\$	\$ ;	3 !	\$ i		\$ !	2	2	3	3	\$	<b>3</b> 3	: 3	3	2	3	<b>3</b> i	\$ 3	2	53	2	: 3	3	3	33
27857	609260	69532	62062	10737	24287	58348	209250	106240	12084	31184	24024	34864	29981	80152	01/661	35380	15062	19007	96/06	C/116	11400	14917	01600	14/97	Ca/77	07540	35552		7(00/	01614	01110	50478	21461	13168	24183	22817	86998	16016	37014	34621	20716	C0/CB	11111	11771	11447	62105	32994	14281	12569 91590
41.01	41.39	41.68	41.82	42.16	42.80	42.95	43.46	43.67	43.94	44.23	44.39	44.60	44.74	99 · 99	<b>4</b> 5.11	45.70	56.64	50.03	12.04	44.04	70.04					1	47.93 4 2 2 4	40. ZO		40.95 00	49.04	50.00	50.27	50.46	50.70	50.82	51.43	51.61	52.46	52.66	53.42	53.0/ 11	24. 14 24. 15		56.16	56.64	57.57	58.56	58.94 60.13

	Table	A13					23.7	0	10897	BV	0 073		410.0	
							23.8	2	31845	vv	0 119		0 040	
	4.0 hours c	ontac	t time				24.1	5	34 195	vv	0 087		0.040	
							24.20	5	31772	vv	0.143		0.045	
RUN # 78	9,	APR	/30/86	20:	12:05		24.76	D	58617	VP	0 107		0.040	
WORKF I LE	ID: C		, WORKFIL	E N	AME :		25.1	8	86955	PV	B 129		0.075	
ID: 000							check	- Doint:	the next	Deek	1. 475		0.107	
AREAL							25.4	1	390840	vv	0 130	,	O APR	
RT	AREA TY	PE	AR/HT		AREAS		25.60		123020	vv	0.150		0.400	
checkpoin	t: the next	pesk	is Al;	bb	0.06 📾	inutes	26.04		40412	ŵ	0 116		0.051	
5.54	2793900	88	0.149		3.491		27.00		16932	PV	0 113		0.031	
6.63	1856400	PB	0.159		2.320		27.29	,	10376	vv	0 118		0.011	
7.27	106630	BP	0.142		0.133		27.9	1	28717	vv	0 101		0 016	
7.67	19074	PV	0.084		0.024		28.0	5	17872	vv	0 094		0 022	
7.91 5	.5541E+07	vv	0.372	6	9.395		28.20	5	38385	vv	0.135		0.048	
9.25	239110	vv	0.166		0.299		28.41	1	29399	vv	0.119		0 017	
9.48	115070	vv	0.109		0.144		28.8	,	18253	vv	0.161		0.023	
9.87	212340	VV .	0.251		0.265		29.12	2	24481	vv	0.161		0.031	
10.22	287330	vv	0.201		0.359		29.85	5	16711	vv	0.102		0.021	
10.39	177760	vv	0.178		0.222		29.97	,	17132	vv	0.087		0.021	
10.72	464900	vv	0.113		0.581		30.60	)	42962	PV	0.113		0.054	
10.87	471150	vv	0.130		0.589		30.86	5	16741	vv	0.152		0.021	
11.13	243370	vv	0.150		0.304		31.25	5	38819	VV .	0.104		0.049	
11.37	42065	VP	0.124		0.053		31.4)	t	31660	VV	0.100		0.040	
11.97	56210	vv	0.229		0.070		31.74	6	14552	VV	0.091		0.018	
12.64	54352	PV	0.133		0.068		31.87	7	17956	VV .	0.080		0.022	
12.96	145550	vv	0.159		0.184	A A1	32.00	)	16289	vv	0.092		0.020	
checkpoin	it: the next	peak	18 A14;	sut	2 2A7	0.01	32.19	)	33544	w	0.153		0.042	
13.38	2630700	VV	0.135		3.20/		32.25	)	16094	vv	0.090		0.020	
13.83	01002	**	0.032		0.077		32.62	2	46099	vv	0.170		0.058	
14.10	13/340	1010	0.11/		0.174		32.90	3	28372	VV .	0.103		0.036	
14.17	167110	~	0.070		0.184		33.08		38034	vv	0.100		0.048	
14.22	83443	vv	0.063		0.104		33.27		20584	VP	0.070		0.026	
14.50	757690	ww	0 374		0 947		33.43		22525	PV	0.090		0.028	
14.02	381640	vv	0 196		0.477		34.28		80998	PV	0.150		0.101	
15 23	366160	vv	0.178		0.458		34.44	•	31186	vv	0.107		0.039	
15 34	427410	vv	0.211		0.534		34.91		155/3	SV.	0.073		0.020	
15 72	460110	vv	0.200		0.575		33.28		43451	PV	0.096		0.054	
15 88	326390	vv	0.158		0.408		35.4/		14614	vv	0.146		0.019	
16 10	584220	vv	0.166		0.730		35.80		12009	**	0.097		0.015	
checkpoi	nt: the next	peak	18 A18:	RT	exact		36.06		13470	172	0.083		0.017	
16.93	1462400	PB	0.108		1.827		36 31		73407	V V	0.108		0.092	
17.72	18421	vv	0.110		0.023		36 67	,	95646	V V V V	0.00/		0.039	
17.95	74105	vv	0.115		0.093		36 71		151280	vv	0.074		V. 107	
18.15	38843	vv	0.198		0.049		checks		***		U. 123	الماليم	0.172	
18.75	19947	VP	0.135		0.025		76 99		789490	NN NN	0.084		0.02 B) n 084	
19.14	24437	PV	0.120		0.031		37.24		26328	vv	0.000		0.700	
19.38	80041	vv	0.113		0.100		37.40		171740	Ŵ	0.130		0 215	
19.66	41651	VV	0.199		0.052		37.62		92736	vv	0.103		0.116	
20.98	13873	PP	0.080		0.017		38.02		14705	vv	0.119		0.018	
21.78	13900	BV	0.124		0.017		38.22		76720	VV	0.105		AP0.0	
22.09	19800	vv	0.110		0.025		38.43	ļ.	43905	vv	0.137		0.055	
22.63	37155	VP	0.090		0.046		39.09	н .	688590	vv	0.093		0.860	
									· · - <del>-</del>					

55.56	54,83	54.25	54.04	53.77	53.40	53.15	52.95	52.52	52.08	51.84	51.50	50.92	50.77	50.52	50.35	50.07	49.86	49.58	49.17	49.00	48.72	48.33	48.11	47.99	47.78	47.61	47.50	47.45	47.19	46.92	46.52	46.16	45.96	45.37	45.20	st. 74	44.43	44.22	43.75	63.51	43.36	62.99	42.80	41.74	41.40	41.09	40.80	40.57	40.38	40.30	40.06	39.83	39.33
22025	28141	42887	11426	38900	13487	50162	30070	97684	30386	25433	61387	50737	30557	30364	29115	70060	22334	26028	50902	62090	39163	71508	207510	13804	139270	64789	14916	22696	25229	22893	19404	10248	16053	40103	32247	135110	43414	26793	71725	42630	61567	55094	62797	58361	869410	54163	106850	59870	62028	40634	297150	307490	163900
PP	Ş	¥	Ş	Ş	Ş	Ş	Ş	\$	\$	Ş		Ş	Ş	Ş	Ş	Ş	\$	2	\$	Ş	Ş	Ş	Ş	Ş	Ş	Ş	\$	V	Ş	2	Ş	Ş	Ş	Ş	Ş	Ş	\$	2	\$	\$ :	\$ :	Ş	2:	\$ :	\$	Ş	Ş	Ş	Ş	Ş	\$	\$	Ş
0.139	0.189	0.200	0.092	0.172	0.106	0.181	0.130	0.202	0.126	0.117	0.161	0.145	0.150	0.132	0.135	0.224	0.136	0.112	0.175	0.139	0.150	0.105	0.099	0.057	0.125	0.130	0.045	0.075	0.105	0.163	0.100	0.134	0.106	0.143	0.114	0,121	0.128	0.093	0.140	0.122	0.134	0.183	0.095	0.112	0.158	0.176	0.149	0.121	0.120	0.081	0.153	0.147	0.168
0.028	0.035	0.054	0.014	0.049	0.017	0.063	0.038	0.122	0.038	0.032	0.077	0.063	0.038	0.038	0.036	0.088	0.028	0.033	0.064	0.078	0.049	0.089	0.259	0.017	0,174	0.081	0.019	0.028	0.032	0.029	0.024	0.013	0.020	0.050	0.040	0.169	0.054	0.031	060 0	0.053	0.052	0.069	0.054	0.073	1 086	0.068	0.134	0.075	0.078	0.051	0.371	0.384	0.205

HUL FACTOR	88.90	85.11	83.12	83.05	79.54	78.63	77.38	77.36	77.32	77.28	74.86	73.98	70.40	69.51	67.14	65.56	64.95	61.00	60.26	57.69	57.65	56.73	56.51	56.25
0.0035E+07 1.0000E+00	44509 PV	51496 VP	20570 W	55140 PV	14209 BV	15004 BV	80250 D VB	20783 W	20833 D VV	55059 VV	46237 VV	14251 W	72778 VV	57070 VV	43671 PV	99689 PV	16499 VV	56418 PV	62066 VV	18169 VV	10310 BV	62898 VV	24737 VV	41063 PV
	0.403	0.305	0.060	0.176	0.152	0.230	0.112	0.033	0.034	0.100	0.198	0.134	0.245	0.205	0.271	0.180	0.161	0.147	0.183	0.096	0.067	0.179	0.141	0.142
	0.056	0.064	0.026	0.069	0.018	0.019	0.100	0.026	0.026	0.069	0.058	0.018	0.091	0.071	0.055	0.112	0.021	0.071	0.078	0.023	0.013	0.079	0.031	0.051

	Table A	14				19.35	57578	VP (	0.087	0	.066
						19.59	18867	VP (	D. 267	0	. 022
	8.0 hours con	tact	time			20.05	26977	PV (	D.083	0	. 031
-						20.82	12578	VV (	0.069	0	.014
RUN # 2	790.	MA	¥/01/86	11.52.11		21.15	17181	VP (	D.085	0	. 020
VORKETL	5 ID- C	1 101	MORKEI	15 NAME:		21.75	25319	VV (	D. 226	0	. 029
1D: 000			, works I	LAL MALTLE.		22.06	26041	vv i	0.099	0	.030
ARFAT						22.44	10433	vv i	0.104	0	.012
PT	ABEA T	VDE	AB /IPT			22.61	63847	vv i	0.086	C	.073
5 09	139450	80	AR/11	AREAL		23.39	23496	PV	0.239	Ċ	0.027
chackood		Dr.	0.130	0.159	<b></b>	23 68	15176	vv	0.096	Ċ	0.017
5 40	4187400	haar	18 41;	subtract	0.01 minute	23 79	43714	vv i	0.171	Ċ	0.050
5.47	4267000	FV MB	0.103	4.8/9		24 03	20863	vv i	0.080	č	0.024
5.75	4,0000	VF DU	0.071	0.050		26.12	37489	vv	0.083	č	0.043
3 03	1693000	FV.	0.101	Z. 154		24.25	36094	vv	0 138	č	061
7.02	100920	VV	0.1/2	0.192		24.25	79697	VP	0 122	ì	1 091
7.24	330150	Ab.	0.1/6	0.383		24.00	110620	Ŵ	0 111	Ì	126
7.02	1/900	<b>PV</b>	0.093	0.021		25.17	430160	w	0 145	ì	490
7.80	4.3242E+U/	vv	0.297	51.486		23.37	136170	vv	0.143		1 155
6.30	1.13//E+07	vv	0.261	12.948		23.37	21600	ww	0.141		0.025
9.44	340240	VV.	0.278	0.445		25.04	21507	w	0.077		0.025
9.80	247140	vv	0.264	0.281		20.01	37666	vv vv	0.179		0.003
10.16	480620	VV	0.176	0.547		20.30	10010		0.177		0.031
10.37	239950	vv	0.168	0.273		20.70	56694	rr wu	0.100		0.055
10.68	697520	vv	0.124	0.794		27.09	33374		0.101		0.005
10.83	341670	vv	0.128	0.389		28.03	31301		0.075		0.016
11.08	261680	vv	0.145	0.298		20.18	31701	<b>VV</b>	0.134		0.030
11.34	49270	VP	0.139	0.056		28.52	41100	101	0.104		0.04/
11.93	22750	PV	0.101	0.026		28.83	22214	102	0.103		0.023
12.05	29758	VP	0.106	0.034		29.11	12144	**	0.121		0.014
12.26	13138	PP	0.088	0.015		29.81	109/4	PV	0.124		0.017
12.55	64020	PV	0.167	0.073		29.92	24201		0.090		0.020
12.92	49050	PP	0.085	0.056		30.56	21984	PV	0.115		0.023
checkpoi	nt: the next	peak	is A14;	add 0.02	minutes	31.22	19612	**	0.108		0.022
13.35	4101100	PB	0.117	4.667		31.40	53541	VP mit	0.113		0.001
13.83	13791	BV	0.082	0.016		31.71	11391	PV	0.085		0.013
14.07	39185	vv	0.090	0.045		31.65	14880	**	0.0/5		0.017
14.18	64676	vv	0.086	0.074		31.98	16195	VV 	0.103		0.016
14.24	47629	W	0.058	0.054		32.27	10194	VB	0.076		0.012
14.37	120990	W	0.113	0.138		32.66	14614	BV	0.120		0.01/
14.46	105570	vv	0.081	0.120		32.87	18006	VV	0.094		0.021
14.58	648720	VV .	0.205	0.738		33.06	23359	VP	0.111		0.02/
14.85	329970	VV	0.149	0.376		33.42	21465	vv	0.105		0.024
15.05	109980 D	vv	0.053	0.125		34.03	15336	PV	0.108		0.018
15.19	539920	VV	0.150	0.614		34.21	111840	vv	0.165		0.127
15.31	557730	w	0.184	0.635		34.89	18300	vv	0.098		0.021
15.68	560990	VV .	0.204	0.638		35.26	25665	PV	0.111		0.029
15.84	330660	vv	0.144	0.376		36.04	189060	vv	0.108		0.215
16.06	583420	vv	0.131	0.664		36.45	67824	٧P	0.083		0.077
checkpoi	nt: the next	peak	1s A18:	add 0.03	minutes	36.69	89300	PP	0.123		0.102
16.90	5008000	VB	0.192	5.699		checkpoin	t: the next	pesk	is D3;	add	0.05 minutes
17.67	88320	BV	0.114	0 101		36.96	1196100	PB	0.105		1.361
17.91	27704	VP	0.092	0 012		37.36	100970	BV	0.109		0.115
18.68	11330	PV	0.071	0.012		37,60	46342	VP	0.078		0.053
19.23	97712	vv	0.087	0 111		37.99	23029	VP	0.092		0.026
				A . 1 1 1							

		0.013	970.0	0.045	0.021	0.015	0.020	0.064	0.023	0.043	0.025	0.020	c10.0		10.0		0.052	0.023	0.021	0.069	0.126	0.014	0.060	0.013	0.035	0.047	0.045																				
		11.0	0.176	0.152	0.196	0.170	0.108	0.168	0.156	0. 165		. 135	0 201 0	0.203	0.080	0.136	0.189	0.066	0.063	0.226	0.484	0.147	0.485	0.069	0.150	0,140	0.113																				
	2	23	3	£	đ	2	3	Z i	\$ :	3	23	3	:3	2	:3	3	3	3	8	3	2			23		\$ }	- 	• c	,																		
	11616	23200	14004	39070	18133	12874	17093	92922	4/60Z		69177	34/11	67332	27342	39026	72572	45997	19784	18634	60400	110700	12690	52738	11327			27100	1.0000F40																			
	58.59	60.01	60.17	60.97	61.70	62.25	89.40				17 17	73.92	74.45	77, 16	77.27	12.31	11.11	77.84	06.77	16.28 00 00	80' '88	97.78 83 58	10.07	00 50	AC 76		TUTAL APPAR	MUL FACTOR-																			
0.040 0.022	0.423	0.049	0.31	0.070	0.018	0.066	0.030	0.612	0.063	0.079	0.106	0.072	0.055	0.035	0.032		0.071	0.034	0.022	0.023	0.032	0.021	0.015	0.120	0.116	0.029	0.020	0.038		0.05	0.035	0.030	0.026	0.076	0.027	0.047	0.044	0.064	0.065	0. 012	0.100		10.0	0.01	0.025	0.085	0.053
0.085 0.127	0.094	0.093	0.120	0.10/	0.070	0.175	0.102	0.174	0.105	0.131	0.177	0.202	0.154	0. 11Z	0.121	0.000	114	0.128	0.109	0.124	0.132	0.102	0.102	0.215	0.115	0.101	0.090	0.094	0.136	0 140	0.097	0.074	0.065	0.153	0.098	0.181	0.126	0.142	0.141	0.099	0.156	601 · D	101.0	121 0	0.142	0, 180	0.157
23	2	3	2 3	\$ 3	:3	3	3	3	3	≩	۶	3	3	\$ !	2 2	23	3	2	2	3	3	3	2	3	3	3	3	5	2 :	5	: 2	3	\$	3	33	3	₹	2	\$ i	\$ ;	3 i	\$ 3	5 9	2	3	3	2
34783 19270	371910	42645	275470	0/6661	14016	56138	25974	537700	55474	17689	92896	62853	47873	1/606	16682	11411		29763	19042	20340	27648	18136	13054	105580	102000	25443	17184	33779	114720	(	22116	26112	23122	66748	23673	41125	36478	55909	57399	06901	87784	4/671	79701	58589	22219	74429	46696
38.20 38.39	39.07	39.30	39.80	40.03	12 07	40.78	41.04	41.39	41.73	41.85	42.85	43.06	43.34	43,46	43.72	67 - <b>44</b>	14 67	52 - 53 52 - 52	45.74	45.94	46.28	46.47	47.17	47.58	47.75	47.97	48.09	48.29	48.66	48.90	49.564	49.67	49.74	50.04	50.30	50.74	50.89	51.48	52.50	53.35	53.70	24.07	81.42	10.00	56.48	56.71	57.66

	Table	A15				19.3	9 96541	٧V	0.104	0,103
						19.6	6 33057	vv	0.199	0.035
	24 hours co	ntact '	time			20.2	4 10494	PV	0.103	0.011
						20.5	6 15046	PP	0.164	0.016
RUN # 7	766,	AP	R/30/86	,18:28:35		20.9	9 16222	PP	0.082	0.017
<b>WORKFILE</b>	E 1D: C		, WORKE	ILE NAME:		21.7	9 30003	BV	0.117	0.032
ID: 000						22.0	9 54546	vv	0.125	0.058
AREA%						22.6	3 51783	٧V	0.165	0.056
RT	AREA	TYPE	AR/HT	AREAT		22.8	2 12563	VP	0.167	0.014
5.12	82563	BP	0.122	0.088		23.0	9 10914	PV	0.090	0.012
checkpoi	int: the nex	t peak	is Al;	subtract 0.07	minutes	23.7	1 13601	PV	0.072	0.015
5.55	1017800	PP	0.150	1.090		23.8	2 \$3730	vv	0.162	0.058
6.65	2274300	BV	0.178	2.436		24.1	5 36171	vv	0.083	0.039
7.04	103450	vv	0.138	0.111		24.2	9 60284	VV	0.175	0.065
7.26	195580	VP	0.194	0.210		24.4	8 13658	VV	0.086	0.015
7.89	6.6721E+07	SPB	0.371	71.454		24.7	1 53752	VP	0.117	0.058
9.36	10352	TVP	0.064	0.011		25.1	7 127840	PV	0.125	0.137
9.87	28295	VP	0.133	0.030		25.4	1 576360	VV	0.140	0.617
10.21	168260	PV	0.162	0.180	,	25.6	1 158300	VV	0.138	0.170
10.40	84112	٧V	0.142	0.090		26.0	4 88966	VV	0.146	0.095
10.72	350950	vv	0.099	0.376		26.2	5 51768	VV	0.147	0.055
10.88	1465500	vv	0.125	1.569		26.5	0 38005	VV	0.149	0.041
11.12	250900	vv	0.143	0.269		27.0	1 75313	Ŵ	0.144	0.081
11.44	139090	vv	0.125	0.149		27.2	3 18916	vv	0.070	0.020
11.63	84710	٧V	0.128	0.091		27.3	0 39329	vv	0.107	0.042
11.96	11608	VV	0.081	0.012		27.5	0 63175	vv	0.230	0.068
12.08	29621	VP	0.113	0.032		27.7	9 24517	vv	0.112	0.026
12.64	59870	PV	0.181	0.064		27.9	1 53450	VV	0.103	0.057
12.95	133260	vv	0.143	0.143		28.0	6 37428	vv	0.118	0.040
13.15	54598	vv	0.088	0.059		28.2	0 60047	vv	0.144	0.064
checkpoi	int: the neg	rt peak	is A14	; subtract 0.0	l minute	28.4	3 64190	VV	0.122	0.069
13.38	2630300	vv	0.138	2.817		28.8	7 47082	VV	0.133	0.050
13.84	97422	vv	0.059	0.104		29.0	5 17555	VV	0.077	0.019
14.08	151080	vv	0.088	0.162		29.1	2 22556	vv	0.087	0.024
14.24	366860	vv	0.188	0.393		29.5	5 49379	vv	0.203	0.053
14.34	85647	vv	0.044	0.092		29.7	3 10037	vv	0.082	0.011
14.37	5039 <b>0</b>	vv	0.026	0.054		29.8	5 23702	VV	0.107	0.025
14.63	933570	vv	0.301	1.000		29.9	6 32962	VV	0.114	0.035
14.90	680530	vv	0.239	0.729		30.2	9 35132	vv	0.210	0.038
15.02	89907	D VV	0.034	0.096		30.5	9 39418	٧V	0.112	0.042
15.06	75900	D VV	0.029	0.081		31.1	0 17483	vv	0.143	0.019
15.08	94032	D VV	0.036	0.101		31.2	5 87025	٧V	0.104	0.093
15.24	541690	vv	0.188	0.580		31.4	1 40778	VV	0.096	0.044
15.34	141840	vv	0.051	0.152		31.7	4 18300	vv	0.086	0.020
15.72	918100	VV	0.161	0.983		31.8	7 31534	VV	0.082	0.034
15.86	489000	vv	0.161	0.524		32.0	1 21893	VV	0.116	0.024
16.12	822720	VB	0.234	0.881		32.2	0 33668	vv	0.133	0.036
checkpo:	int: the nex	xt peak	is Al8	; subtract 0.0	l minute	32.2	9 14282	VV	0.067	0.015
16.94	1239300	BB	0.117	1.327		32.6	1 64347	vv	0.138	0.069
17.73	23874	BV	0.127	0.026		32.9	0 41755	vv	0.113	0.045
17.94	31834	vv	0.134	0.034		33.0	9 38186	vv	0.110	0.041
18.14	23026	٧V	0.123	0.025		33.2	8 49176	vv	0.093	0.053
18.74	12370	VP	0.129	0.013		33.4	5 25729	VP	0.090	0.028
19.16	35525	PV	0.184	0.038		34.2	4 208390	VV	0.140	0.223

34.44	11715	3		2 266	50.52	24549	≩	0.100	0.026	
14. 97	20312				50.92	45416	3	0.133	0.049	
35.29	46080	: 3			51.07	17248	3	0.122	0.019	
35.48	96601	5	0, 105		51.50	50960	2	0.128	0.055	
35.91	15304	3	0.073	910 0	51.77	10905	3	0.097	0.012	
36.06	232730	3	0.114	0.249	52.51	40502	2	0.103	0.043	
36.47	17271	48	0.085	0.083	52.98	20525	3	0.142	0.022	
36.72	182860	٨	0.115	0.196	53.38	30405	<b>s</b> i	0.161	0.033	
checkpoint:	the next	peak	ie 03;	add 0.02 minute	53.76	31927	2 ]	0.129	40.0 400.0	
36.99	984370	3	0.087	1.054	47.40	29542 15845	\$ 3	121 0	0.010	
37.24	16350	31	0.084	0.016	56.26	51418	2	0.136	0.055	
04.10	01/922	}}	0.127	0.241	56.49	46663	3	0.180	0.050	
20.15	124560	3	0.102	0.133	56.70	22877	3	0.074	0.025	
	000001	2 3	0. 128	0.113	57.29	13169	4	0, 165	0.014	
27.0C	16203	\$ 3		0.101	57.67	51296	a.	0.145	0.042	
39.10	824770	:3			58.15	10976	3	0.139	0.012	
39.33	121260	3	0.160	011.0	60.24	69589	\$	0.268	0.075	
39.82	792080	3	0.154	0.848	60.99	57082	È.	0.152	0.061	
40.32	105220	3	0.204	0.113	61.76	10262	2	0.115	0.011	
40.55	26624	3	0.113	0.029	64.12	17328	2	0.179	0.019	
40.70	23920	3	0.100	0.026	64.95	6065	\$ i	0.279	0.063	
40.82	26466	\$	0.090	0.028	65.52	28982	\$ į	0.070	160.0	
41.12	35741	3	0.154	0.038	67.05	13798	\$ i	0.095	0.015	
41.39	845000	3	0.158	0.905	<b>65</b> .02	1166	\$	0.15/	0.036	
41.76	43137	3	0.098	0.046	68.10	26/52	\$ i	0.092	0.028	
41.87	43077	٩Y	0.114	0.046	66.17	46694	\$ ;	0.100	0.00	
42.19	19245	2	0.143	0.021	04.60	21262	\$ !	0.121	0.025	
42.87	122040	٨	0.162	10.131	79.07	0496/		0.269	0.056	
43.35	62333	3	0.128	0.067	12.00		2			
43.49	38469	٩٧	0.111	0.041	10.2	94261	\$ 3	101.0	- 10 · 0	
43.74	46369	₹	0.117	0.050	10.11					
43.96	11549	5	0.115	0.012		61691	2 3	110 110	0.020	
44.41	16886	3	0.103	0.018		74.013	2 3	0.110		
45.20	14359	2	0.072	0.015	90.00 VV SN	0/010	: 3	111.0	0.00	
	12320	<b>8</b> :	0.090	0.013	11 28	1111	3		0.016	
4000 20	19111	5	0.105	0.012	20 ° 25	11077 1110	: 3	0.456	0.090	
11 47	13151	\$ 3	0.052	0.015	TOTAL AREA-	9.3376E4	5			
46. 32	15826	:3	0.120	0 017	MUL FACTOR=	1.0000E4	ş			
46.54	19428	٩٧	0.095	0.021						
46.92	20741	3	0.122	0.022						
47.19	26193	\$	0.092	0.028						
47.51	47687	2	0.093	0.051						
47.61	105220	3	0.154	0.113						
47.78	147590	3	0.130	0.158						
48.00	28804	3	0.112	0.031						
48.33	54593	d A	0.090	0.059						
48.71	33237	2	0.128	0.036						
48.99	59658	3	0.121	0.064						
49.15	49705	\$ i	0.150	0.053						
49.3/ 50.06	2/611	2 7	0.060	0.012						
	11704	23	0.134	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2						
	טפנונ	**	0.140	0.034						
	Table	A16				22.81	13239	W	0.134	0.025
-------------	--------------	--------------	---------	--------------	------------	------------	----------	-------------	--------	---------------
						23.30	13369	<b>PV</b>	0.112	0.026
	pH 3	,				23.45	16618	vv	0.161	0.012
						23.80	\$6508	vv	0.196	0.108
	55, 10. 0	AP	R/30/86	,13:10:08		24.04	32763	VV	0.077	0.063
NORREILE	1D: C		WORKE	ILE NAME:		24.15	56817	VV	0.166	0.109
ADEAN						24.70	72085	VP	0.122	0.138
RALAS DT		-				25.17	144600	PV	0.141	0.276
sheckee/a	ARLA I	TPE	AR/HT	AREAS		25.40	377540	vv	0.135	0.721
c cc	1431000	. peak	15 AL;	BUDtract 0.0	D7 minutes	25.85	22101	VV	0.117	0.042
5.55	1431000	88	0.153	2.733		26.04	39306	vv	0.127	0.075
7 74	1981900	BV VAV	0.203	3.765		26.24	28190	W	0.163	0.054
7 97	7877000	1947 1947	0.211	0.344		26.50	10172	vv	0.092	0.019
8 10	9579700	vu	0.1/3	15.042		26.99	26317	PV	0.119	0.050
8.12	\$423900	Va	0.170	10.294		27.28	12442	W	0.144	0.024
9 48	42760	10	0 166	10.337		27.61	17436	BV	0.108	0.033
9.87	59565	PV	0.122	0.082		27.92	32672	BH	0.134	0.062
10.20	196550	vv	0 211	0.114		28.05	10733	HCH	0.076	0.021
10.72	356470	vv	0 115	0.575		28.21	46648	NM	0.176	0.089
10.88	568280	vv	0 121	1 085		28.41	37788	нH	0.121	0.072
11.12	286580	vv	0 151	0 547		28.53	26735	<b>KO</b> K	0.117	0.051
11.36	114020	VP	0.144	0.218		28.88	23794	ЮH	0.141	0.045
11.78	51814	PV	0.135	0.099		29.03	10683	HDA	0.085	0.020
11.96	16411	vv	0.079	0.031		29.11	12036	HCH	0.091	0.023
12.08	31523	VP	0 139	0 040		29.29	26100	HH	0.166	0.050
12.59	67086	PV	0.192	0.128		29.55	12150	KCH	0.115	0.023
12.96	61021	PV	0.113	0 117		29.72	17173	ЮH	0.117	0.033
13.14	32706	VV	0.092	0.063		29.83	29928	MH	0.098	0.057
checkpoin	t:the next	peak	In A14:	subtract 0.0	1 minute	29.95	31059	HH	0.103	0.059
13.38	2547500	vv	0.126	4.865		30.18	35736	WH	0.197	0.068
13.64	101660	vv	0.110	0.194		30.83	27182	HOH	0.095	0.052
14.21	26045	vv	0.108	0.050		31.24	43473	HOM	0.113	0.083
14.62	141530	PV	0.153	0.270		31.41	33015	MP	0.088	0.063
14.68	121150	VV	0.184	0.231		31.74	16040	PH	0.077	0.031
15.21	20513	BV	0.077	0.039		32.17	21030	NV	0.131	0.040
15.36	117100	VV	0.204	0.224		32.01	80849	**	0.142	0.116
15.72	472580	VV	0.115	0.902		32.90	32350	**	0.098	0.062
15.86	139310	VV .	0.124	0.266		33.00	109310		0.091	0.209
16.11	333310	VP	0.162	0.637		33.44	14204	171	0.0//	0.027
checkpoin	t: the next	peak	is A18;	RT exect		33.07	10111	1714	0.132	0.028
16.93	4024000	PB	0.136	7.684		36 23	17111	<b>VV</b>	0 104	0.037
17.70	27324	BV	0.079	0.052		34.50	20223	171	0.104	0.033
17.93	32048	vv	0.099	0.061		34 90	18217	WW I	0.111	0.039
18.11	14968	vv	0.147	0.029		15 10	16410	W	0.005	0.035
18.71	85182	VP	0.122	0.163		35.50	16707	10	0.111	0.001
19.38	66948	VP	0.094	0.128		35 AL	12124	VV VV	0.132	0.031
19.65	38730	PV	0.179	0.074		35 92	13447	vv	0.001	0.024
20.20	17489	PP	0.201	0.033		36.14	48367	vv	0.002	0.020
20.84	15896	PV	0.080	0.030		36 17	46601	~~	0.137	0.072
21.72	45281	PV	0.304	0.087		36 47	\$7334	vv	0.003	0.009
22.22	23381	vv	0.173	0.045		36.72	145060	vv	0 133	0.110
22.51	16647	vv	0.135	0.032		charkpoint	the nert	NV DAAL	i= D1-	add 0 02 m/mm
22.63	25655	vv	0.097	0.049		36.99	1221500	VV	0.094	2.333

50.75 50.91	50.51	SO. 35	49.70	49.59	49.02	48.71	40.UI	48.01	47.78	47.65	47.18	47.02	46 81	40. JU	46.37	46.20	45.95	45.83	45.58	45.36	45.10 10	44.35	43.95	43.77	43,47	43.40	42.88	42.81	42 41	41.35	41.16	41.10	40.34	40.38	40.04	39.83	39.42	10.01			38.22	38.07	
68099 195140	53535	204580	87047	96850	155780	091691	01.0710	57220	104740	234990	48371	30923	21102	3/15/	57862	32247	27374	11615	10657	14601	06718	27571	50242	35177	123290	190710	61564	64684	18694	1971500	38720	35504	61044	109360	172610	273010	132060	125260	894000	04/03	41228	14068	01077
\$\$	23	5 5	į٤	Ş	\$ :	53	53	\$:	\$:	\$:	\$:	\$ :	53	1	\$	Ş	Ş	2	Ş	\$:	2 3	2	Ş	Ş	\$	5 5	٤	\$	53	12	\$	\$ :	٤ \$	Ş	Ş	\$	\$ :	٤ :	53	2 2	5	Ş	
0.095 0.220	0.075	0.242	0.120	0.146	0.222	0.252	0.178	0.123	0.139	0.216	0.137	0.124	0.104	0.124	0.145	0.139	0.113	0.126	0.097	0.105	0 121	0.148	0.114	0.130	0.144	0.155	0.081	0.121	0.107	0.169	0.094	0.106	0.109	0.156	0.216	0.192	0.163	0.097	0.030	0.150	0.094	0.097	
			. 0	0	<u>.</u>	<u> </u>	<b>-</b> -	•	•	0		-	<b>-</b> -			0.0	0	0	0	<u>.</u>	-	0.0	0	0		• •					0	0		0.1	0	0	0			2		0.0	0.0

		ġ	1.0000E-	HUL FACTOR=
		5	4 3367E4	TOTAL ARFA=
0.07	0.205	Ş	37530	88.86
0.02	0.089	Ş	11778	88.76
0.05	0.233	Ş	29354	85.22
0.04	0.178	Ş	25200	79.47
0.05	0.057	Ş	29873	77.36
0.09	0.109	2	50558	77.32
1.79	0.407	Ş	941690	74.12
0.06	0.220	BV	35764	71.48
0.12	0.232	Ş	63247	70.43
0.04	0.233	Ş	22991	69.88
0.04	0.096	Ş	21799	69.47
0.07	0.133	Ş	40015	68.62
0.02	0.191	Ŋ	14550	68.24
0.06	0.226	2	36107	66.88
0.14	0.179	ą.	74236	65.58
0.05	0.163	Ş	26255	64.80
0.02	0.149	Ş	13061	64.13
0.12	0.195	Ş	66582	62.61
0.17	0.193	Ş	90702	61.00
1.08	0.239	Ş	568020	60.20
0.82	0.250	Ş	432620	59.10
0.06	0.139	P	31196	57.70
0.10	0.162	Ş	54787	56.76
0.17	0.128	Ş	93044	56.27
0.15	0.206	Ş	79959	55.56
0.05	0.121	Ş	29057	\$5.07
0.17	0.236	Ş	90557	54.84
0.06	0.111	Ş	31755	54.60
0.13	0.160	Ş	72568	54.25
0.27	0.162	Ş	143060	53.78
0.18	0.168	Ş	95891	53.53
1.11	0.417	Ş	581630	52.56
0.23	0.120	Ş	122500	52.21
0.19	0.100	Ş	100990 1	52.04
1.52	0.326	Ş	000090	51.62
0.18	0.105	Ş	96064	51.21
0.28	0.163	Ş	149740	51.11

.

		24.13	40160	vv	0.094	0.061
Table A17		24.46	14932	vv	0.109	0.023
		24.68	81021	٧P	0.109	0.122
DH 5		25.16	111160	PV	0.135	0.168
Ph S		25.40	480680	VV .	0.153	0.726
PIN # 791 HAY/01/86	16:30:36	26.02	86193	W	0.176	0.130
WORKFILE ID. C	E NAME:	26.22	28644	WV .	0.114	0.043
10-000		26.48	33972	VV .	0.149	0.051
ARFAT		26.78	37186	W	0.252	0.056
RT AREA TYPE AR/HT	AREA%	26.97	44860	WV .	0.177	0.068
checknoint; the next peak is Al; a	ubtract 5.48	27.19	13446	VV	0.067	0.020
5 51 5064000 BB 0.174	7.643	27.27	27489	VV	0.113	0.042
6 62 1740600 BV 0.169	2.627	27.53	53804	VV	0.243	0.081
7 25 165160 VP 0.183	0.249	27.88	42054	VV .	0.120	0.064
7.88 2.0569E+07 PV 0.195	31.045	28.04	28205	VV	0.118	0.043
8.06 1.1564E+07 D VV 0.161	17.454	28.17	38369	VV	0.152	0.058
8.31 7744000 VB 0.240	11.688	28.40	57914	W	0.143	0.087
9.46 15204 BP 0.110	0.023	28.85	33205	VV	0.178	0.050
9.86 71219 PV 0.169	0.108	29.11	26400	VV	0.175	0.040
10.18 289840 VV 0.175	0.438	29.55	17866	vv	0.159	0.027
10.37 130080 VV 0.159	0.196	29.82	23205	vv	0.119	0.035
10.69 424650 VV 0.114	0.641	29.93	25710	vv	0.128	0.039
10.84 371770 VV 0.132	0.561	30.13	20675	vv	0.125	0.031
11.09 162290 VV 0.148	0.245	30.57	46978	vv	0.141	0.071
11.35 48019 VP 0.126	0.073	30.84	10562	WV .	0.107	0.016
11.96 16915 PV 0.091	0.026	31.22	33051	VV.	0.108	0.050
12.05 27115 VV 0.112	0.041	31.39	28000	VV .	0.100	0.042
12.58 64142 PV 0.178	0.097	31.72	12030	W	0.083	0.018
12.94 36674 PP 0.097	0.055	31.85	16225	VV	0.084	0.025
checkpoint: the next peak is A14;	add 0.01 minutes	31.98	11186	VV.	0.093	0.017
13.36 3687900 PB 0.113	5.566	32.14	26929	vv	0.147	0.041
14,18 19618 VV 0.081	0.030	32.39	50880	<b>VV</b>	0.135	0.077
14.59 357130 VV 0.218	0.539	32.07	20419	**	0.102	0.031
14.86 198270 VV 0.179	0.299	33.00	20332	**	0.117	0.031
15.20 185450 VV 0.139	0.280	33.29	24412		0.007	0.03/
15.32 333380 VV 0.216	0.503	33.42	10008	BW .	0.075	0.024
15.70 327510 VV 0.189	0.474	34.27	36579	WW	0.120	0.051
15.85 246990 VV 0.153	0.3/3	34.42	12317	w	0.087	0.000
16.07 766770 VB 0.151	1.157	35 26	28216	80	0 103	0.043
checkpoint: the next peer is Alo;	2 844	15 89	15283	Ŵ	0.084	0.023
16.91 1898/00 BB 0.11/	2.000	36 03	\$5801	vv	0.169	0.084
17.09 20200 VV 0.103	0.040	36.36	24709	vv	0.087	0.037
[/.93 34303 VV U.103	0.029	36.45	67330	vv	0.099	0.102
18./U 18924 VF U.132	0.023	36.70	129640	Ŵ	0.131	0.196
19.11 2/343 VV 0.102	0.042	checknoint:	the next	nesk	is D3: add	1 0.04 minutes
19.36 32368 VP 0.133	0.041	36.97	615220	vv	0.101	1.231
21 74 2360 VV 0 190	0.036	37.21	24614	VV .	0.085	0.037
22.06 13509 VV 0.149	0.051	37.37	111610	VV .	0.140	0.169
22.00 55565 W 0.149	0.089	37.60	85646	W	0.124	0.129
23 38 10355 PV 0.177	0.016	38.20	40130	W	0.094	0.061
23.30 10333 FV 0.1// 23.60 15553 VV 0.083	0.024	38.39	55190	VP	0.165	0.083
23.05 13333 VV 0.003	0.073	39.07	685630	W	0.094	1.035
24.03 15513 VV 0.000	0.023	39.30	145610	VV	0.191	0.220
TA'AA TILTA AA A'AAA		-				

39.81 19.07	296620 181640	33	0.139	0.448 0 479	67.06	15603	3	0.136	0.024
40.04	SADAI	3			69.17	14985	\$	0.160	0.023
40.78	190420	3	0.147	0.207	79.42	1007	\$	0.103	0.040
41.12	56537	3	0.166	0.065	10.01		23	0.050	0.023
41.35	1114300	3	0.162	1.682	70.15	14955	3	0.062	0.02
41.73	77646	3	0.115	0.117	70.36	134310	3	0.282	0.203
41.84	70200	3 i	0.157	0.106	71.40	13444	3	0.230	0.020
79.74	82.304	2 9	0.160	0.124	71.92	90065	3	0.398	0.089
43.35	19298	2	0.087	0.029	86.67	36547	3	0.178	0.055
43.47	43507	3	0.138	0.066	14.40	11111	5	1.237	800.0
43.74	68726	3	0.114	0.104	77.24	76310	: 3	0.111	511.0
43.93	17394	\$	0.124	0.026	77.29	36812	3	0,049	0.056
44.20	130740	3 :	0.097	0.197	77.32	86074 1	3	0.112	0.130
	99559	\$ !	0.133	0.099	82.99	60624	2	0.163	0.092
44. /] 45. 18	134340	\$ 3	0.121	0.203	83.05	42719	3	0.102	0.065
1.14	1111	3	0 097	0.020	84.95	10529	\$	0.096	0.016
45.93	26427	: ≩	0.119	0.043		00021	\$ }	0/0.0	0.019
46.11	28738	3	0.128	0.043	TITAL ABEA-	19869 9	2	717.0	nen n
46.28	21510	3	0.093	0.033	MIL FACTOR	1 000064	Ì		
46.84	13970	2	0.098	0.021			3		
47.17	12872	2	0.080	0.019					
47.58	91625	3	0.204	0.138					
47.75	115870	3	0.106	0.179					
48.09	189510	\$	0.108	0.286					
16.9	71726	≥ :	0.113	0.108					
48.52 48.52	10/01	\$ 3	0.104	0.016					
10.01	9071C	3							
50 03	96739	\$ 3	121.0	0.104					
50.49	10590	:3	0.079	0.016					
50.74	15302	3	960.0	0.023					
50.89	32699	3	0.120	0.049					
51.46	52244	3	0.140	0.079					
E0.25	13859	\$	0.083	0.021					
00.20	668539 66539	\$ 3	0.176	0.134					
53.73	10807	3	0.147	0.066					
54.20	50389	3	0.208	0.076					
54.78	29356	3	0.161	0.044					
55.15	16786	3	0.127	0.025					
55.51	66617	3	0.207	0.063					
56.21	15417	2	0.056	0.023					
56.23	22165 L	3	0.074	0.034					
56.71	29222	2	0.131	0.044					
57.65	32110	4	0.151	0.049					
60.19	82454	<b>4</b> i	0.189	0.125					
60.95 41 24	61936	2	0.159	0.094					
01 79	465.91		0.150	0.015					
65 11	17688	: \$	0.179	0.021					
65.50	62021	: <b>d</b>	0.179	0.124					

Table	A18

×

#### pH 9

	pH 9	,			
RUN # 79 WORKFILE ID: 000	9. ID: C	MA	7/01/86 ,WORKF1	,20:11:17 LE NAME:	
AREAS					
RT	AREA T	TPE .	AR/HT	AREAS	
checkpoin	t: the next	peak	10 Al;	subtract 0	.03 minutes
5.51	10/3/0	5P	0.212	0.147	
0.62	2482500	BV 110	0.201	3.394	
7.23	100100	VP Mu	0.190	0.257	
7.04	J4/33	VV	0.075	43 000	
7.07 <b>-</b>	330700	<b>V</b> V	0.347	02.777	
9,23	2257,50	vv	0.207	0.314	
9 84	188510	vv	0.237	0.310	
10 39	405280	ww	0.150	0.238	
10.35	466940	w	0 126	0.534	
10.70	288140	ww	0.120 0.130	0.038	
11 11	200600	vv	0 165	0.374	
12 03	49492	vv	0 213	0.048	
12.00	10572	VP	0.215	0.005	
12.94	17155	PV	0 108	0.014	
checkpoint	t the next	neak	1 A14	BT evect	
13 37	1678300	VR	0 117	2 294	
14.23	13118	PV	0 092	0 018	
14.43	16972	vv	0 073	0 023	
14.62	203540	vv	0 181	0 278	
14.90	121000	vv	0 165	0 165	
15.21	144930	vv	0 118	0 198	
15.32	112670	vv	0 115	0.154	
15.70	45981	BV	0 116	0 063	
15.85	57493	vv	0.133	0.079	
16.10	117160	V.	0.158	0 160	
checkpoint	t: the next	Deak	in AIR:	add 0.02	minutes
16.91	1683200	38	0.118	2.301	
17.69	15528	IV	0.141	0.021	
17.94	28169	VP	0.081	0.039	
19.38	27187	BV	0.096	0.037	
19.64	13652	vv	0.203	0.019	
20.55	11371	VP	0.172	0.016	
20.98	13666	PV	0.090	0.019	
21.77	22981	VV	0.154	0.031	
22.07	11144	VP	0.132	0.015	
22.62	19684	PV	0.134	0.027	
23.68	17907	VV	0.098	0.025	
23.81	31833	VV	0.181	0.044	
24.02	12525	VV	0.086	0.017	
24.13	29405	vv	0.084	0.040	
24.68	48951	VP	0.110	0.067	
25.14	640480	PV	0.107	0.876	
checkpoin	t: the next	peak	1# A25;	add 0.04	minutes

25.37	5806200	vv	0 147	7 918
25.75	187290 D	vv	0.081	0 254
25 85	92728 0	vv	0.056	0.117
26 01	149490	vv	0 110	0.127
26.01	103130	vv	0.110	0.204
26.11	67687 D	υv	0.075	0.141
20.21	83331		0.003	0.093
20.27	93/21	**	0.097	0.128
20.38	34004	**	0.058	0.075
20.4/	39991 0	~~	0.045	0.055
20.72	40641 B	vv	0.053	0.056
26.95	51605	vv	0.064	0.071
27.14	32606	vv	0.046	0.045
27.23	162900	VV	0.185	0.223
27.40	45240	vv	0.067	0.062
27.53	79594	VV	0.111	0.109
27.89	93031	vv	0.148	0.127
28.05	50339	vv	0.113	0.069
28.21	74818	vv	0.176	0.102
28.53	46546	VV	0.138	0.064
28.83	31437	VV	0.148	0.043
29.11	11348	VV .	0.076	0.016
29.93	66309	VP	0.163	0.091
30.30	14868	PP	0.116	0.020
30.56	53392	PP	0.186	0.073
31.23	502320	<b>PB</b>	0.118	0.687
31.72	12486	3P	0.082	0.017
32.05	40732	PV	0.125	0.056
32.42	18714	vv	0.124	0.026
32.59	51621	vv	0.192	0.071
32.87	27292	VV	0.123	0.037
33.07	54414	VV	0.095	0.074
33.25	18513	VV .	0.076	0.025
33.42	26237	VV	0.104	0.036
34.09	115010	vv	0.084	0.157
34.28	52585	VV	0.128	0.072
34.42	28468	VV	0.097	0.039
34.89	17699	vv	0.092	0.024
35.27	25185	PV	0.125	0.034
36.04	728380	VV	0.107	0.996
36.34	89844	VV	0.096	0.123
36.45	163630	VV	0.103	0.224
36.70	137780	VV	0.139	0.188
checkpoint	: the next	peak	is D3; add	0.04 minutes
36.97	671160	vv	0.091	0.918
37.22	27602	vv	0.092	0.038
37.39	144520	vv	0.134	0.198
37.60	104580	vv	0.108	0.143
37.83	16206	vv	0.101	0.022
38.00	20405	vv	0.102	0.028
38.21	20650	vv	0.109	0.028
38.63	12968	VP	0.097	0.018
39 08	214410	vv	0 101	0 293
39.30	74517	VP	0.134	0 102
10 80	1984600	PR	0 100	2 713

|          | 0.400  |  |   |  | 0 027   | 0.039  | 0.129   | 0.224  | 0.118  | 0.043   
   
   
   
  | 0.041  
   
   
   
  | 0.122   | 0.362  |   |   
   
   
   |  |   |  
  |  
   
   
  |   |  |   |  |  |   |  |   |  
   
   |   
   |   |  |  
   |   
   |   |  |   |  
  |  |  |   |   |  
   |   |   |   |  |
|----------|--|--|---|--|---|--|---|--|--
--
--
--
--
--
--
--
---	---
--
--
--
---|--|---|---
--
--
---
---|--|---|--|--|---|--|---
--
--
--|---|---|--
--
--|---|---|--
---
--
---	--	--	---	---
5	\$ 3	: 3	2	3
   
   
   
  | 3  
   
   
   
  | \$  | 2  | 58  | 3   
   
   
   |  |   |  
  |  
   
   
  |   |  |   |  |  |   |  |   |  
   
   |   
   |   |  |  
   |   
   |   |  |   | |
  |  |  |   |   |  
   |   |   |   |  |
|          | 1000C  | 11145  | 409630  | 41282  | 13514   | 20558  | 72384   | 12101  | 22083  | 10032   
   
   
   
  | 12147 D  
   
   
   
  | 12507   | 62700  | +20+10-1  |   
   
   
   |  |   |  
  |  
   
   
  |   |  |   |  |  |   |  |   |  
   
   |   
   |   |  |  
   |   
   |   |  |   | |
  |  |  |   |   |  
   |   |   |   |  |
|          | 07.6   | 66.0   | 2.66  | 7.17   | 7.20  | 7.23   | 7.26  | 8.49   | 2.84   | 2.89  
   
   
   
  | 2.96   
   
   
   
  | 4.94  | 6./3<br>TAI ABFA-  | L FACTOR  |   
   
   
   |  |   |  
  |  
   
   
  |   |  |   |  |  |   |  |   |  
   
   |   
   |   |  |  
   |   
   |   |  |   | |
  |  |  |   |   |  
   |   |   |   |  |
| <b>.</b> |  |  | •   | -  |   | -  | ~   | ~  | •  | •   
   
   
   
  | •  
   
   
   
  |   | Ĭ  |   |   
   
   
   |  |   |  
  |  
   
   
  |   |  |   |  |  |   |  |   |  
   
   |   
   |   |  |  
   |   
   |   |  |   | | | | | | | |
  |  |  |   |   |  
   |   |   |   |  |
|          |  |  |   |  |   |  |   |  |  |   
   
   
   
  |  
   
   
   
  |   |  |   |   
   
   
   |  |   |  
  |  
   
   
  |   |  |   |  |  |   |  |   |  
   
   |   
   |   |  |  
   |   
   |   |  |   | |
  |  |  |   |   |  
   |   |   |   |  |
| 0.015    | 0.822  | 0.113  | 0.057   | 0.064  | 0.031   | 0.050  | 0.039   | 0.034  | 0.067  | 0.019   
   
   
   
  | 0.025  
   
   
   
  | 0.019   | 0.015  | 0.056   | 0.110   
   
   
   | 0.069  | 0.048   | 0.031  
  | 0.044  
   
   
  | 0.045   | 0.082  | 0.022   | 0.049  | 0 090 0  | 0.021   | 0.066  | 0.104   | 0.126  
   
   | 0.202   
   | 0.053   | 0.201  | 0.141  
   | 0,140   
   | 0,040   | 0.168  | 0.177   | 0.048  
  | 0.138  | 0.028  | 0.044   | 0.014   | 0.015  
   | 0.051   | 0.074   | 0.099   | 0.021  |
| 0.117    | 0.165  | 0.162  | 0.166   | 0.143  | 0.102   | 0.095  | 001.0   | 0.072  | 0.122  | 190.0   
   
   
   
  | 0.090  
   
   
   
  | 0.102   | 0.096  | 0.111   | 0.205   
   
   
   | 0.137  | 0.125   | 0.101  
  | 0.150  
   
   
  | 0.150   | 0.217  | 0.087   | 0.096  | 0.142  | 0.046   | 0.128  | 0.153   | 0.196  
   
   | 0.205   
   | 0.070   | 0.192  | 0.171  
   | 0.179   
   | 0.061   | 607 D  | 0.263   | 0.105  
  | 0.209  | 0.162  | 0.146   | 0.092   | 0.186  
   | 0.139   | 0.239   | 0.186   | 162  |
| 2        | 3  | 2  | 3   | 3  | 3   | \$ ;   | \$ 3  |  | \$ !   | 23  
   
   
   
  | : 2  
   
   
   
  | :3  | 3  | \$  | 3   
   
   
   | 33   | :3  | 3  
  | 3  
   
   
  | 3   | 31   | 23  | \$ 3   | :3   | 3   | \$   | 3   | 3  
   
   | 3 :   
   | \$ 3  | :3   | 3  
   | 3   
   | <b>3</b> i  | \$ 3   | :3  | 3  
  | \$   | \$   | ٩P  | 3   | 3  
   | 4 ×   | 2 !   | 7   | 2  |
| 10980    | 601120   | 82270  | 41962   | 46558  | 02622   | 8/190  | 09597   |  | 00101  | 00501   
   
   
   
  | 11837  
   
   
   
  | 13673   | 10990  | 40728   | 80318   
   
   
   | 50734  | 34965   | 22486  
  | 32210  
   
   
  | 33032   | 60028  | 15695   | 06066  | 65778  | 15197   | 48429  | 75729   | 61616  
   
   | 147600  
   | 36513<br>144900   | 147050   | 103190   
   | 102100  
   | 29522   | 061671   | 129400  | 34855  
  | 100730   | 20192  | 32493   | 10080   | 12864  
   | 37575   | 53789   | ( 497 )   | 61907  |
| 1.12     | 1.41   | 2.82   | 6.6   | 5  | 2   | 2.12   | 777   |  |  | 7 . 7   
   
   
   
  | 6.20   
   
   
   
  | 6.82  | 0.03   | 7.16  | 3   
   
   
   | 8.   | 7.98  | 8.08   
  | 8.29   
   
   
  | 8.69  | 60.6   |   | 0 10   | 0.50   | 0.63  | 0.74   | 0.87  | 1.04   
   
   | 69.1  
   |   | 2.48   | 2.72   
   | 2.94  
   | 1.5   | 4 21 C   | 5.51  | 6.44   
  | 6.71   | 7.25   | 7.63  | 8.68  | 9.87   
   | 0.16  | 0.61  | 0.Y.0   | <b>0</b> 2. <b>1</b>   |
|          | 41.12 10980 PV 0.117 0.015 57 0.5 10 10 10 10 10 10 10 10 10 10 10 10 10 | 41.12 10900 PV 0.117 0.015 67.06 30887 VY 0.260<br>41.41 601120 VV 0.165 0.822 69.40 4378 VY 0.260 | 41.12 10990 PV 0.117 0.015 61.06 30887 VV 0.260<br>41.41 601120 VV 0.165 0.822 69.40 47728 VV 0.20<br>42.82 82270 PV 0.162 0.113 70.33 33148 VV 0.176 | 41.12 10990 PV 0.117 0.015 67.06 30887 VV 0.260<br>41.41 601120 VV 0.165 0.822 69.40 47928 VV 0.196<br>42.82 82270 PV 0.166 0.113 70.33 33187 VV 0.113<br>43.07 41962 VV 0.166 0.057 72.66 406470 PV 0.211 | 41.12 10990 PV 0.117 0.015 67.06 30887 VV 0.206<br>41.41 601120 VV 0.165 0.822 69.40 4.7928 VV 0.196<br>42.82 82202 VV 0.166 0.0113 70.33 33185 VV 0.117<br>43.07 41962 VV 0.166 0.007 72.66 409630 PV 0.232<br>43.35 46558 VV 0.143 0.064 77.17 41787 VV 0.023 | 41.12     10990     PV     0.117     0.015     67.06     30887     VV     0.201       41.41     601120     VV     0.165     0.822     69.40     47928     VV     0.196       42.82     82270     PV     0.113     70.33     33185     VV     0.113       42.35     41.952     PV     0.113     70.33     33185     VV     0.113       43.35     455.36     VV     0.166     0.057     77.17     41362     VV     0.093       43.35     22920     VV     0.102     0.031     77.21     41282     VV     0.093       43.35     22920     VV     0.102     0.031     77.21     41282     VV     0.039 | 41.12 10990 PV 0.117 0.015 67.06 3087 V 0.260<br>42.82 8220 PV 0.165 0.133 69.40 5728 V 0.196<br>42.82 8220 PV 0.165 0.133 70.33 3187 V 0.117<br>43.07 41962 V 0.166 0.057 77.17 41282 V 0.089<br>43.50 22920 V 0.163 0.064 77.17 41282 V 0.089<br>43.50 22920 V 0.095 0.050 77.12 133158 V 0.003 | 41.12     10990     PV     0.117     0.015     67.06     30887     V     0.266       41.41     601120     VV     0.165     0.812     V     0.196       42.82     82200     VV     0.165     0.113     70.33     33187     VV     0.196       43.07     41962     VV     0.166     0.057     72.66     409630     PV     0.232       43.50     4558     VV     0.166     0.051     77.17     41282     PV     0.232       43.50     22200     VV     0.102     0.051     77.17     41282     VV     0.023       43.72     36178     VV     0.102     0.050     77.20     13516     VV     0.033       43.72     36178     VV     0.050     0.033     77.20     13516     VV     0.033       44.42     28390     VV     0.033     77.26     23546     V8     0.033 | 41.12     10990     PV     0.117     0.015     67.06     30887     W     0.205       41.41     601120     V     0.165     0.822     69.40     4928     W     0.196       43.07     41962     W     0.165     0.057     70.33     33185     W     0.196       43.07     41962     W     0.166     0.057     72.66     409610     PV     0.232       43.35     46558     W     0.163     0.064     77.17     41282     W     0.233       43.50     22970     W     0.102     0.031     77.20     13514     W     0.033       44.42     28930     W     0.103     0.050     77.20     13514     W     0.023       44.42     28930     W     0.103     0.050     77.20     13514     W     0.023       44.42     28930     W     0.103     0.039     77.26     12101     V     0.123       44.42     28930     W     0.092     0.039     77.26     12101     V     0.123 | 41.12     10990     FV     0.117     0.015     67.06     30887     FV     0.202       41.41     601120     VV     0.165     0.822     69.40     4928     VV     0.196       42.82     82200     VV     0.165     0.812     0.113     59.40     49928     VV     0.196       43.07     41962     VV     0.166     0.057     72.66     409630     PV     0.232       43.05     4558     VV     0.162     0.051     77.17     41282     PV     0.033       43.50     22920     VV     0.102     0.051     77.17     41282     PV     0.033       43.72     36178     VV     0.102     0.050     77.23     20558     PV     0.033       44.42     28300     VV     0.102     0.039     77.26     20558     VV     0.123       44.54     24.54     24973     VV     0.122     0.039     77.26     20558     VV     0.123       44.54     24.54     24973     VV     0.122     0.057     77.26     20558     VV     0.123       44.54     24.54     24973     VV     0.122     0.035     77.26     20558     VV     0.123 </td <td>41.12     10990     PV     0.117     0.015     67.06     5087     V     0.126       42.182     PV     0.1120     PV     0.113     57.06     593.60     593.67     V     0.195       43.07     41962     VV     0.165     0.113     70.33     33185     VV     0.195       43.07     41962     VV     0.165     0.051     77.17     41282     VV     0.203       43.50     22920     VV     0.113     77.17     41282     VV     0.033       43.72     36178     VV     0.103     77.17     41282     VV     0.033       43.72     36178     VV     0.031     77.12     21354     VV     0.033       44.5     28930     VV     0.033     77.23     21354     VV     0.033       44.5     28930     VV     0.033     77.23     21364     VP     0.033       44.5     24.50     VV     0.033     77.26     72364     VP     0.033       44.5     24.50     VV     0.034     77.26     72364     VP     0.034       44.5     24.50     VV     0.034     0.034     77.26     72364     VP     0.035    <tr< td=""><td>41.112       10990       FV       0.117       0.015       67.06       30887       FV       0.205         41.41       601120       FV       0.165       0.822       69.46       59387       FV       0.196         43.07       41962       FV       0.165       0.812       FV       0.193       57.16       33185       FV       0.196         43.07       41962       FV       0.166       0.057       77.17       417.17       417.82       FV       0.233         43.50       27570       FV       0.102       0.051       77.17       41282       FV       0.023         43.72       36178       FV       0.102       0.051       77.17       41282       FV       0.023         43.72       36178       FV       0.102       0.051       77.26       23546       FV       0.033         44.42       28390       FV       0.033       77.26       72364       FV       0.234         44.42       24970       FV       0.033       77.26       73346       FV       0.234         44.42       24930       FV       0.033       0.034       77.26       7346       FV       0.234</td><td>41.112       10990       W       0.117       0.015       67.06       3087       W       0.201         41.41       601120       W       0.113       70.33       33187       W       0.196         43.07       41962       W       0.165       0.613       70.33       33187       W       0.196         43.07       41962       W       0.166       0.057       77.17       4328       W       0.232         43.53       46558       W       0.166       0.031       77.17       41382       W       0.023         43.50       27970       W       0.102       0.031       77.26       13514       W       0.023         43.75       36170       W       0.102       0.031       77.26       7396       W       0.023         44.42       28390       W       0.035       77.26       7396       W       0.023         44.70       48791       W       0.035       0.035       77.26       7396       W       0.224         44.72       28390       W       0.1027       0.035       77.26       7396       W       0.224         44.72       2890       W       0.</td><td>41.112       10990       W       0.117       0.015       67.06       3087       W       0.205         41.41       601120       W       0.165       0.822       69.40       579.8       W       0.195         43.07       41962       W       0.165       0.057       77.26       593.40       6.93.69       W       0.195         43.07       41962       W       0.166       0.057       77.26       409619       W       0.232         43.53       46558       W       0.166       0.051       77.26       13514       W       0.023         43.54       24973       W       0.103       0.039       77.26       13514       W       0.023         44.42       28390       W       0.103       0.039       77.26       13514       W       0.023         44.42       28390       W       0.102       0.039       77.26       72384       W       0.122         44.42       2890       0.030       77.26       72384       W       0.122         44.42       2800       W       0.039       77.26       72384       W       0.033         44.42       103000       W</td><td>41.12       10990       W       0.117       0.015       67.06       3087       W       0.205         42.82       82.70       W       0.115       0.013       70.33       31187       W       0.195         43.15       8270       W       0.165       0.057       70.33       31187       W       0.195         43.07       41962       W       0.166       0.057       70.33       31187       W       0.117         43.07       41962       W       0.166       0.051       77.17       41282       W       0.203         43.72       36178       W       0.166       0.050       77.17       41282       W       0.203         43.72       36178       W       0.095       0.050       77.26       13514       W       0.023         44.5       24971       W       0.095       0.054       77.26       12304       W       0.023         44.5       24971       W       0.012       0.014       82.84       12012       W       0.023         44.5       24971       W       0.012       0.014       82.84       12012       W       0.0124         44.5       <td< td=""><td>41.12     10980     PV     0.117     0.015     67.06     30837     VY     0.136       42.8     82.70     PV     0.1165     0.057     77.17     47.928     VY     0.195       42.07     41962     VY     0.165     0.057     77.17     47.928     VY     0.119       43.35     4558     VY     0.166     0.054     77.17     41282     VY     0.031       43.35     4558     VY     0.183     0.064     77.17     41282     VY     0.033       45.45     23930     VY     0.093     0.031     77.17     41282     VY     0.033       45.45     23930     VY     0.033     77.26     75.36     VY     0.033       45.45     23930    
VY     0.033     77.26     72364     VY     0.033       44.42     23910     VY     0.033     77.26     72364     VY     0.033       44.42     23910     VY     0.033     77.26     72364     VY     0.033       44.5     2391     VY     0.034     77.26     72364     VY     0.033       44.5     244     2003     VY     0.034     77.26     72364     VY     0.03</td><td>41.12       10980       FV       0.117       0.015       0.12       0.117       0.015         42.1       601120       FV       0.165       0.123       0.015       FV       0.196         42.1       82.20       FV       0.165       0.051       77.17       4.7928       FV       0.195         43.03       44558       VV       0.166       0.051       77.17       4.7928       VV       0.195         43.03       44558       VV       0.143       0.064       77.17       41282       VV       0.031         45.12       36178       VV       0.193       77.17       41282       VV       0.033         45.17       36178       VV       0.033       77.23       20354       VV       0.033         45.17       36178       VV       0.034       77.23       20354       VV       0.033         45.17       46170       40100       VV       0.034       77.23       20354       VV       0.033         45.17       40100       VV       0.034       77.23       20354       VV       0.033         46.70       40100       VV       0.034       77.23       20354</td><td>41.12       10980       PV       0.117       0.015       0.12       0.015         42.1       10110       V       0.116       0.015       0.117       0.019         42.1       10112       10115       0.015       0.113       70.05       30817       VV       0.195         42.07       11962       VV       0.165       0.051       70.117       417.32       VV       0.195         43.03       4558       VV       0.143       0.064       77.17       41282       VV       0.031         43.03       25920       VV       0.102       0.031       77.26       13516       VV       0.033         45.17       36178       VV       0.102       0.031       77.26       73345       VV       0.033         45.17       36178       VV       0.102       0.034       77.26       73345       VV       0.033         45.17       36170       VV       0.033       77.26       73345       VV       0.033         45.17       41700       VV       0.034       77.26       73345       VV       0.033         45.17       4180       VV       0.037       0.041       0.027</td><td>11.12       10980       FV       0.117       0.015       67.06       30837       W       0.136         22.81       82.70       FV       0.165       0.053       67.06       30837       W       0.195         22.07       41962       VV       0.165       0.053       67.06       30837       W       0.195         23.05       41962       VV       0.165       0.051       77.20       417.23       W       0.233         23.05       25920       VV       0.102       0.031       77.20       13516       VV       0.023         23.15       25930       VV       0.102       0.031       77.20       13516       VV       0.023         24.55       28130       VV       0.102       0.034       77.26       7236       VV       0.032         24.57       36170       VV       0.102       0.014       77.26       72364       VV       0.023         24.57       58170       VV       0.037       77.26       72364       VV       0.024         24.57       58100       VV       0.037       77.26       72364       VV       0.024         24.51       10300       <td< td=""><td>41.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         42.00       41962       VV       0.165       0.057       77.17       47928       VV       0.195         42.01       82.70       VV       0.165       0.057       77.17       47928       VV       0.195         43.55       VV       0.165       0.057       77.17       47928       VV       0.195         43.50       VV       0.143       0.054       77.17       41282       VV       0.203         43.77       23930       VV       0.193       77.26       4928       VV       0.203         44.2       23930       VV       0.102       0.033       77.26       7234       VP       0.234         45.5       23930       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.034       77.26       7234       VP       0.234         46.5       23931       VV       0.122</td></td<><td>11.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         22.01       82.20       PV       0.165       0.057       77.17       47928       W       0.195         23.05       82.20       W       0.165       0.057       77.17       47928       W       0.195         23.05       82.965       W       0.143       0.064       77.17       41282       W       0.137         23.05       22930       W       0.193       77.17       41282       W       0.039         23.72       23910       W       0.102       0.039       77.26       409510       W       0.013         23.72       23910       W       0.102       0.039       77.26       409510       W       0.033         24.5       23910       W       0.102       0.034       77.26       7234       W       0.033         24.5       2401       W       0.122       0.034       77.26       7236       W       0.033         24.5       2403       W       0.122       0.045       82.36       W       0.033         24.5       16610       W       0</td><td>11.12       10980       FV       0.117       0.015       0.125       0.135         12.61       60.1120       FV       0.165       0.057       77.17       0.0135       FV       0.113         12.07       61.962       VV       0.165       0.057       77.17       67.06       30817       VV       0.113         12.07       61.962       VV       0.165       0.054       77.17       41282       VV       0.136         12.17       36178       VV       0.183       0.004       77.17       41282       VV       0.033         12.17       36178       VV       0.193       77.26       13514       VV       0.033         12.17       36179       VV       0.103       77.26       72364       VV       0.033         12.16       1000       VV       0.034       77.26       72364       VV       0.033         14.72       23918       VV       0.035       77.26       72364       VV       0.034         14.72       2497       11877       VV       0.035       17.26       72364       VV       0.034         14.72       2497       11877       VV       0.035</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         12.13       10960       PV       0.117       0.015       0.117       0.019       VV       0.195       VV       0.023       VV       0.033       VV       0.034</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.116       0.013       VV       0.123         22.02       41962       VV       0.165       0.057       7.013       31318       VV       0.136         23.07       41962       VV       0.165       0.057       7.013       31318       VV       0.137         23.13       46558       VV       0.183       0.004       77.17       41282       VV       0.013         23.17       23930       VV       0.103       77.17       41282       VV       0.023         45.17       661.60       1097       VV       0.039       77.26       409510       VV       0.012         45.17       661.60       1090       VV       0.102       0.039       77.26       7234       VV       0.012         45.17       2003       0.039       77.26       7234       VV       0.023         46.17       4070       0.014       0.014       0.014       0.013       VV       0.012         46.17       4070       0.039       77.26       7234       VV       0.023         46.16       11837       VV</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.106       30807       VV       0.136         22.01       10120       VV       0.165       0.057       77.17       17.928       VV       0.195         23.03       45558       VV       0.165       0.057       77.17       41282       VV       0.195         43.05       VV       0.143       0.094       77.17       41282       VV       0.093         43.17       17       27.01       17.26       499510       VV       0.023         44.12       23930       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       7234       VV       0.023         44.12       23931       VV       0.122       0.043       0.014       0.023       VV       0.023         44.12       23931       VV       0.123       VV       0.123       VV       0.023         44.12       23910       &lt;</td><td>11.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         22.01       82.01120       W       0.185       0.053       77.17       17.928       W       0.193         23.03       82.50       W       0.185       0.054       77.17       41282       W       0.193         53.73       4558       W       0.185       0.054       77.17       41282       W       0.033         53.73       25930       W       0.193       77.17       41282       W       0.033         53.72       25931       W       0.102       0.034       77.26       72364       W       0.033         54.70       40       1002       0.034       77.26       72364       W       0.033         54.70       20100       W       0.112       0.014       0.023       W       0.033         54.71       20100       W       0.122       0.014       0.023       W       0.033         54.70       11837       W       0.122       0.014       0.023       W       0.033         54.71       11837       W       0.1022      
0.014       0.023</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         22.10       PV       0.116       0.051       77.17       17.17       17.17       0.196       0.019         23.13       41962       VV       0.165       0.051       77.17       41282       VV       0.193         23.73       45962       VV       0.166       0.031       77.17       41282       VV       0.031         23.75       23930       VV       0.103       0.031       77.26       409610       VV       0.033         24.42       23930       VV       0.103       0.034       77.26       409610       VV       0.033         24.42       23930       VV       0.103       77.26       2394       VV       0.033         24.42       23931       VV       0.034       77.26       7234       VV       0.033         24.42       23931       VV       0.034       77.26       7236       VV       0.033         24.43       71.000       11837       VV       0.034       77.26       7236       VV       0.033         24.43       11837       VV</td><td>11.12       10980       PV       0.117       0.015       0.0120       PV       0.117       0.019         12.01       10960       PV       0.117       0.015       0.113       17.17       17.33       17.928       VV       0.195         12.02       11962       VV       0.165       0.051       77.17       17.17       17.128       VV       0.013         12.12       25970       VV       0.185       0.031       77.26       12954       VV       0.033         12.12       25910       VV       0.102       0.033       77.26       12945       VV       0.033         12.12       25190       VV       0.103       0.034       77.26       12945       VV       0.033         12.12       10010       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       10100       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       11877       VV       0.035       0.014       0.023       VV       0.033         14.57       11877       VV       0.035       0.014       0.023<td>11.12       10980       Y       0.117       0.015       0.0120       Y       0.117       0.0136         22.01       10960       Y       0.117       0.015       0.057       Y       0.196         23.03       45558       Y       0.185       0.057       77.17       41282       Y       0.013         43.05       Y       0.183       0.094       77.17       41282       Y       0.013         43.17       17       27.01       17.26       40950       Y       0.023         44.2       23380       Y       0.039       77.26       409510       Y       0.013         44.12       23390       Y       0.123       0.039       77.26       409510       Y       0.013         44.12       23910       Y       0.122       0.039       77.26       7234       Y       0.013         44.15       2391       Y       0.122       0.014       0.013       Y       0.023         44.15       2391       Y       0.123       0.014       0.023       Y       0.023         44.15       2491       11837       Y       0.023       0.043       Y       0.023</td><td>41.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         42.1       10980       W       0.117       0.015       0.051       W       0.119         43.3       44558       W       0.143       0.054       77.17       41282       W       0.119         43.5       W       0.143       0.056       0.031       77.17       41282       W       0.013         43.7       17       17       17       17       17       41282       W       0.031         44.2       23910       W       0.102       0.034       77.26       1294       W       0.013         44.2       23910       W       0.122       0.034       77.26       1294       W       0.033         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.023         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.013         44.3       10000       W       0.122       0.014       0.023       W       0.013         45.3       11807       W       0.023       W</td><td>11.11       0.0100       W       0.117       0.015       0.012       W       0.119         0.1120       W       0.116       0.013       0.113       0.013       W       0.113         0.1120       W       0.165       0.057       0.051       17.17       0.1132       W       0.113         0.1120       W       0.165       0.051       77.17       0.1232       W       0.0133         0.1121       0.0102       0.0103       0.0114       0.0133       77.17       0.1232       W       0.023         0.1121       0.0102       0.0103       0.0104       0.0103       77.17       0.1232       W       0.023         0.1111       0.0103       W       0.1113       0.0114       0.013       W       0.0123         0.1187       W       0.0104       W       0.014       0.014       0.023       W       0.023         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       0.014</td><td>11.12       10980       W       0.117       0.015       0.015       0.015       0.016       0.013         0.2.01       W       0.165       0.015       0.013<td>11.11       10990       W       0.117       0.015       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.0</td><td>11.12       10000       W       0.117       0.005       0.061       0.011       0.0</td><td>11.12       10000       W       0.117       0.005       47.32       40.9630       W       0.126         0.130       4558       W       0.165       0.057       47.31       4136       W       0.133         0.130       4558       W       0.165       0.057       77.31       3136       W       0.133         0.130       4558       W       0.165       0.031       77.31       3136       W       0.031         0.131       W       0.095       0.031       77.33       21363       W       0.033         0.132       23930       W       0.032       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       0.034       9.136       0.043         0.145       23010       W       0.035       0.034       9.136       0.043       0.043         0.145       24710       W       0.035       0.034       9.136       0.043       0.043         0.145       113010       W       0.135       0.035</td><td>11.11       01030       W       0.117       0.005       W       0.105         12.12       01030       W       0.117       0.015     
 0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015</td><td>11.11       01000       W       0.117       0.005       W       0.105         12.10       W 1012       W       0.117       0.013       0.013       W       0.113         12.10       W 1012       W       0.105       0.003       77.11       11.135       W       0.105         12.10       W 1012       0.013       0.024       0.135       W       0.135       W       0.135         12.10       W 1012       0.013       0.012       0.013       77.13       11354       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2036       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2031       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 10.012       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 1187       W 10.012       W 10.012       <t< td=""><td>11.11       01090       W       0.117       0.005       W       0.105         12.12       01090       W       0.117       0.005       0.005       0.005         12.15       0.0120       W       0.116       0.005       0.015       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.012       0.012         12.15       0.0120       W       0.105       0.012       0.012       0.012       0.012         12.15       0.0120       W       0.102       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W</td><td>11.11       11.0900       W       0.117       0.015       0.133       0.061       W       0.126         12.510       W       0.116       0.015</td><td>11.11       01930       W       0.117       0.015       0.135       0.061       W       0.136         12.12       01300       W       0.116       0.017       72.26       0.061       W       0.136         12.15       0130       0135       0135       0135       W       0.135       0135       W       0.135         12.15       0130       W       0102       0131       0135       W       0.135         12.15       0130       W       0102       0135       W       0.135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       013</td><td>11.11       11.0900       W       0.117       0.015       0</td><td>11.11       10000       W       0.113       0.003       W       0.113       0.003       W       0.103         10.11       10000       W       0.113       0.003       77.20       0.003       77.31       W       0.103         10.12       1000       W       0.113       0.003       77.21       0.003       77.23<!--</td--><td>11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101</td><td>1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01</td><td>11.11       110700       W       0.113       0.005       0.</td><td>11.1       11000       W       111       0.001       W       0.013       W</td></td></t<></td></td></td></td></td<></td></tr<></td> | 41.12     10990     PV     0.117     0.015     67.06     5087     V     0.126       42.182     PV     0.1120     PV     0.113     57.06     593.60     593.67     V     0.195      
43.07     41962     VV     0.165     0.113     70.33     33185     VV     0.195       43.07     41962     VV     0.165     0.051     77.17     41282     VV     0.203       43.50     22920     VV     0.113     77.17     41282     VV     0.033       43.72     36178     VV     0.103     77.17     41282     VV     0.033       43.72     36178     VV     0.031     77.12     21354     VV     0.033       44.5     28930     VV     0.033     77.23     21354     VV     0.033       44.5     28930     VV     0.033     77.23     21364     VP     0.033       44.5     24.50     VV     0.033     77.26     72364     VP     0.033       44.5     24.50     VV     0.034     77.26     72364     VP     0.034       44.5     24.50     VV     0.034     0.034     77.26     72364     VP     0.035 <tr< td=""><td>41.112       10990       FV       0.117       0.015       67.06       30887       FV       0.205         41.41       601120       FV       0.165       0.822       69.46       59387       FV       0.196         43.07       41962       FV       0.165       0.812       FV       0.193       57.16       33185       FV       0.196         43.07       41962       FV       0.166       0.057       77.17       417.17       417.82       FV       0.233         43.50       27570       FV       0.102       0.051       77.17       41282       FV       0.023         43.72       36178       FV       0.102       0.051       77.17       41282       FV       0.023         43.72       36178       FV       0.102       0.051       77.26       23546       FV       0.033         44.42       28390       FV       0.033       77.26       72364       FV       0.234         44.42       24970       FV       0.033       77.26       73346       FV       0.234         44.42       24930       FV       0.033       0.034       77.26       7346       FV       0.234</td><td>41.112       10990       W       0.117       0.015       67.06       3087       W       0.201         41.41       601120       W       0.113       70.33       33187       W       0.196         43.07       41962       W       0.165       0.613       70.33       33187       W       0.196         43.07       41962       W       0.166       0.057       77.17       4328       W       0.232         43.53       46558       W       0.166       0.031       77.17       41382       W       0.023         43.50       27970       W       0.102       0.031       77.26       13514       W       0.023         43.75       36170       W       0.102       0.031       77.26       7396       W       0.023         44.42       28390       W       0.035       77.26       7396       W       0.023         44.70       48791       W       0.035       0.035       77.26       7396       W       0.224         44.72       28390       W       0.1027       0.035       77.26       7396       W       0.224         44.72       2890       W       0.</td><td>41.112       10990       W       0.117       0.015       67.06       3087       W       0.205         41.41       601120       W       0.165       0.822       69.40       579.8       W       0.195         43.07       41962       W       0.165       0.057       77.26       593.40       6.93.69       W       0.195         43.07       41962       W       0.166       0.057       77.26       409619       W       0.232         43.53       46558       W       0.166       0.051       77.26       13514       W       0.023         43.54       24973       W       0.103       0.039       77.26       13514       W       0.023         44.42       28390       W       0.103       0.039       77.26       13514       W       0.023         44.42       28390       W       0.102       0.039       77.26       72384       W       0.122         44.42       2890       0.030       77.26       72384       W       0.122         44.42       2800       W       0.039       77.26       72384       W       0.033         44.42       103000       W</td><td>41.12       10990       W       0.117       0.015       67.06       3087       W       0.205         42.82       82.70       W       0.115       0.013       70.33       31187       W       0.195         43.15       8270       W       0.165       0.057       70.33       31187       W       0.195         43.07       41962       W       0.166       0.057       70.33       31187       W       0.117         43.07       41962       W       0.166       0.051       77.17       41282       W       0.203         43.72       36178       W       0.166       0.050       77.17       41282       W       0.203         43.72       36178       W       0.095       0.050       77.26       13514       W       0.023         44.5       24971       W       0.095       0.054       77.26       12304       W       0.023         44.5       24971       W       0.012       0.014       82.84       12012       W       0.023         44.5       24971       W       0.012       0.014       82.84       12012       W       0.0124         44.5       <td< td=""><td>41.12     10980     PV     0.117     0.015     67.06     30837     VY     0.136       42.8     82.70     PV     0.1165     0.057     77.17     47.928     VY     0.195       42.07     41962     VY     0.165     0.057     77.17     47.928     VY     0.119       43.35     4558     VY     0.166     0.054     77.17     41282     VY     0.031       43.35     4558     VY     0.183     0.064     77.17     41282     VY     0.033       45.45     23930     VY     0.093     0.031     77.17     41282     VY     0.033       45.45     23930     VY     0.033     77.26     75.36     VY     0.033       45.45     23930     VY     0.033     77.26     72364     VY     0.033       44.42     23910     VY     0.033     77.26     72364     VY     0.033       44.42     23910     VY     0.033     77.26     72364     VY     0.033       44.5     2391     VY     0.034     77.26     72364     VY     0.033       44.5     244     2003     VY     0.034     77.26     72364     VY     0.03</td><td>41.12       10980       FV       0.117       0.015       0.12       0.117       0.015         42.1       601120       FV       0.165       0.123       0.015       FV       0.196         42.1       82.20       FV       0.165       0.051       77.17       4.7928       FV       0.195         43.03       44558       VV       0.166       0.051       77.17       4.7928       VV       0.195         43.03       44558       VV       0.143       0.064       77.17       41282       VV       0.031         45.12       36178       VV       0.193       77.17       41282       VV       0.033         45.17       36178       VV       0.033       77.23       20354       VV       0.033         45.17       36178       VV       0.034       77.23       20354       VV       0.033         45.17       46170       40100       VV       0.034       77.23       20354       VV       0.033         45.17       40100       VV       0.034       77.23       20354       VV       0.033         46.70       40100       VV       0.034       77.23       20354</td><td>41.12       10980       PV       0.117       0.015       0.12       0.015         42.1       10110       V       0.116       0.015       0.117       0.019         42.1       10112       10115       0.015       0.113       70.05       30817       VV       0.195         42.07       11962       VV       0.165       0.051       70.117       417.32       VV       0.195         43.03       4558       VV       0.143       0.064       77.17       41282       VV       0.031         43.03       25920       VV       0.102       0.031       77.26       13516       VV       0.033         45.17       36178       VV       0.102       0.031       77.26       73345       VV       0.033         45.17       36178       VV       0.102       0.034       77.26       73345       VV       0.033         45.17       36170       VV       0.033       77.26       73345       VV       0.033         45.17       41700       VV       0.034       77.26       73345       VV       0.033         45.17       4180       VV       0.037       0.041       0.027</td><td>11.12       10980       FV       0.117       0.015       67.06       30837       W       0.136         22.81       82.70       FV       0.165       0.053       67.06       30837       W       0.195         22.07       41962       VV       0.165       0.053       67.06       30837       W       0.195         23.05       41962       VV       0.165       0.051       77.20       417.23       W       0.233         23.05       25920       VV       0.102       0.031       77.20       13516       VV       0.023         23.15       25930       VV       0.102       0.031       77.20       13516       VV       0.023         24.55       28130       VV       0.102       0.034       77.26       7236       VV       0.032         24.57       36170       VV       0.102       0.014       77.26       72364       VV       0.023         24.57       58170       VV       0.037       77.26       72364       VV       0.024         24.57       58100       VV       0.037       77.26       72364       VV       0.024         24.51       10300       <td< td=""><td>41.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         42.00       41962       VV       0.165       0.057       77.17       47928       VV       0.195         42.01       82.70       VV       0.165       0.057       77.17       47928       VV       0.195         43.55       VV       0.165       0.057       77.17       47928       VV       0.195         43.50       VV       0.143       0.054       77.17       41282       VV       0.203         43.77       23930       VV       0.193       77.26       4928       VV       0.203         44.2       23930       VV       0.102       0.033       77.26       7234       VP       0.234         45.5       23930       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV      
0.122       0.034       77.26       7234       VP       0.234         46.5       23931       VV       0.122</td></td<><td>11.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         22.01       82.20       PV       0.165       0.057       77.17       47928       W       0.195         23.05       82.20       W       0.165       0.057       77.17       47928       W       0.195         23.05       82.965       W       0.143       0.064       77.17       41282       W       0.137         23.05       22930       W       0.193       77.17       41282       W       0.039         23.72       23910       W       0.102       0.039       77.26       409510       W       0.013         23.72       23910       W       0.102       0.039       77.26       409510       W       0.033         24.5       23910       W       0.102       0.034       77.26       7234       W       0.033         24.5       2401       W       0.122       0.034       77.26       7236       W       0.033         24.5       2403       W       0.122       0.045       82.36       W       0.033         24.5       16610       W       0</td><td>11.12       10980       FV       0.117       0.015       0.125       0.135         12.61       60.1120       FV       0.165       0.057       77.17       0.0135       FV       0.113         12.07       61.962       VV       0.165       0.057       77.17       67.06       30817       VV       0.113         12.07       61.962       VV       0.165       0.054       77.17       41282       VV       0.136         12.17       36178       VV       0.183       0.004       77.17       41282       VV       0.033         12.17       36178       VV       0.193       77.26       13514       VV       0.033         12.17       36179       VV       0.103       77.26       72364       VV       0.033         12.16       1000       VV       0.034       77.26       72364       VV       0.033         14.72       23918       VV       0.035       77.26       72364       VV       0.034         14.72       2497       11877       VV       0.035       17.26       72364       VV       0.034         14.72       2497       11877       VV       0.035</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         12.13       10960       PV       0.117       0.015       0.117       0.019       VV       0.195       VV       0.023       VV       0.033       VV       0.034</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.116       0.013       VV       0.123         22.02       41962       VV       0.165       0.057       7.013       31318       VV       0.136         23.07       41962       VV       0.165       0.057       7.013       31318       VV       0.137         23.13       46558       VV       0.183       0.004       77.17       41282       VV       0.013         23.17       23930       VV       0.103       77.17       41282       VV       0.023         45.17       661.60       1097       VV       0.039       77.26       409510       VV       0.012         45.17       661.60       1090       VV       0.102       0.039       77.26       7234       VV       0.012         45.17       2003       0.039       77.26       7234       VV       0.023         46.17       4070       0.014       0.014       0.014       0.013       VV       0.012         46.17       4070       0.039       77.26       7234       VV       0.023         46.16       11837       VV</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.106       30807       VV       0.136         22.01       10120       VV       0.165       0.057       77.17       17.928       VV       0.195         23.03       45558       VV       0.165       0.057       77.17       41282       VV       0.195         43.05       VV       0.143       0.094       77.17       41282       VV       0.093         43.17       17       27.01       17.26       499510       VV       0.023         44.12       23930       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       7234       VV       0.023         44.12       23931       VV       0.122       0.043       0.014       0.023       VV       0.023         44.12       23931       VV       0.123       VV       0.123       VV       0.023         44.12       23910       &lt;</td><td>11.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         22.01       82.01120       W       0.185       0.053       77.17       17.928       W       0.193         23.03       82.50       W       0.185       0.054       77.17       41282       W       0.193         53.73       4558       W       0.185       0.054       77.17       41282       W       0.033         53.73       25930       W       0.193       77.17       41282       W       0.033         53.72       25931       W       0.102       0.034       77.26       72364       W       0.033         54.70       40       1002       0.034       77.26       72364       W       0.033         54.70       20100       W       0.112       0.014       0.023       W       0.033         54.71       20100       W       0.122       0.014       0.023       W       0.033         54.70       11837       W       0.122       0.014       0.023       W       0.033         54.71       11837       W       0.1022       0.014       0.023</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         22.10       PV       0.116       0.051       77.17       17.17       17.17       0.196       0.019         23.13       41962       VV       0.165       0.051       77.17       41282       VV       0.193         23.73       45962       VV       0.166       0.031       77.17       41282       VV       0.031         23.75       23930       VV       0.103       0.031       77.26       409610       VV       0.033         24.42       23930       VV       0.103       0.034       77.26       409610       VV       0.033         24.42       23930       VV       0.103       77.26       2394       VV       0.033         24.42       23931       VV       0.034       77.26       7234       VV       0.033         24.42       23931       VV       0.034       77.26       7236       VV       0.033         24.43       71.000       11837       VV       0.034       77.26       7236       VV       0.033         24.43       11837       VV</td><td>11.12       10980       PV       0.117       0.015       0.0120       PV       0.117       0.019         12.01       10960       PV       0.117       0.015       0.113       17.17       17.33       17.928       VV       0.195         12.02       11962       VV       0.165       0.051       77.17       17.17       17.128       VV       0.013         12.12       25970       VV       0.185       0.031       77.26       12954       VV       0.033         12.12       25910       VV       0.102       0.033       77.26       12945       VV       0.033         12.12       25190       VV       0.103       0.034       77.26       12945       VV       0.033         12.12       10010       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       10100       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       11877       VV       0.035       0.014       0.023       VV       0.033         14.57       11877       VV       0.035       0.014       0.023<td>11.12       10980       Y       0.117       0.015       0.0120       Y       0.117       0.0136         22.01       10960       Y       0.117       0.015       0.057       Y       0.196         23.03       45558       Y       0.185       0.057       77.17       41282       Y       0.013         43.05       Y       0.183       0.094       77.17       41282       Y       0.013         43.17       17       27.01       17.26       40950       Y       0.023         44.2       23380       Y       0.039       77.26       409510       Y       0.013         44.12       23390       Y       0.123       0.039       77.26       409510       Y       0.013         44.12       23910       Y       0.122       0.039       77.26       7234       Y       0.013         44.15       2391       Y       0.122       0.014       0.013       Y       0.023         44.15       2391       Y       0.123       0.014       0.023       Y       0.023         44.15       2491       11837       Y       0.023       0.043       Y       0.023</td><td>41.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         42.1       10980       W       0.117       0.015       0.051       W       0.119         43.3       44558       W       0.143       0.054       77.17       41282       W       0.119         43.5       W       0.143       0.056       0.031       77.17       41282       W       0.013         43.7       17       17       17       17       17       41282       W       0.031         44.2       23910       W       0.102       0.034       77.26       1294       W       0.013         44.2       23910       W       0.122       0.034       77.26       1294       W       0.033         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.023         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.013         44.3       10000       W       0.122       0.014       0.023       W       0.013         45.3       11807       W       0.023       W</td><td>11.11       0.0100       W       0.117       0.015       0.012       W       0.119         0.1120       W       0.116       0.013       0.113       0.013       W       0.113         0.1120       W       0.165       0.057       0.051       17.17      
0.1132       W       0.113         0.1120       W       0.165       0.051       77.17       0.1232       W       0.0133         0.1121       0.0102       0.0103       0.0114       0.0133       77.17       0.1232       W       0.023         0.1121       0.0102       0.0103       0.0104       0.0103       77.17       0.1232       W       0.023         0.1111       0.0103       W       0.1113       0.0114       0.013       W       0.0123         0.1187       W       0.0104       W       0.014       0.014       0.023       W       0.023         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       0.014</td><td>11.12       10980       W       0.117       0.015       0.015       0.015       0.016       0.013         0.2.01       W       0.165       0.015       0.013<td>11.11       10990       W       0.117       0.015       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.0</td><td>11.12       10000       W       0.117       0.005       0.061       0.011       0.0</td><td>11.12       10000       W       0.117       0.005       47.32       40.9630       W       0.126         0.130       4558       W       0.165       0.057       47.31       4136       W       0.133         0.130       4558       W       0.165       0.057       77.31       3136       W       0.133         0.130       4558       W       0.165       0.031       77.31       3136       W       0.031         0.131       W       0.095       0.031       77.33       21363       W       0.033         0.132       23930       W       0.032       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       0.034       9.136       0.043         0.145       23010       W       0.035       0.034       9.136       0.043       0.043         0.145       24710       W       0.035       0.034       9.136       0.043       0.043         0.145       113010       W       0.135       0.035</td><td>11.11       01030       W       0.117       0.005       W       0.105         12.12       01030       W       0.117       0.015</td><td>11.11       01000       W       0.117       0.005       W       0.105         12.10       W 1012       W       0.117       0.013       0.013       W       0.113         12.10       W 1012       W       0.105       0.003       77.11       11.135       W       0.105         12.10       W 1012       0.013       0.024       0.135       W       0.135       W       0.135         12.10       W 1012       0.013       0.012       0.013       77.13       11354       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2036       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2031       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 10.012       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 1187       W 10.012       W 10.012       <t< td=""><td>11.11       01090       W       0.117       0.005       W       0.105         12.12       01090       W       0.117       0.005       0.005       0.005         12.15       0.0120       W       0.116       0.005       0.015       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.012       0.012         12.15       0.0120       W       0.105       0.012       0.012       0.012       0.012         12.15       0.0120       W       0.102       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W</td><td>11.11       11.0900       W       0.117       0.015       0.133       0.061       W       0.126         12.510       W       0.116       0.015</td><td>11.11       01930       W       0.117       0.015       0.135       0.061       W       0.136         12.12       01300       W       0.116       0.017       72.26       0.061       W       0.136         12.15       0130       0135       0135       0135       W       0.135       0135       W       0.135         12.15       0130       W       0102       0131       0135       W       0.135         12.15       0130       W       0102       0135       W       0.135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       013</td><td>11.11       11.0900       W       0.117    
  0.015       0</td><td>11.11       10000       W       0.113       0.003       W       0.113       0.003       W       0.103         10.11       10000       W       0.113       0.003       77.20       0.003       77.31       W       0.103         10.12       1000       W       0.113       0.003       77.21       0.003       77.23<!--</td--><td>11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101</td><td>1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01</td><td>11.11       110700       W       0.113       0.005       0.</td><td>11.1       11000       W       111       0.001       W       0.013       W</td></td></t<></td></td></td></td></td<></td></tr<> | 41.112       10990       FV       0.117       0.015       67.06       30887       FV       0.205         41.41       601120       FV       0.165       0.822       69.46       59387       FV       0.196         43.07       41962       FV       0.165       0.812       FV       0.193       57.16       33185       FV       0.196         43.07       41962       FV       0.166       0.057       77.17       417.17       417.82       FV       0.233         43.50       27570       FV       0.102       0.051       77.17       41282       FV       0.023         43.72       36178       FV       0.102       0.051       77.17       41282       FV       0.023         43.72       36178       FV       0.102       0.051       77.26       23546       FV       0.033         44.42       28390       FV       0.033       77.26       72364       FV       0.234         44.42       24970       FV       0.033       77.26       73346       FV       0.234         44.42       24930       FV       0.033       0.034       77.26       7346       FV       0.234 | 41.112       10990       W       0.117       0.015       67.06       3087       W       0.201         41.41       601120       W       0.113       70.33       33187       W       0.196         43.07       41962       W       0.165       0.613       70.33       33187       W       0.196         43.07       41962       W       0.166       0.057       77.17       4328       W       0.232         43.53       46558       W       0.166       0.031       77.17       41382       W       0.023         43.50       27970       W       0.102       0.031       77.26       13514       W       0.023         43.75       36170       W       0.102       0.031       77.26       7396       W       0.023         44.42       28390       W       0.035       77.26       7396       W       0.023         44.70       48791       W       0.035       0.035       77.26       7396       W       0.224         44.72       28390       W       0.1027       0.035       77.26       7396       W       0.224         44.72       2890       W       0. | 41.112       10990       W       0.117       0.015       67.06       3087       W       0.205         41.41       601120       W       0.165       0.822       69.40       579.8       W       0.195         43.07       41962       W       0.165       0.057       77.26       593.40       6.93.69       W       0.195         43.07       41962       W       0.166       0.057       77.26       409619       W       0.232         43.53       46558       W       0.166       0.051       77.26       13514       W       0.023         43.54       24973       W       0.103       0.039       77.26       13514       W       0.023         44.42       28390       W       0.103       0.039       77.26       13514       W       0.023         44.42       28390       W       0.102       0.039       77.26       72384       W       0.122         44.42       2890       0.030       77.26       72384       W       0.122         44.42       2800       W       0.039       77.26       72384       W       0.033         44.42       103000       W | 41.12       10990       W       0.117       0.015       67.06       3087       W       0.205         42.82       82.70       W       0.115       0.013       70.33       31187       W       0.195         43.15       8270       W       0.165       0.057       70.33       31187       W       0.195         43.07       41962       W       0.166       0.057       70.33       31187       W       0.117         43.07       41962       W       0.166       0.051       77.17       41282       W       0.203         43.72       36178       W       0.166       0.050       77.17       41282       W       0.203         43.72       36178       W       0.095       0.050       77.26       13514       W       0.023         44.5       24971       W       0.095       0.054       77.26       12304       W       0.023         44.5       24971       W       0.012       0.014       82.84       12012       W       0.023         44.5       24971       W       0.012       0.014       82.84       12012       W       0.0124         44.5 <td< td=""><td>41.12     10980     PV     0.117     0.015     67.06     30837     VY     0.136       42.8     82.70     PV     0.1165     0.057     77.17     47.928     VY     0.195       42.07     41962     VY     0.165     0.057     77.17     47.928     VY     0.119       43.35     4558     VY     0.166     0.054     77.17     41282     VY     0.031       43.35     4558     VY     0.183     0.064     77.17     41282     VY     0.033       45.45     23930     VY     0.093   
 0.031     77.17     41282     VY     0.033       45.45     23930     VY     0.033     77.26     75.36     VY     0.033       45.45     23930     VY     0.033     77.26     72364     VY     0.033       44.42     23910     VY     0.033     77.26     72364     VY     0.033       44.42     23910     VY     0.033     77.26     72364     VY     0.033       44.5     2391     VY     0.034     77.26     72364     VY     0.033       44.5     244     2003     VY     0.034     77.26     72364     VY     0.03</td><td>41.12       10980       FV       0.117       0.015       0.12       0.117       0.015         42.1       601120       FV       0.165       0.123       0.015       FV       0.196         42.1       82.20       FV       0.165       0.051       77.17       4.7928       FV       0.195         43.03       44558       VV       0.166       0.051       77.17       4.7928       VV       0.195         43.03       44558       VV       0.143       0.064       77.17       41282       VV       0.031         45.12       36178       VV       0.193       77.17       41282       VV       0.033         45.17       36178       VV       0.033       77.23       20354       VV       0.033         45.17       36178       VV       0.034       77.23       20354       VV       0.033         45.17       46170       40100       VV       0.034       77.23       20354       VV       0.033         45.17       40100       VV       0.034       77.23       20354       VV       0.033         46.70       40100       VV       0.034       77.23       20354</td><td>41.12       10980       PV       0.117       0.015       0.12       0.015         42.1       10110       V       0.116       0.015       0.117       0.019         42.1       10112       10115       0.015       0.113       70.05       30817       VV       0.195         42.07       11962       VV       0.165       0.051       70.117       417.32       VV       0.195         43.03       4558       VV       0.143       0.064       77.17       41282       VV       0.031         43.03       25920       VV       0.102       0.031       77.26       13516       VV       0.033         45.17       36178       VV       0.102       0.031       77.26       73345       VV       0.033         45.17       36178       VV       0.102       0.034       77.26       73345       VV       0.033         45.17       36170       VV       0.033       77.26       73345       VV       0.033         45.17       41700       VV       0.034       77.26       73345       VV       0.033         45.17       4180       VV       0.037       0.041       0.027</td><td>11.12       10980       FV       0.117       0.015       67.06       30837       W       0.136         22.81       82.70       FV       0.165       0.053       67.06       30837       W       0.195         22.07       41962       VV       0.165       0.053       67.06       30837       W       0.195         23.05       41962       VV       0.165       0.051       77.20       417.23       W       0.233         23.05       25920       VV       0.102       0.031       77.20       13516       VV       0.023         23.15       25930       VV       0.102       0.031       77.20       13516       VV       0.023         24.55       28130       VV       0.102       0.034       77.26       7236       VV       0.032         24.57       36170       VV       0.102       0.014       77.26       72364       VV       0.023         24.57       58170       VV       0.037       77.26       72364       VV       0.024         24.57       58100       VV       0.037       77.26       72364       VV       0.024         24.51       10300       <td< td=""><td>41.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         42.00       41962       VV       0.165       0.057       77.17       47928       VV       0.195         42.01       82.70       VV       0.165       0.057       77.17       47928       VV       0.195         43.55       VV       0.165       0.057       77.17       47928       VV       0.195         43.50       VV       0.143       0.054       77.17       41282       VV       0.203         43.77       23930       VV       0.193       77.26       4928       VV       0.203         44.2       23930       VV       0.102       0.033       77.26       7234       VP       0.234         45.5       23930       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.034       77.26       7234       VP       0.234         46.5       23931       VV       0.122</td></td<><td>11.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         22.01       82.20       PV       0.165       0.057       77.17       47928       W       0.195         23.05       82.20       W       0.165       0.057       77.17       47928       W       0.195         23.05       82.965       W       0.143       0.064       77.17       41282       W       0.137         23.05       22930       W       0.193       77.17       41282       W       0.039         23.72       23910       W       0.102       0.039       77.26       409510       W       0.013         23.72       23910       W       0.102       0.039       77.26       409510       W       0.033         24.5       23910       W       0.102       0.034       77.26       7234       W       0.033         24.5       2401       W       0.122       0.034       77.26       7236       W       0.033         24.5       2403       W       0.122       0.045       82.36       W       0.033         24.5       16610       W       0</td><td>11.12       10980       FV       0.117       0.015       0.125       0.135         12.61       60.1120       FV       0.165       0.057       77.17       0.0135       FV       0.113         12.07       61.962       VV       0.165       0.057       77.17       67.06       30817       VV       0.113         12.07       61.962       VV       0.165       0.054       77.17       41282       VV       0.136         12.17       36178       VV       0.183       0.004       77.17       41282       VV       0.033         12.17       36178       VV       0.193       77.26       13514       VV       0.033         12.17       36179       VV       0.103       77.26       72364       VV       0.033         12.16       1000       VV       0.034       77.26       72364       VV       0.033         14.72       23918       VV       0.035       77.26       72364       VV       0.034         14.72       2497       11877       VV       0.035       17.26       72364       VV       0.034         14.72       2497       11877       VV       0.035</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         12.13       10960       PV       0.117       0.015       0.117       0.019       VV       0.195       VV       0.023       VV       0.033       VV       0.034</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.116       0.013       VV       0.123         22.02       41962       VV       0.165       0.057       7.013       31318       VV       0.136         23.07       41962       VV       0.165       0.057       7.013       31318       VV       0.137         23.13       46558       VV       0.183       0.004       77.17       41282       VV       0.013         23.17       23930       VV       0.103       77.17       41282       VV       0.023         45.17       661.60       1097       VV       0.039       77.26       409510       VV       0.012         45.17       661.60       1090       VV       0.102       0.039       77.26       7234       VV       0.012         45.17       2003       0.039       77.26       7234       VV       0.023         46.17       4070       0.014       0.014       0.014       0.013       VV       0.012         46.17       4070       0.039       77.26       7234       VV       0.023         46.16       11837       VV</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.106       30807       VV       0.136         22.01       10120       VV       0.165       0.057       77.17       17.928       VV       0.195         23.03       45558       VV       0.165       0.057       77.17       41282       VV       0.195         43.05       VV       0.143       0.094       77.17       41282       VV       0.093         43.17       17       27.01       17.26       499510       VV       0.023         44.12       23930       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       7234       VV       0.023         44.12       23931       VV       0.122       0.043       0.014       0.023       VV       0.023         44.12       23931       VV       0.123       VV       0.123       VV       0.023         44.12       23910       &lt;</td><td>11.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         22.01       82.01120       W       0.185       0.053       77.17       17.928       W       0.193         23.03       82.50       W       0.185       0.054       77.17       41282       W       0.193         53.73       4558       W       0.185       0.054       77.17       41282       W       0.033         53.73       25930       W       0.193       77.17       41282       W       0.033         53.72       25931       W       0.102       0.034       77.26       72364       W       0.033         54.70       40       1002       0.034       77.26       72364       W       0.033         54.70       20100       W       0.112       0.014       0.023       W       0.033         54.71       20100       W       0.122       0.014       0.023       W      
0.033         54.70       11837       W       0.122       0.014       0.023       W       0.033         54.71       11837       W       0.1022       0.014       0.023</td><td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         22.10       PV       0.116       0.051       77.17       17.17       17.17       0.196       0.019         23.13       41962       VV       0.165       0.051       77.17       41282       VV       0.193         23.73       45962       VV       0.166       0.031       77.17       41282       VV       0.031         23.75       23930       VV       0.103       0.031       77.26       409610       VV       0.033         24.42       23930       VV       0.103       0.034       77.26       409610       VV       0.033         24.42       23930       VV       0.103       77.26       2394       VV       0.033         24.42       23931       VV       0.034       77.26       7234       VV       0.033         24.42       23931       VV       0.034       77.26       7236       VV       0.033         24.43       71.000       11837       VV       0.034       77.26       7236       VV       0.033         24.43       11837       VV</td><td>11.12       10980       PV       0.117       0.015       0.0120       PV       0.117       0.019         12.01       10960       PV       0.117       0.015       0.113       17.17       17.33       17.928       VV       0.195         12.02       11962       VV       0.165       0.051       77.17       17.17       17.128       VV       0.013         12.12       25970       VV       0.185       0.031       77.26       12954       VV       0.033         12.12       25910       VV       0.102       0.033       77.26       12945       VV       0.033         12.12       25190       VV       0.103       0.034       77.26       12945       VV       0.033         12.12       10010       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       10100       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       11877       VV       0.035       0.014       0.023       VV       0.033         14.57       11877       VV       0.035       0.014       0.023<td>11.12       10980       Y       0.117       0.015       0.0120       Y       0.117       0.0136         22.01       10960       Y       0.117       0.015       0.057       Y       0.196         23.03       45558       Y       0.185       0.057       77.17       41282       Y       0.013         43.05       Y       0.183       0.094       77.17       41282       Y       0.013         43.17       17       27.01       17.26       40950       Y       0.023         44.2       23380       Y       0.039       77.26       409510       Y       0.013         44.12       23390       Y       0.123       0.039       77.26       409510       Y       0.013         44.12       23910       Y       0.122       0.039       77.26       7234       Y       0.013         44.15       2391       Y       0.122       0.014       0.013       Y       0.023         44.15       2391       Y       0.123       0.014       0.023       Y       0.023         44.15       2491       11837       Y       0.023       0.043       Y       0.023</td><td>41.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         42.1       10980       W       0.117       0.015       0.051       W       0.119         43.3       44558       W       0.143       0.054       77.17       41282       W       0.119         43.5       W       0.143       0.056       0.031       77.17       41282       W       0.013         43.7       17       17       17       17       17       41282       W       0.031         44.2       23910       W       0.102       0.034       77.26       1294       W       0.013         44.2       23910       W       0.122       0.034       77.26       1294       W       0.033         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.023         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.013         44.3       10000       W       0.122       0.014       0.023       W       0.013         45.3       11807       W       0.023       W</td><td>11.11       0.0100       W       0.117       0.015       0.012       W       0.119         0.1120       W       0.116       0.013       0.113       0.013       W       0.113         0.1120       W       0.165       0.057       0.051       17.17       0.1132       W       0.113         0.1120       W       0.165       0.051       77.17       0.1232       W       0.0133         0.1121       0.0102       0.0103       0.0114       0.0133       77.17       0.1232       W       0.023         0.1121       0.0102       0.0103       0.0104       0.0103       77.17       0.1232       W       0.023         0.1111       0.0103       W       0.1113       0.0114       0.013       W       0.0123         0.1187       W       0.0104       W       0.014       0.014       0.023       W       0.023         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       0.014</td><td>11.12       10980       W       0.117       0.015       0.015       0.015       0.016       0.013         0.2.01       W       0.165       0.015       0.013<td>11.11       10990       W       0.117       0.015       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.0</td><td>11.12       10000       W       0.117       0.005       0.061       0.011       0.0</td><td>11.12       10000       W       0.117       0.005       47.32       40.9630       W       0.126         0.130       4558       W       0.165       0.057       47.31       4136       W       0.133         0.130       4558       W       0.165       0.057       77.31       3136       W       0.133         0.130       4558       W       0.165       0.031       77.31       3136       W       0.031         0.131       W       0.095       0.031       77.33       21363       W       0.033         0.132       23930       W       0.032       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       0.034       9.136       0.043         0.145       23010       W       0.035       0.034       9.136       0.043       0.043         0.145       24710       W       0.035       0.034       9.136       0.043       0.043         0.145       113010       W       0.135       0.035</td><td>11.11       01030       W       0.117       0.005       W       0.105         12.12       01030       W       0.117       0.015
      0.015       0.015</td><td>11.11       01000       W       0.117       0.005       W       0.105         12.10       W 1012       W       0.117       0.013       0.013       W       0.113         12.10       W 1012       W       0.105       0.003       77.11       11.135       W       0.105         12.10       W 1012       0.013       0.024       0.135       W       0.135       W       0.135         12.10       W 1012       0.013       0.012       0.013       77.13       11354       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2036       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2031       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 10.012       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 1187       W 10.012       W 10.012       <t< td=""><td>11.11       01090       W       0.117       0.005       W       0.105         12.12       01090       W       0.117       0.005       0.005       0.005         12.15       0.0120       W       0.116       0.005       0.015       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.012       0.012         12.15       0.0120       W       0.105       0.012       0.012       0.012       0.012         12.15       0.0120       W       0.102       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W</td><td>11.11       11.0900       W       0.117       0.015       0.133       0.061       W       0.126         12.510       W       0.116       0.015</td><td>11.11       01930       W       0.117       0.015       0.135       0.061       W       0.136         12.12       01300       W       0.116       0.017       72.26       0.061       W       0.136         12.15       0130       0135       0135       0135       W       0.135       0135       W       0.135         12.15       0130       W       0102       0131       0135       W       0.135         12.15       0130       W       0102       0135       W       0.135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       013</td><td>11.11       11.0900       W       0.117       0.015       0</td><td>11.11       10000       W       0.113       0.003       W       0.113       0.003       W       0.103         10.11       10000       W       0.113       0.003       77.20       0.003       77.31       W       0.103         10.12       1000       W       0.113       0.003       77.21       0.003       77.23<!--</td--><td>11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101</td><td>1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01</td><td>11.11       110700       W       0.113       0.005       0.</td><td>11.1       11000       W       111       0.001       W       0.013       W</td></td></t<></td></td></td></td></td<> | 41.12     10980     PV     0.117     0.015    
67.06     30837     VY     0.136       42.8     82.70     PV     0.1165     0.057     77.17     47.928     VY     0.195       42.07     41962     VY     0.165     0.057     77.17     47.928     VY     0.119       43.35     4558     VY     0.166     0.054     77.17     41282     VY     0.031       43.35     4558     VY     0.183     0.064     77.17     41282     VY     0.033       45.45     23930     VY     0.093     0.031     77.17     41282     VY     0.033       45.45     23930     VY     0.033     77.26     75.36     VY     0.033       45.45     23930     VY     0.033     77.26     72364     VY     0.033       44.42     23910     VY     0.033     77.26     72364     VY     0.033       44.42     23910     VY     0.033     77.26     72364     VY     0.033       44.5     2391     VY     0.034     77.26     72364     VY     0.033       44.5     244     2003     VY     0.034     77.26     72364     VY     0.03 | 41.12       10980       FV       0.117       0.015       0.12       0.117       0.015         42.1       601120       FV       0.165       0.123       0.015       FV       0.196         42.1       82.20       FV       0.165       0.051       77.17       4.7928       FV       0.195         43.03       44558       VV       0.166       0.051       77.17       4.7928       VV       0.195         43.03       44558       VV       0.143       0.064       77.17       41282       VV       0.031         45.12       36178       VV       0.193       77.17       41282       VV       0.033         45.17       36178       VV       0.033       77.23       20354       VV       0.033         45.17       36178       VV       0.034       77.23       20354       VV       0.033         45.17       46170       40100       VV       0.034       77.23       20354       VV       0.033         45.17       40100       VV       0.034       77.23       20354       VV       0.033         46.70       40100       VV       0.034       77.23       20354 | 41.12       10980       PV       0.117       0.015       0.12       0.015         42.1       10110       V       0.116       0.015       0.117       0.019         42.1       10112       10115       0.015       0.113       70.05       30817       VV       0.195         42.07       11962       VV       0.165       0.051       70.117       417.32       VV       0.195         43.03       4558       VV       0.143       0.064       77.17       41282       VV       0.031         43.03       25920       VV       0.102       0.031       77.26       13516       VV       0.033         45.17       36178       VV       0.102       0.031       77.26       73345       VV       0.033         45.17       36178       VV       0.102       0.034       77.26       73345       VV       0.033         45.17       36170       VV       0.033       77.26       73345       VV       0.033         45.17       41700       VV       0.034       77.26       73345       VV       0.033         45.17       4180       VV       0.037       0.041       0.027 | 11.12       10980       FV       0.117       0.015       67.06       30837       W       0.136         22.81       82.70       FV       0.165       0.053       67.06       30837       W       0.195         22.07       41962       VV       0.165       0.053       67.06       30837       W       0.195         23.05       41962       VV       0.165       0.051       77.20       417.23       W       0.233         23.05       25920       VV       0.102       0.031       77.20       13516       VV       0.023         23.15       25930       VV       0.102       0.031       77.20       13516       VV       0.023         24.55       28130       VV       0.102       0.034       77.26       7236       VV       0.032         24.57       36170       VV       0.102       0.014       77.26       72364       VV       0.023         24.57       58170       VV       0.037       77.26       72364       VV       0.024         24.57       58100       VV       0.037       77.26       72364       VV       0.024         24.51       10300 <td< td=""><td>41.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         42.00       41962       VV       0.165       0.057       77.17       47928       VV       0.195         42.01       82.70       VV       0.165       0.057       77.17       47928       VV       0.195         43.55       VV       0.165       0.057       77.17       47928       VV       0.195         43.50       VV       0.143       0.054       77.17       41282       VV       0.203         43.77       23930       VV       0.193       77.26       4928       VV       0.203         44.2       23930       VV       0.102       0.033       77.26       7234       VP       0.234         45.5       23930       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.034       77.26       7234       VP       0.234         46.5       23931       VV       0.122</td></td<> <td>11.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         22.01       82.20       PV       0.165       0.057       77.17       47928       W       0.195         23.05       82.20       W       0.165       0.057       77.17       47928       W       0.195         23.05       82.965       W       0.143       0.064       77.17       41282       W       0.137         23.05       22930       W       0.193       77.17       41282       W       0.039         23.72       23910       W       0.102       0.039       77.26       409510       W       0.013         23.72       23910       W       0.102       0.039       77.26       409510       W       0.033         24.5       23910       W       0.102       0.034       77.26       7234       W       0.033         24.5       2401       W       0.122       0.034       77.26       7236       W       0.033         24.5       2403       W       0.122       0.045       82.36       W       0.033         24.5       16610       W       0</td> <td>11.12       10980       FV       0.117       0.015       0.125       0.135         12.61       60.1120       FV       0.165       0.057       77.17       0.0135       FV       0.113         12.07       61.962       VV       0.165       0.057       77.17       67.06       30817       VV       0.113         12.07       61.962       VV       0.165       0.054       77.17       41282       VV       0.136         12.17       36178       VV       0.183       0.004       77.17       41282       VV       0.033         12.17       36178       VV       0.193       77.26       13514       VV       0.033         12.17       36179       VV       0.103       77.26       72364       VV       0.033         12.16       1000       VV       0.034       77.26       72364       VV       0.033         14.72       23918       VV       0.035       77.26       72364       VV       0.034         14.72       2497       11877       VV       0.035       17.26       72364       VV       0.034         14.72       2497       11877       VV       0.035</td> <td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         12.13       10960       PV       0.117       0.015       0.117       0.019       VV       0.195       VV       0.023       VV       0.033       VV       0.034</td> <td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.116       0.013       VV       0.123         22.02       41962       VV       0.165       0.057       7.013       31318       VV       0.136         23.07       41962       VV       0.165       0.057       7.013       31318       VV       0.137         23.13       46558       VV       0.183       0.004       77.17       41282       VV       0.013         23.17       23930       VV       0.103       77.17       41282       VV       0.023         45.17       661.60       1097       VV       0.039       77.26       409510       VV       0.012         45.17       661.60       1090       VV       0.102       0.039       77.26       7234       VV       0.012         45.17       2003       0.039       77.26       7234       VV       0.023         46.17       4070       0.014       0.014       0.014       0.013       VV       0.012         46.17       4070       0.039       77.26       7234       VV       0.023         46.16       11837       VV</td> <td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.106       30807       VV       0.136         22.01       10120       VV       0.165       0.057       77.17       17.928       VV       0.195         23.03       45558       VV       0.165       0.057       77.17       41282       VV       0.195         43.05       VV       0.143       0.094       77.17       41282       VV       0.093         43.17       17       27.01       17.26       499510       VV       0.023         44.12       23930       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       7234       VV       0.023         44.12       23931       VV       0.122       0.043       0.014       0.023       VV       0.023         44.12       23931       VV       0.123       VV       0.123       VV       0.023         44.12       23910       &lt;</td> <td>11.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         22.01       82.01120       W       0.185       0.053       77.17       17.928       W       0.193         23.03       82.50       W       0.185       0.054       77.17       41282       W       0.193         53.73       4558       W       0.185       0.054       77.17       41282       W       0.033         53.73       25930       W       0.193       77.17
      41282       W       0.033         53.72       25931       W       0.102       0.034       77.26       72364       W       0.033         54.70       40       1002       0.034       77.26       72364       W       0.033         54.70       20100       W       0.112       0.014       0.023       W       0.033         54.71       20100       W       0.122       0.014       0.023       W       0.033         54.70       11837       W       0.122       0.014       0.023       W       0.033         54.71       11837       W       0.1022       0.014       0.023</td> <td>11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         22.10       PV       0.116       0.051       77.17       17.17       17.17       0.196       0.019         23.13       41962       VV       0.165       0.051       77.17       41282       VV       0.193         23.73       45962       VV       0.166       0.031       77.17       41282       VV       0.031         23.75       23930       VV       0.103       0.031       77.26       409610       VV       0.033         24.42       23930       VV       0.103       0.034       77.26       409610       VV       0.033         24.42       23930       VV       0.103       77.26       2394       VV       0.033         24.42       23931       VV       0.034       77.26       7234       VV       0.033         24.42       23931       VV       0.034       77.26       7236       VV       0.033         24.43       71.000       11837       VV       0.034       77.26       7236       VV       0.033         24.43       11837       VV</td> <td>11.12       10980       PV       0.117       0.015       0.0120       PV       0.117       0.019         12.01       10960       PV       0.117       0.015       0.113       17.17       17.33       17.928       VV       0.195         12.02       11962       VV       0.165       0.051       77.17       17.17       17.128       VV       0.013         12.12       25970       VV       0.185       0.031       77.26       12954       VV       0.033         12.12       25910       VV       0.102       0.033       77.26       12945       VV       0.033         12.12       25190       VV       0.103       0.034       77.26       12945       VV       0.033         12.12       10010       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       10100       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       11877       VV       0.035       0.014       0.023       VV       0.033         14.57       11877       VV       0.035       0.014       0.023<td>11.12       10980       Y       0.117       0.015       0.0120       Y       0.117       0.0136         22.01       10960       Y       0.117       0.015       0.057       Y       0.196         23.03       45558       Y       0.185       0.057       77.17       41282       Y       0.013         43.05       Y       0.183       0.094       77.17       41282       Y       0.013         43.17       17       27.01       17.26       40950       Y       0.023         44.2       23380       Y       0.039       77.26       409510       Y       0.013         44.12       23390       Y       0.123       0.039       77.26       409510       Y       0.013         44.12       23910       Y       0.122       0.039       77.26       7234       Y       0.013         44.15       2391       Y       0.122       0.014       0.013       Y       0.023         44.15       2391       Y       0.123       0.014       0.023       Y       0.023         44.15       2491       11837       Y       0.023       0.043       Y       0.023</td><td>41.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         42.1       10980       W       0.117       0.015       0.051       W       0.119         43.3       44558       W       0.143       0.054       77.17       41282       W       0.119         43.5       W       0.143       0.056       0.031       77.17       41282       W       0.013         43.7       17       17       17       17       17       41282       W       0.031         44.2       23910       W       0.102       0.034       77.26       1294       W       0.013         44.2       23910       W       0.122       0.034       77.26       1294       W       0.033         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.023         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.013         44.3       10000       W       0.122       0.014       0.023       W       0.013         45.3       11807       W       0.023       W</td><td>11.11       0.0100       W       0.117       0.015       0.012       W       0.119         0.1120       W       0.116       0.013       0.113       0.013       W       0.113         0.1120       W       0.165       0.057       0.051       17.17       0.1132       W       0.113         0.1120       W       0.165       0.051       77.17       0.1232       W       0.0133         0.1121       0.0102       0.0103       0.0114       0.0133       77.17       0.1232       W       0.023         0.1121       0.0102       0.0103       0.0104       0.0103       77.17       0.1232       W       0.023         0.1111       0.0103       W       0.1113       0.0114       0.013       W       0.0123         0.1187       W       0.0104       W       0.014       0.014       0.023       W       0.023         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       0.014</td><td>11.12       10980       W       0.117       0.015       0.015       0.015       0.016       0.013         0.2.01       W       0.165       0.015       0.013<td>11.11       10990       W       0.117       0.015       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.0</td><td>11.12       10000       W       0.117       0.005       0.061       0.011       0.0</td><td>11.12       10000       W       0.117       0.005       47.32       40.9630       W       0.126         0.130       4558       W       0.165       0.057       47.31       4136       W       0.133         0.130       4558       W       0.165       0.057       77.31       3136       W       0.133         0.130       4558       W       0.165       0.031       77.31       3136       W       0.031         0.131       W       0.095       0.031       77.33       21363       W       0.033         0.132       23930       W       0.032       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       0.034       9.136       0.043         0.145       23010       W       0.035       0.034       9.136       0.043       0.043         0.145       24710       W       0.035       0.034       9.136       0.043       0.043         0.145       113010       W       0.135       0.035</td><td>11.11       01030       W       0.117       0.005       W       0.105         12.12       01030       W       0.117       0.015      
0.015       0.015</td><td>11.11       01000       W       0.117       0.005       W       0.105         12.10       W 1012       W       0.117       0.013       0.013       W       0.113         12.10       W 1012       W       0.105       0.003       77.11       11.135       W       0.105         12.10       W 1012       0.013       0.024       0.135       W       0.135       W       0.135         12.10       W 1012       0.013       0.012       0.013       77.13       11354       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2036       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2031       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 10.012       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 1187       W 10.012       W 10.012       <t< td=""><td>11.11       01090       W       0.117       0.005       W       0.105         12.12       01090       W       0.117       0.005       0.005       0.005         12.15       0.0120       W       0.116       0.005       0.015       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.012       0.012         12.15       0.0120       W       0.105       0.012       0.012       0.012       0.012         12.15       0.0120       W       0.102       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W</td><td>11.11       11.0900       W       0.117       0.015       0.133       0.061       W       0.126         12.510       W       0.116       0.015</td><td>11.11       01930       W       0.117       0.015       0.135       0.061       W       0.136         12.12       01300       W       0.116       0.017       72.26       0.061       W       0.136         12.15       0130       0135       0135       0135       W       0.135       0135       W       0.135         12.15       0130       W       0102       0131       0135       W       0.135         12.15       0130       W       0102       0135       W       0.135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       013</td><td>11.11       11.0900       W       0.117       0.015       0</td><td>11.11       10000       W       0.113       0.003       W       0.113       0.003       W       0.103         10.11       10000       W       0.113       0.003       77.20       0.003       77.31       W       0.103         10.12       1000       W       0.113       0.003       77.21       0.003       77.23<!--</td--><td>11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101</td><td>1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01</td><td>11.11       110700       W       0.113       0.005      
0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.005       0.</td><td>11.1       11000       W       111       0.001       W       0.013       W</td></td></t<></td></td></td> | 41.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         42.00       41962       VV       0.165       0.057       77.17       47928       VV       0.195         42.01       82.70       VV       0.165       0.057       77.17       47928       VV       0.195         43.55       VV       0.165       0.057       77.17       47928       VV       0.195         43.50       VV       0.143       0.054       77.17       41282       VV       0.203         43.77       23930       VV       0.193       77.26       4928       VV       0.203         44.2       23930       VV       0.102       0.033       77.26       7234       VP       0.234         45.5       23930       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.033       77.26       7234       VP       0.234         46.5       23931       VV       0.122       0.034       77.26       7234       VP       0.234         46.5       23931       VV       0.122 | 11.12       10980       PV       0.117       0.015       67.06       30837       W       0.136         22.01       82.20       PV       0.165       0.057       77.17       47928       W       0.195         23.05       82.20       W       0.165       0.057       77.17       47928       W       0.195         23.05       82.965       W       0.143       0.064       77.17       41282       W       0.137         23.05       22930       W       0.193       77.17       41282       W       0.039         23.72       23910       W       0.102       0.039       77.26       409510       W       0.013         23.72       23910       W       0.102       0.039       77.26       409510       W       0.033         24.5       23910       W       0.102       0.034       77.26       7234       W       0.033         24.5       2401       W       0.122       0.034       77.26       7236       W       0.033         24.5       2403       W       0.122       0.045       82.36       W       0.033         24.5       16610       W       0 | 11.12       10980       FV       0.117       0.015       0.125       0.135         12.61       60.1120       FV       0.165       0.057       77.17       0.0135       FV       0.113         12.07       61.962       VV       0.165       0.057       77.17       67.06       30817       VV       0.113         12.07       61.962       VV       0.165       0.054       77.17       41282       VV       0.136         12.17       36178       VV       0.183       0.004       77.17       41282       VV       0.033         12.17       36178       VV       0.193       77.26       13514       VV       0.033         12.17       36179       VV       0.103       77.26       72364       VV       0.033         12.16       1000       VV       0.034       77.26       72364       VV       0.033         14.72       23918       VV       0.035       77.26       72364       VV       0.034         14.72       2497       11877       VV       0.035       17.26       72364       VV       0.034         14.72       2497       11877       VV       0.035 | 11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         12.13       10960       PV       0.117       0.015       0.117       0.019       VV       0.195       VV       0.023       VV       0.033       VV       0.034 | 11.12       10980       PV       0.117       0.015       0.0120       VV       0.116       0.013       VV       0.123         22.02       41962       VV       0.165       0.057       7.013       31318       VV       0.136         23.07       41962       VV       0.165       0.057       7.013       31318       VV       0.137         23.13       46558       VV       0.183       0.004       77.17       41282       VV       0.013         23.17       23930       VV       0.103       77.17       41282       VV       0.023         45.17       661.60       1097       VV       0.039       77.26       409510       VV       0.012         45.17       661.60       1090       VV       0.102       0.039       77.26       7234       VV       0.012         45.17       2003       0.039       77.26       7234       VV       0.023         46.17       4070       0.014       0.014       0.014       0.013       VV       0.012         46.17       4070       0.039       77.26       7234       VV       0.023         46.16       11837       VV | 11.12       10980       PV       0.117       0.015       0.0120       VV       0.106       30807       VV       0.136         22.01       10120       VV       0.165       0.057       77.17       17.928       VV       0.195         23.03       45558       VV       0.165       0.057       77.17       41282       VV       0.195         43.05       VV       0.143       0.094       77.17       41282       VV       0.093         43.17       17       27.01       17.26       499510       VV       0.023         44.12       23930       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       499510       VV       0.013         44.12       23931       VV       0.102       0.039       77.26       7234       VV       0.023         44.12       23931       VV       0.122       0.043       0.014       0.023       VV       0.023         44.12       23931       VV       0.123       VV       0.123       VV       0.023         44.12       23910       < | 11.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         22.01       82.01120       W       0.185       0.053       77.17       17.928       W       0.193         23.03       82.50       W       0.185       0.054       77.17       41282       W       0.193         53.73       4558       W       0.185       0.054       77.17       41282       W       0.033         53.73       25930       W       0.193       77.17       41282       W       0.033         53.72       25931       W       0.102       0.034       77.26       72364       W       0.033         54.70       40       1002       0.034       77.26       72364       W       0.033         54.70       20100       W       0.112       0.014       0.023       W       0.033         54.71       20100       W       0.122       0.014       0.023       W       0.033         54.70       11837       W       0.122       0.014       0.023       W       0.033         54.71       11837       W       0.1022       0.014       0.023 | 11.12       10980       PV       0.117       0.015       0.0120       VV       0.117       0.019         22.10       PV       0.116       0.051       77.17       17.17       17.17       0.196       0.019         23.13       41962       VV       0.165       0.051       77.17       41282       VV       0.193         23.73       45962       VV       0.166       0.031       77.17       41282       VV       0.031         23.75       23930       VV       0.103       0.031       77.26       409610       VV       0.033         24.42       23930       VV       0.103       0.034       77.26       409610       VV       0.033         24.42       23930       VV       0.103       77.26       2394       VV       0.033         24.42       23931       VV       0.034       77.26       7234       VV       0.033         24.42       23931       VV       0.034       77.26       7236       VV       0.033         24.43       71.000       11837       VV       0.034       77.26       7236       VV       0.033         24.43       11837       VV | 11.12       10980       PV       0.117       0.015       0.0120       PV       0.117       0.019         12.01       10960       PV       0.117       0.015       0.113       17.17       17.33       17.928       VV       0.195         12.02       11962       VV       0.165       0.051       77.17       17.17       17.128       VV       0.013         12.12       25970       VV       0.185       0.031       77.26       12954       VV       0.033         12.12       25910       VV       0.102       0.033       77.26       12945       VV       0.033         12.12       25190       VV       0.103       0.034       77.26       12945       VV       0.033         12.12       10010       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       10100       VV       0.037       0.014       0.033       77.26       12945       VV       0.033         14.57       11877       VV       0.035       0.014       0.023       VV       0.033         14.57       11877       VV       0.035       0.014       0.023 <td>11.12       10980       Y       0.117       0.015       0.0120       Y       0.117       0.0136         22.01       10960       Y       0.117       0.015       0.057       Y       0.196         23.03       45558       Y       0.185       0.057       77.17       41282       Y       0.013         43.05       Y       0.183       0.094       77.17       41282       Y       0.013         43.17       17       27.01       17.26       40950       Y       0.023         44.2       23380       Y       0.039       77.26       409510       Y       0.013         44.12       23390       Y       0.123       0.039       77.26       409510       Y       0.013         44.12       23910       Y       0.122       0.039       77.26       7234       Y       0.013         44.15       2391       Y       0.122       0.014       0.013       Y       0.023         44.15       2391       Y       0.123       0.014       0.023       Y       0.023         44.15       2491       11837       Y       0.023       0.043       Y       0.023</td> <td>41.12       10980       W       0.117       0.015       0.0120 
     W       0.117       0.013         42.1       10980       W       0.117       0.015       0.051       W       0.119         43.3       44558       W       0.143       0.054       77.17       41282       W       0.119         43.5       W       0.143       0.056       0.031       77.17       41282       W       0.013         43.7       17       17       17       17       17       41282       W       0.031         44.2       23910       W       0.102       0.034       77.26       1294       W       0.013         44.2       23910       W       0.122       0.034       77.26       1294       W       0.033         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.023         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.013         44.3       10000       W       0.122       0.014       0.023       W       0.013         45.3       11807       W       0.023       W</td> <td>11.11       0.0100       W       0.117       0.015       0.012       W       0.119         0.1120       W       0.116       0.013       0.113       0.013       W       0.113         0.1120       W       0.165       0.057       0.051       17.17       0.1132       W       0.113         0.1120       W       0.165       0.051       77.17       0.1232       W       0.0133         0.1121       0.0102       0.0103       0.0114       0.0133       77.17       0.1232       W       0.023         0.1121       0.0102       0.0103       0.0104       0.0103       77.17       0.1232       W       0.023         0.1111       0.0103       W       0.1113       0.0114       0.013       W       0.0123         0.1187       W       0.0104       W       0.014       0.014       0.023       W       0.023         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       0.014</td> <td>11.12       10980       W       0.117       0.015       0.015       0.015       0.016       0.013         0.2.01       W       0.165       0.015       0.013<td>11.11       10990       W       0.117       0.015       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.0</td><td>11.12       10000       W       0.117       0.005       0.061       0.011       0.0</td><td>11.12       10000       W       0.117       0.005       47.32       40.9630       W       0.126         0.130       4558       W       0.165       0.057       47.31       4136       W       0.133         0.130       4558       W       0.165       0.057       77.31       3136       W       0.133         0.130       4558       W       0.165       0.031       77.31       3136       W       0.031         0.131       W       0.095       0.031       77.33       21363       W       0.033         0.132       23930       W       0.032       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       0.034       9.136       0.043         0.145       23010       W       0.035       0.034       9.136       0.043       0.043         0.145       24710       W       0.035       0.034       9.136       0.043       0.043         0.145       113010       W       0.135       0.035</td><td>11.11       01030       W       0.117       0.005       W       0.105         12.12       01030       W       0.117       0.015</td><td>11.11       01000       W       0.117       0.005       W       0.105         12.10       W 1012       W       0.117       0.013       0.013       W       0.113         12.10       W 1012       W       0.105       0.003       77.11       11.135       W       0.105         12.10       W 1012       0.013       0.024       0.135       W       0.135       W       0.135         12.10       W 1012       0.013       0.012       0.013       77.13       11354       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2036       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2031       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 10.012       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 1187       W 10.012       W 10.012       <t< td=""><td>11.11       01090       W       0.117       0.005       W       0.105         12.12       01090       W       0.117       0.005       0.005       0.005         12.15       0.0120       W       0.116       0.005       0.015       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.012       0.012         12.15       0.0120       W       0.105       0.012       0.012       0.012       0.012         12.15       0.0120       W       0.102       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W</td><td>11.11       11.0900       W       0.117       0.015       0.133       0.061       W       0.126         12.510       W       0.116       0.015 
     0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015       0.015</td><td>11.11       01930       W       0.117       0.015       0.135       0.061       W       0.136         12.12       01300       W       0.116       0.017       72.26       0.061       W       0.136         12.15       0130       0135       0135       0135       W       0.135       0135       W       0.135         12.15       0130       W       0102       0131       0135       W       0.135         12.15       0130       W       0102       0135       W       0.135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       013</td><td>11.11       11.0900       W       0.117       0.015       0</td><td>11.11       10000       W       0.113       0.003       W       0.113       0.003       W       0.103         10.11       10000       W       0.113       0.003       77.20       0.003       77.31       W       0.103         10.12       1000       W       0.113       0.003       77.21       0.003       77.23<!--</td--><td>11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101</td><td>1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01</td><td>11.11       110700       W       0.113       0.005       0.</td><td>11.1       11000       W       111       0.001       W       0.013       W</td></td></t<></td></td> | 11.12       10980       Y       0.117       0.015       0.0120       Y       0.117       0.0136         22.01       10960       Y       0.117       0.015       0.057       Y       0.196         23.03       45558       Y       0.185       0.057       77.17       41282       Y       0.013         43.05       Y       0.183       0.094       77.17       41282       Y       0.013         43.17       17       27.01       17.26       40950       Y       0.023         44.2       23380       Y       0.039       77.26       409510       Y       0.013         44.12       23390       Y       0.123       0.039       77.26       409510       Y       0.013         44.12       23910       Y       0.122       0.039       77.26       7234       Y       0.013         44.15       2391       Y       0.122       0.014       0.013       Y       0.023         44.15       2391       Y       0.123       0.014       0.023       Y       0.023         44.15       2491       11837       Y       0.023       0.043       Y       0.023 | 41.12       10980       W       0.117       0.015       0.0120       W       0.117       0.013         42.1       10980       W       0.117       0.015       0.051       W       0.119         43.3       44558       W       0.143       0.054       77.17       41282       W       0.119         43.5       W       0.143       0.056       0.031       77.17       41282       W       0.013         43.7       17       17       17       17       17       41282       W       0.031         44.2       23910       W       0.102       0.034       77.26       1294       W       0.013         44.2       23910       W       0.122       0.034       77.26       1294       W       0.033         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.023         44.2       2391       W       0.122       0.014       0.012       0.013       W       0.013         44.3       10000       W       0.122       0.014       0.023       W       0.013         45.3       11807       W       0.023       W | 11.11       0.0100       W       0.117       0.015       0.012       W       0.119         0.1120       W       0.116       0.013       0.113       0.013       W       0.113         0.1120       W       0.165       0.057       0.051       17.17       0.1132       W       0.113         0.1120       W       0.165       0.051       77.17       0.1232       W       0.0133         0.1121       0.0102       0.0103       0.0114       0.0133       77.17       0.1232       W       0.023         0.1121       0.0102       0.0103       0.0104       0.0103       77.17       0.1232       W       0.023         0.1111       0.0103       W       0.1113       0.0114       0.013       W       0.0123         0.1187       W       0.0104       W       0.014       0.014       0.023       W       0.023         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       W       0.014       0.014       0.023       W       0.024         0.1187       W       0.014       0.014 | 11.12       10980       W       0.117       0.015       0.015       0.015       0.016       0.013         0.2.01       W       0.165       0.015       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013       0.013      
0.013       0.013 <td>11.11       10990       W       0.117       0.015       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.0</td> <td>11.12       10000       W       0.117       0.005       0.061       0.011       0.0</td> <td>11.12       10000       W       0.117       0.005       47.32       40.9630       W       0.126         0.130       4558       W       0.165       0.057       47.31       4136       W       0.133         0.130       4558       W       0.165       0.057       77.31       3136       W       0.133         0.130       4558       W       0.165       0.031       77.31       3136       W       0.031         0.131       W       0.095       0.031       77.33       21363       W       0.033         0.132       23930       W       0.032       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       0.034       9.136       0.043         0.145       23010       W       0.035       0.034       9.136       0.043       0.043         0.145       24710       W       0.035       0.034       9.136       0.043       0.043         0.145       113010       W       0.135       0.035</td> <td>11.11       01030       W       0.117       0.005       W       0.105         12.12       01030       W       0.117       0.015</td> <td>11.11       01000       W       0.117       0.005       W       0.105         12.10       W 1012       W       0.117       0.013       0.013       W       0.113         12.10       W 1012       W       0.105       0.003       77.11       11.135       W       0.105         12.10       W 1012       0.013       0.024       0.135       W       0.135       W       0.135         12.10       W 1012       0.013       0.012       0.013       77.13       11354       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2036       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2031       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 10.012       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 1187       W 10.012       W 10.012       <t< td=""><td>11.11       01090       W       0.117       0.005       W       0.105         12.12       01090       W       0.117       0.005       0.005       0.005         12.15       0.0120       W       0.116       0.005       0.015       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.012       0.012         12.15       0.0120       W       0.105       0.012       0.012       0.012       0.012         12.15       0.0120       W       0.102       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W</td><td>11.11       11.0900       W       0.117       0.015       0.133       0.061       W       0.126         12.510       W       0.116       0.015</td><td>11.11       01930       W       0.117       0.015       0.135       0.061       W       0.136         12.12       01300       W       0.116       0.017       72.26       0.061       W       0.136         12.15       0130       0135       0135       0135       W       0.135       0135       W       0.135         12.15       0130       W       0102       0131       0135       W       0.135         12.15       0130       W       0102       0135       W       0.135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       013</td><td>11.11       11.0900       W       0.117       0.015       0</td><td>11.11      
10000       W       0.113       0.003       W       0.113       0.003       W       0.103         10.11       10000       W       0.113       0.003       77.20       0.003       77.31       W       0.103         10.12       1000       W       0.113       0.003       77.21       0.003       77.23<!--</td--><td>11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101</td><td>1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01</td><td>11.11       110700       W       0.113       0.005       0.</td><td>11.1       11000       W       111       0.001       W       0.013       W</td></td></t<></td> | 11.11       10990       W       0.117       0.015       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.136       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.135       W       0.035       W       0.0 | 11.12       10000       W       0.117       0.005       0.061       0.011       0.0 | 11.12       10000       W       0.117       0.005       47.32       40.9630       W       0.126         0.130       4558       W       0.165       0.057       47.31       4136       W       0.133         0.130       4558       W       0.165       0.057       77.31       3136       W       0.133         0.130       4558       W       0.165       0.031       77.31       3136       W       0.031         0.131       W       0.095       0.031       77.33       21363       W       0.033         0.132       23930       W       0.032       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       77.23       23354       W       0.033         0.145       23930       W       0.035       0.034       0.034       9.136       0.043         0.145       23010       W       0.035       0.034       9.136       0.043       0.043         0.145       24710       W       0.035       0.034       9.136       0.043       0.043         0.145       113010       W       0.135       0.035 | 11.11       01030       W       0.117       0.005       W       0.105         12.12       01030       W       0.117       0.015 | 11.11       01000       W       0.117       0.005       W       0.105         12.10       W 1012       W       0.117       0.013       0.013       W       0.113         12.10       W 1012       W       0.105       0.003       77.11       11.135       W       0.105         12.10       W 1012       0.013       0.024       0.135       W       0.135       W       0.135         12.10       W 1012       0.013       0.012       0.013       77.13       11354       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2036       W       0.013         12.11       W 1012       0.013       W 1012       0.013       77.23       2031       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         44.05       11801       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 10.012       W 10.012       0.013       W 10.012       0.013       W       0.013         45.05       W 1187       W 10.012       W 10.012 <t< td=""><td>11.11       01090       W       0.117       0.005       W       0.105         12.12       01090       W       0.117       0.005       0.005       0.005         12.15       0.0120       W       0.116       0.005       0.015       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.012       0.012         12.15       0.0120       W       0.105       0.012       0.012       0.012       0.012         12.15       0.0120       W       0.102       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W       0.012       0.012       0.012
      0.012       0.012         12.15       0.012       W</td><td>11.11       11.0900       W       0.117       0.015       0.133       0.061       W       0.126         12.510       W       0.116       0.015</td><td>11.11       01930       W       0.117       0.015       0.135       0.061       W       0.136         12.12       01300       W       0.116       0.017       72.26       0.061       W       0.136         12.15       0130       0135       0135       0135       W       0.135       0135       W       0.135         12.15       0130       W       0102       0131       0135       W       0.135         12.15       0130       W       0102       0135       W       0.135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       013</td><td>11.11       11.0900       W       0.117       0.015       0</td><td>11.11       10000       W       0.113       0.003       W       0.113       0.003       W       0.103         10.11       10000       W       0.113       0.003       77.20       0.003       77.31       W       0.103         10.12       1000       W       0.113       0.003       77.21       0.003       77.23<!--</td--><td>11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101</td><td>1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01</td><td>11.11       110700       W       0.113       0.005       0.</td><td>11.1       11000       W       111       0.001       W       0.013       W</td></td></t<> | 11.11       01090       W       0.117       0.005       W       0.105         12.12       01090       W       0.117       0.005       0.005       0.005         12.15       0.0120       W       0.116       0.005       0.015       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.005       0.012         12.15       0.0120       W       0.105       0.005       0.012       0.012       0.012         12.15       0.0120       W       0.105       0.012       0.012       0.012       0.012         12.15       0.0120       W       0.102       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.010       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W       0.012       0.012       0.012       0.012       0.012         12.15       0.012       W | 11.11       11.0900       W       0.117       0.015       0.133       0.061       W       0.126         12.510       W       0.116       0.015 | 11.11       01930       W       0.117       0.015       0.135       0.061       W       0.136         12.12       01300       W       0.116       0.017       72.26       0.061       W       0.136     
   12.15       0130       0135       0135       0135       W       0.135       0135       W       0.135         12.15       0130       W       0102       0131       0135       W       0.135         12.15       0130       W       0102       0135       W       0.135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0.135         12.15       0130       W       0102       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       0135       W       0135       W       0135         12.15       0130       W       0135       W       013 | 11.11       11.0900       W       0.117       0.015       0 | 11.11       10000       W       0.113       0.003       W       0.113       0.003       W       0.103         10.11       10000       W       0.113       0.003       77.20       0.003       77.31       W       0.103         10.12       1000       W       0.113       0.003       77.21       0.003       77.23 </td <td>11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101</td> <td>1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01</td> <td>11.11       110700       W       0.113       0.005       0.</td> <td>11.1       11000       W       111       0.001       W       0.013       W</td> | 11.1       10000       W       0.113       0.005       W       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       10000       W       0.113       0.005       0.133       W       0.133         10.1       1000       W       0.105       0.001       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.134         10.1       1000       W       0.105       0.001       0.013       0.134       W       0.105         10.1       1000       W       0.105       0.013       0.013       0.105       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.105         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.105       0.013       0.013       W       0.103         10.1       1000       W       0.113       W       0.103       W       0.103         10.101 | 1111       10700       W       0.11       0.01         1211       10700       W       0.11       0.01         1211       10701       W       0.10       0.01         1211       10701       W       0.10       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01         1211       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       10701       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01       0.01         1111       10701       0.01       0.01       0.01       0.01       0.01 | 11.11       110700       W       0.113       0.005       0. | 11.1       11000       W       111       0.001       W       0.013       W |

0.097 0.042 0.045 0.045 0.045 0.056 0.056 0.056 0.017 0.014 0.014 0.017 0.017 0.017 0.017 0.017

Table A19	24.15 24234 VV 0.078 0.027
	24.27 14996 VV 0.095 0.017
pH 11	24.70 48044 VP 0.122 0.053
	25.14 602410 PV 0.098 0.668
RUN # 786, APR/30/86,14:52:07	checkpoint: the next peak is A25; add 0.03 minutes
WORKFILE ID: C ,WORKFILE NAME:	25.38 4997500 VB 0.126 5.544
1D: 000	27.06 23158 VV 0.120 0.026
AREA%	27.25 46161 VV 0.157 0.051
RT AREA TYPE AR/HI AREAS	27.50 10060 VV 0.064 0.011
5.12 49971 D BB 0.140 0.055	27.93 20224 VV 0.110 0.022
6.65 623830 BV 0.167 0.872	28.23 12000 PP 0.098 0.013
6.95 64744 VV U.109 U.072	28.55 13707 BV 0.107 0.015
7.05 93940 VV 0.157 0.104	29.16 12113 VV 0.117 0.013
7.28 152030 VP 0.1/7 0.107	29.86 24841 BV 0.090 0.028
7.66 60074 PV 0.076 0.007	30.32 17834 PP 0.125 0.020
checkpoint: AS is next; Ri is dir becaus peak is broad	30.58 32599 PV 0.104 0.036
	31.25 930860 PB 0.120 1.033
	32.07 66028 PV 0.211 0.073
9.52 21029 PP 0.141 0.024	32.44 19301 VV 0.119 0.021
9.8/ 83483 FF 0.131 0.531	32.60 28372 VV 0.136 0.032
10.41 479000 PV 0.131 0.351	32.71 36727 VV 0.133 0.041
10.72 703220 VV 0.117 0.70	32.90 21494 VV 0.103 0.024
10.87 571440 VV 0.110 0.179	33.09 28233 VV 0.096 0.031
11.12 101020 VV 0.131 0.023	33.44 18386 PP 0.090 0.020
12.08 S8414 RV 0.217 0.065	34.11 177110 PB 0.088 0.197
12.51 55188 PV 0 128 0.062	34.92 19783 PP 0.096 0.022
12.31 5550 VV 0.135 0.050	JS.JI S5688 PV 0.151 0.062
12.96 101850 VV 0.176 0.113	J5.80 15554 VV 0.196 0.017
13 26 124620 VV 0.091 0.360	30.00 I390100 VV 0.107 I.349
checkpoint the next peak is A14; subtract 0.01 minute	
13 38 690880 VV 0,142 0.767	30.47 143040 VV 0.111 0.139 26.73 02/03 MV 0.136 0.10/
13.87 178840 VV 0.211 0.198	checkmeint: the next such in D2, and 0.02 minutes
14.24 236700 VV 0.269 0.263	$\frac{16}{36} = \frac{13}{32} = 13$
14.37 75978 VV 0.084 0.084	37 26 23383 VV 0,066 0,056
14,44 99555 VV 0.102 0.110	37 38 67146 WV 0 140 0 052
14.62 484970 VV 0.228 0.538	37 63 112190 W 0.097 0.125
14.89 387750 VV 0.277 0.430	38.02 21225 WV 0.108 0.024
15.22 270920 VV 0.163 0.301	38.25 38156 VV 0.086 0.042
15.34 318220 VV 0.229 0.353	38,34 58532 VV 0,132 0,065
15.72 495220 VV 0.222 0.549	39.10 200530 VB 0.108 0.223
16.13 224100 VP 0.245 0.249	39.82 2609100 PB D.096 2.895
checkpoint: the next peak is A18; RT exact	40.80 22586 VP 0.109 0.025
16.93 1667400 PB 0.114 1.850	41.33 8174700 PB 0.152 9.069
17,70 19816 BV 0.148 0.022	42.76 43094 PV 0.083 0.048
17.95 29896 VV 0.080 0.033	42.84 76788 VV 0.136 0.085
18.14 11360 VP 0.103 0.013	42.98 96664 VV 0.171 0.107
19.38 24409 VV 0.094 0.027	43.45 102530 VV 0.181 0.114
20.55 14289 VP 0.144 0.016	43.75 15016 VV 0.099 0.017
21.79 15656 VV 0.171 0.017	43.96 12558 VP 0.086 0.014
23.32 11273 PV 0.117 0.013	44.36 444570 VV 0.151 0.493
23.69 19841 VV 0.111 0.022	44.73 86717 VV 0.252 0.096
23.88 17973 VV 0.135 0.020	45.19 379770 VV 0.154 0.421
24.04 12872 VV 0.092 0.014	45.79 52108 VV 0.252 0.058

42473       W       0.158       0.067         187470       W       0.112       0.068         187460       W       0.112       0.068         187460       W       0.112       0.066         18110       W       0.112       0.066         18110       W       0.112       0.065         181110       W       0.1130       0.055         181110       W       0.1130       0.055         181110       W       0.1130       0.055         181110       W       0.1130       0.055         181110       W       0.113       0.055         181110       W       0.113       0.055         181110       W       0.113       0.055         181110       W       0.113       0.113         20156       W       0.113       0.112         2113110       W       0.113       0.112         20156       W       0.113       0.112         20156       W       0.113       0.123         20156       W       0.113       0.123         20156       W       0.113       0.123         20156       <
42473       W       0.158         61333       W       0.150         57465       W       0.112         57465       W       0.112         52485       W       0.112         52485       W       0.112         51915       W       0.112         61915       W       0.112         61915       W       0.1130         61916       W       0.1130         619170       W       0.123         61918       W       0.130         61919       W       0.130         61919       W       0.130         61919       W       0.130         619190       W       0.130         619190       W       0.131         9111100       W       0.131 <trr>       9111111111       9153       &lt;</trr>
42473 42473 53487 53487 53487 53487 53487 53487 53487 53487 53487 53487 53487 53487 53487 53487 535780 5355780 535578 555552 555552 7 7 113947 113947 113949

					19.68	140700	PV	0.080
	Teb	le A20	)		19.86	1117800	vv	0.111
					19.99	279400	vv	0.123
5	ng Browide,	10	chlorin	e dose	20.31	79112	vv	0.159
		-			20.52	20828	٧V	0.098
RUN #	769,		PR/27/86	.18:24:52	20.92	76260	PV	0.195
WORKFIL	£ ID: C		, WORKF	ILE NAME:	21.29	37930	vv	0.146
ID: 000	1				21.80	61346	PV	0.143
AREA%					22.04	129380	AA.	0.108
RT	AREA	TYPE	AR/HT	AREAL	22.52	21159	PV	0.085
6.10	436570	BP	0.218	0.197	22.63	18412	VP	0.078
6.62	4.4640E+07	SPB	0.279	20.158	22.86	205530	PV	0.108
7.92	2280800	TBV	0.166	1.030	23.22	245980	W	0.083
8.11	2621500	TVV	0.193	1.184	23.39	430070	vv	0.119
6.4Z	1500700	TVV	0.153	0.678	23.77	335490	VV	0.119
8.49	2609700	DTVB	0.272	1.178	24.14	86291	VV	0.111
9.35	383410	BV	0.117	0.173	24.30	112210	vv	0.167
7.02	185640	vv	0.165	0.084	Z4.61	36360	vv	0.070
7.71	15513	vv	0.074	0.007	24.71	203540		0.128
10.01	23/2000	PH	0.133	1.071	24.97	34609		0.094
11 40	5.152/E+0/	SHB	0.258	23.267	23.18	26183	VV MV	0.115
11.40	250070	TBP	0.084	0.113	23.47	24/080		0.142
11.00	265700	TPB	0.078	0.129	25.03	12377		0.043
12 50	105130	181	0.143	0.165	23.01	1140300	vv	0.004
12.50	53548	VD	0.061	0.005	26.00	215330	ve	0.113
11.22	192720	VP VU	0.147	0.024	74 57	14220		0.088
13.39	484440		0.109	0.087	26.57	39017	vv	0.078
13.54	44063	ה עע	0.131	0.219	26 80	103190	vv	0 093
13.73	2861000	VV	0.043	0.020	27.09	33085	vv	0.179
13.87	3380000	vv	0.215	1.292	27.21	105030	vv	0.121
14.29	94799	vv	0.076	1.520	27.47	1798300	vv	0.092
14.32	373570	DVV	0 100	0.149	27.88	99939	W	0.137
14.46	75303	vv	0.024	0.109	28.07	190520	vv	0.113
14.50	168970	DVV	0.053	0.074	28.22	120870	VV	0.112
14.64	424710	vv	0.114	0 192	28.41	124710	WV.	0.169
14.67	163820	D VV	0.044	0 074	28.67	46798	VV	0.084
14.72	154620	VV	0.042	0.070	28.84	131150	vv	0.118
14.88	3075500	vv	0.158	1.389	29.12	99938	٧V	0.099
15.10	386230	vv	0.070	0.174	29.31	24653	W	0.080
15.22	477810	vv	0.083	0.216	29.46	25084	. <b>VV</b>	0.080
checkpoi	nt: the nex	t peak	is brom	oform	29.62	209200	WV.	0.139
15.37	1552000	VH	0.204 )	0.701	29.80	54068	vv	0.096
15.69	5.1591E+07	SHD	0.252	23.296	29.96	79009	vv	0.113
15.99	1011000	TBB	0.082	0.457	30.13	28624	vv	0.077
16.34	50623	TBB	0.072	0.023	30.29	35432	vv	0.112
16.94	2757000	TVV	0.160	1.245	30.60	357950	vv	0.099
17.23	229420 1	DTVV .	0.102	0.104	30.98	62899	W	0.114
17.38	88108 1	UTVB	0.108	0.040	31.28	179980	VV.	0.107
17.03	133910	BV	0.087	0.061	31.40	90999	VV	0.100
17.00	353380	vv	0.136	0.160	31.72	247540	VV.	0.056
10.11	93968	VP	0.102	0.042	31.92	37461	VV	0.080
10.34	22916	PP	0.125	0.010	32.17	48590	VP	0.094
19 20	330450	VV	0.093	0.149	32.53	33516	m	0.0/3
17.47	103150	VP	0.149	0.047				

0.064

0.505 0.126 0.036

0.009 0.034 0.017 0.028

0.058

0.010 0.008 0.093 0.111 0.194 0.152 0.040 0.051 0.017

0.092 0.016 0.025 0.112

0.006 0.623 0.515 0.097

0.006 0.018 0.047 0.015

0.047

0.045

0.055

0.021

0.045

0.011 0.095

0.024

0.013

0.016

0.162

0.028

0.081

0.112

0.017

0.015

32.59	26197	HH	0.077	0.012	43.47	143600	2	0.059	0.065			ł		
32.77	1721500	E.	760.0	0.777	43.65	1270000	3	0.123	0.574	53.02	15542	\$ 1	0.052	0.0
33.04	13196	АМ	0.058	0.006	43.74	904560	3	0.110	0.409	23.11	101/6	23	0.07	
33.19	26322	<b>6</b>	0.072	0.012	43.94	683380	3	0.128	0.309	23.23	00/845	<b>;</b>		
33.37	66460	H	0.061	0.030	44.20	538090	3	0.130	0.243		210012	\$ 3	0.100	760 Q
33.54	103950	Ē	0.088	0.047		06/571	\$	0.127	0.057		01430	: 3	146	
33.89	166640	H	0.127	0.075	60. <b>44</b>		\$ 3	0.093	0.051	27.00 54 21	17035	: 3	0.123	0.008
34.23	34000	H	0.083	0.015	16.11	266930	: 3	0.140	0.398	34.49	46456	2	0.127	0.021
34.05	106210	Ē	0.114	0.048	45.21	275260	: 3	0.150	0.121	54.68	23704	3	0.089	0.011
00.4C	76197	23	0.144	0.114	45.29	162190	3	0,103	0.082	55.28	36469	3	0.132	0.017
35.29	22966		0.078	170.0	45.63	747390	3	0.189	0.338	55.54	45804	3	0.135	0.021
35.50	56971	Ē	0.001	0.026	45,86	72110	≩	0.088	0.033	55.73	23752	3	0.117	0.011
35.62	305090	Ð	0.109	0.139	45.99	92531	3	0.119	0.042	55.85	22150	\$ 3	160.0	010.0
35.79	86179	Ē	0.092	0.039	46.13	86536	3	0.106	0.039	59.63 5	9/016	2 3	0.100	
35.92	30245	H	0.063	0.014	99.64	270790	≥ !	0.233	0.122	20.23	0/0010	: 3		0.026
36.04	241610	H	0.140	0.109	10.04	44186	\$	0.127	0.044	30.40	20106	: 3	0.047	010 0
36.21	30342	HQ	0.044	0.014	40.04	914950	≥ ;	0.153	0.045	20.20 26 74	19691	: 3	0,060	0.008
36.54	724290	Ē	0.244	0.327	1 1 2	015500	23	(77) (77)	860.0	24.80	37365	3	0.130	0.017
36.70	381550	Ē	0.142	0.172	47.72	411780	: 3	0.110		51.49	137730	2	0.129	0.062
36.90	070679	Ē	0.128	0.293	47.93	38324 D	: 3	0.051	C.190	58.23	11675	3	0.060	0.005
37.24	91120	Ē	0.065	0.023	48.09	932590	: 3	0.125	0.41	58.41	10549	\$	0.063	0.005
	324940	Ë j	0.177	0.147	48.36	36013	:3	0.050	0 012	58.51	26882	5	0.101	0.012
.0.15	072401	Į	0.175	0.074	48.43	70568	3	0.080	0.012	58.69	16835	3	0.077	0.008
10.15	110100	5	0.000	0.044	48.56	172870	3	0.109	0.078	58.77	20650	\$	0.061	0.00
40 ML	048461	5		C 000	48.66	205300	3	0.118	0.093	58.62	24123	3	0.062	0.011
38.22	109710	Ē		0.050	48.83	261990	3	0.160	0.118	59.44	65001	3	0.106	0.029
38.44	130850	Ē	0.182	0.059	49.02	84478	3	0.097	0.038	60.78	61099	\$ !	0.100	000 0
38.67	27390	ÿ	0.096	0.012	49.17	54057	3	0.085	0.024	60.93	100670	3	0.195	
38.92	53632	Ŧ	0, 101	0.024	49.23	0 29793 D	3	0.058	0.015	61.30	012664	23	0.107	0 148
39.09	599600	Ē	0.134	0.271	49.29	13003	3	0.028	0.006	81.75 51.75	10/4/01	5	0 102	0.029
39.27	120980	Ð	0.067	0.055	49.40	014942	\$ !	0.136	0.112	27.70 27.71	62885	: 3	0.100	0.028
39.36	013120	Ā	0.136	0.141	10.67	10100	\$ 3		0.052	65.22	44195	3	0.120	0.020
39.54	223610	Ţ.	0.108	0.101	49.81	29897	:3	102		65.40	43358	3	0.150	0.020
39.69 20.00	125600	Ē	0.111	0.058	49.84	42646 D	: 3	0 058		65.68	78532	3	0.223	0.036
19.90		5 3	0.158	0.160	49.99	118740	3	0.119	10.0	66.82	35105	3	0.132	0.016
20.04	199950	5 3	0.099	0.135	50.10	39173 D	3	0.087	0.018	67.43	10311	3	0.098	0.005
40.78	513080	Ē	0.120	0.775	50.20	13756 D	3	0.042	0.006	67.94	20652	<b>≥</b> i	0.152	400 0
41.09	190710	Ē	0.135	0.086	50.30	37664	3	0.112	0.017	69.37	10401	2 2	0.249	090 0
41.34	258310	Ð	0.140	0.117	50.40 50	19934	\$ į	0.084	0.009	10.22	01/201	2 2	12.0	0.007
41.53	560440	ž	0.095	0.253	70.00	000141	\$	0.145	0.064		476770	2	0.266	0.215
41.69	537490	Æ	0.171	0.243	20 00	1 2454C	23	0.04/	0.016	11.11	17072	2	960.0	0.008
41.90	198270	Ž	0.098	0.090	51.02	62828	5	7117 0 107	0.032	81.33	21304	3	0.105	0.010
4Z.00	248280	ž	0.120	0.112	51.74	1744	2			81.44	39530	3	0.171	0.018
42.25	625750	Ē	0.141	0.283	51.41	14616	: 3		000.0	82.88	11374	3	0.103	0.005
42.34 1	149520	Ē	0.105	0.068	51.46	25757	:3	0.048	0.00	TOTAL AREA	= 2.2146E	80 <b>-</b>		
00.14	1049/01	Ē	0.112	0.047	51.80	618360	3	0.110	0 276	MUL FACTOR	= 1.0000E	B		
B/ . 74	145030	5 3	0,100	0.035	52.22	14659	2	0.062	0.007					
00.34	1405000	53	191.0	c/0.0	52.47	48412	:≩	0.125	0.022					
41.74	017056	5 5		0.015	52.73	54750	3	0.118	0.025					
43.35	151400 0	E	0.073	0.068	\$2.92	15713	3	0.068	0.007					
				****										

### **APPENDIX 4**

This appendix includes the data used to calculate the coefficient  $K_LA$  in the aeration experiment (Table A21).

Time (minutes)	Dissolved Oxygen (mg/L)
0:00	0.2
0:33	1.0
1:00	1.8
1:15	2.2
1:30	2.6
1:45	3.9
2:00	4.8
2:15	5.0
2:30	5.6
2:45	5.7
3:00	6.2
3:30	6.5
4:00	6.5
4:30	6.5
5:00	6.6
6:00	6.7

## Table A21 Aeration Data

#### **APPENDIX 5**

In an effort to compare the San Diego effluent with other plants, two other plants were selected for investigation, the Whittier Narrows treatment plant in Los Angeles County, and an aquaculture treatment system in central Florida.

Methylene chloride extractable organics were analyzed for the Whittier Narrows and a Florida plant's gravimetrically, by GC, and by GC/MS. This survey was done to compare the profiles of the solvent extractable organics from these two plants with the identified compounds at the San Diego Wastewater Treatment Plant. The Florida plant provides a water hyacinth based secondary treatment plant for the comparison, whereas the Whittier Narrows plant allows for comparison to activated sludge treatment.

The Whittier Narrows Plant is an activated sludge facility, with primary clarification operating at an F/M ratio of approximately 0.50/days. This plant is one of the LA County Sanitation Districts inland plants. It receives largely domestic wastewater, with most industrial waters being routed around the Whittier Narrows Plant to the Joint Plant at Carson. The Florida plant is a water hyacinth facility. It uses a single stage basin, approximately 0.5 meters deep, with a hydraulic retention time of approximately one day.

Tables B1 through B3 summarize the gravimetric data and the lump GC data on the three treatment plants. The data used for the San Diego plant represent an average of all the collected samples (Tables 9 and 10) whereas the data on the Whittier Narrows and Florida plants represent a single sampling (4/86). The data shown in Table B1 shows several similarities and differences between the samples. The non-polar fractions (1 and 2) roughly represent one quarter to one third of the total extract (gravimetrically). The Florida plant extract seems to be primarily composed of gas chromatographable polar compounds since 75% of the extract is polar by weight and the non-polar fractions represent a small fraction (7%) of the total FID area. The GC analysis of the Florida wastewater treatment plant sample shows the presence of many straight chain fatty acids. In contrast, the San Diego and Whittier Narrows samples show large amounts of non-polar compounds in their chromatographs (69 and 72%, respectively).

The Whittier Narrows plant extract gives a much larger ECD response than either of the other two plants. Most of this ECD response is due to chlorination by-products which were previously discussed. These compounds were in low concentrations however (less than 1  $\mu$ g/l) and were consequently not identifiable by GC/MS for the Whittier Narrows extract. These compounds were detectable by the more sensitive ECD and showed retention time matches with the halogenated chlorination by-products (Table 14). It is plausible that the influent to the Whittier Narrows plant contained larger amounts of these halogenated compounds, causing high effluent concentrations were higher.

The GC and GC/MS for the San Diego Wastewater Treatment Plant effluent extract were previously shown (Figures 12 and 13). Fig-

Treatment Plant	Weight (mg/L)	Total Weight Represented in Fractions 1,2	% Gravimetric Area Represented by Fractions 1,2	% of the FID Ratio of Total ECD/FID Areas
San Diego	5.04	32	69	0.81
Disney World	14.91	25	7	0.20
Whittier Narrows	2.61	27	72	6.11

### Table B1 General Makeup of Treatment Plant Extracts

.

Scan No.	RT (minutes)	ID Compound Name or Formula	Conc. (µg/L)	% Confidence in ID	Method of ID
269		chloroform	ND	>95	1,2,3
294		bromochloromethane	ND	>95	1,2,3
448	8.18	chloroiodomethane	0.4	90	1
474	8.26	benzene, 1-ethyl, 4-methyl	0.4	70	1,2
483	8.50	2-pentyl furan	0.4	80	1,2
595	12.60	benzene 1,2,3, trimethyl	0.5	70	1,2
659	14.50	tetradecane (is)	11.0	>95	1,2,3
709	15.51	1,4 dichlorobenzene	0.3	>95	1,2,3
752	17.51	1,3 dichlorobenzene	7.1	>95	1,2,3
759	17.80	$C_{17}$ aliphatic hydrocarbon	2.9	90	1
843	20.40	2-furancarboxaldehyde, 5-methyl	3.7	90	1,2
907	22.54	1-hexanone-1-phenyl	10.5	70	1,2
949	24.01	$C_{19}$ aliphatic	2.3	90	1
1146	30.53	tetradecanal	3.9	60	1
1203	32.45	hexadecanal	4.8	80	1
1213	32.76	phenol	5.3	>95	1,2,3
1265	34.45	1-decanoic acid	3.5	>95	1,2,3
1283	34.75	p-cresol	3.1	>95	1,2,3
1308	35.90	phosphoric acid- tributyl ester	10.0	90	1,2
1410	39.39	1h-pyrole-2,5 dione- 3-ethyl-4-methyl	2.9	60	1,2

# Table B2.Compounds Identified in the Whittier Narrows Wastewater<br/>Treatment Plant Secondary Effluent (4/86) by GC/MS

Scan No.	RT (minutes)	ID Compound Name or Formula	Conc. (µg/L)	% Confidence in ID	Method of ID
1419	39.64	1-undecanoic acid	2.0	>95	1,2,3
1421	39.81	phenol 2-(1,1-dimethylethyl)	4.0	85	1,2
1463	40.90	1-hexadecanol	1.3	90	1,2,3
1503	42.58	1-propanone,1-(methoxyphenyl)	4.6	80	1,2
1560	44.43	1-dodecanoic acid	6.5	>95	1,2,3
1573	44.91	2(5H)-furanone, 5-methyl-5phenyl	1.6	70	1,2
1616	46.38	1-octadecanol	4.1	90	1,2,3
1631	46.91	phenol, 4-(2,2,3,3- tetramethylbutyl)	6.8	70	1,2
1660	47.83	branched $C_{13}$ acid	1.1	90	1,2
1671	48.16	4-nonyl-phenol	0.3	90	1,2
1682	48.32	nonyl-phenol	0.8	90	1,2
	48.55	long chain alkylphenol	0.2		F2
	48.6	long chain alkylphenol	1.3		F2
1690	48.82	1-tetradecanoic acid	9.4	>95	1,2,3
1722	49.93	benzenemethanol, alpha-phenyl	4.8	60	1,2
1724	50.02	1-pentadecanoic acid	7.3	>95	1,2,3
1812	53.35	1-hexadecanoic acid	72.6	>95	1,2,3
1913	57.72	$C_{31}$ n-alkane	4.9	>95	1,2,3
1958	59.56	1-octadecanoic acid	53.1	>95	1,2,3
19 <b>87</b>	60.75	pthalate compound	22.3	90	1,2
2003	61.53	$(C_{20}H_{30}O_4)$	32.5	90	1,2

# Table B2.Compounds Identified in the Whittier Narrows WastewaterTreatment Plant Secondary Effluent (4/86) by GC/MS (Continued)

#### Table B2. Compounds Identified in the Whittier Narrows Wastewater Treatment Plant Secondary Effluent (4/86) by GC/MS (Continued)

Scan No.	RT (minutes)	ID Compound Name or Formula	Conc. (µg/L)	% Confidence in ID	Method of ID
2109	62.51	pthalate compound	15.0	90	1,2
2380 -	78.14	pthalate compound $C_{15} - C_{33}$ n-alkanes	8.6 -	90 >95	1,2 3

Key:

1.	manual interpretation of MS data
2.	computerized matching of MS data
3.	GC retention time matched with known standards
ND	not determined because peaks are too broad

confidence in ID is a personal judgement %

concentrations evaluated based on area response of similar classes of compounds.

(is) internal standard

Scan	RT	ID Compound	Conc.	% Confidence	Method
Number	(minutes)	Name or Formula	(µg/L)	in ID	of ID
	<u>````</u>	······			· · · · · · · · · · · · · · · · · · ·
244		decane (is)	ND	>95	1,2,3
267		chloroform	ND	>95	1,2,3
282		methyl benzene	ND	95	1,2
293		bromochloromethane	ND	>95	1,2,3
383		1,4 dimethyl benzene	ND	90	1,2
522	10.33	benzene, 1-methyl-3- (1-methylethyl)	2.1	90	1,2
658	14.56	tetradecane (is)	10.0	>95	1,2,3
780	17.77	$C_{10}H_{16}O$	5.2	60	1
899	22.23	cyclohexanol,5-methyl -2-(1 methylethyl)	31.3	85	1,2
932	23.21	1-octanoic acid	165.0	>95	1,2,3
952	23.98	$C_{10}$ alcohol	10.1	90	1
997	25.32	branched Coacid	108.9	90	1,2
1089	28.39	1-nonanoic acid	179.4	>95	1,2,3
1138	30.18	aromatic alcohol	22.9	80	1,2
1169	30.84	branched $C_{10}$ acid	14.8	90	1,2
1179	31.08	branched C10 acid	3.1	90	1,2
1203	32.39	hexadecanal	4.9	70	1,2
1212	32.67	phenol	17.8	>95	1,2,3
1230	33.34	branched $C_{10}$ acid	1.9	90	1,2
1260	34.17	1-decanoic acid	148.0	>95	1,2,3
1271	34.64	p-cresol	207.7	>95	1,2,3
1277	34.87	m-cresol (is)	8.6	>95	1,2,3
1416	39.45	1-undecanoic acid	89.1	>95	1,2,3
1463	40.85	1-hexadecanol	1.3	90	1,2,3
1531	43.44	1-H-indole	14.3	90	1,2
1558	44.27	1-dodecanoic acid	78.3	>95	1,2,3
1615	46.32	1-octadecanol	6.2	90	1,2,3
1630	46.83	phenol 4-(1,1,3,3- tetramethyl-butyl	56.5	90	1,2
1651	47.38	benzene acetic acid	13.8	60	1,2
1671	48.23	alkyl phenol	31.4	80	1,2
1680	48.59	nonyl-phenol	91.2	90	1,2
1690	48.79	1-tetradecanoic acid	109.1	>95	1,2,3
1700	49.05	4-dodecyl phenol	39.2	90	1,2
1789	52.21	1H-indole,2,3-dihydro 4-methyl	4.3	80	1,2

# Table B3Compounds Identified in the Florida Waste Water TreatmentTreatment Plant Secondary Effluent (4/86) by GC/MS

Scan	RT	ID Compound	Conc.	% Confidence	Method
Number	(minutes)	Name or Formula	(µg/L)	in ID	of ID
1812	53.45	1-hexadecanoic acid	1052.4	>95	1,2,3
1837	54.33	branched $C_{16}$ or $C_{17}$ acid	127.1	90	1,2
1870	54.70	branched $C_{16}$ or $C_{17}$ acid	68.7	90	1,2
1913	57.68	$C_{31}$ n-alkane	18.0	90	1,2,3
1959	59.58	1-octadecanoic acid	248.0	>95	1,2,3
1987	60.74	1-nonadecanoic acid	281.1	>95	1,2,3
2380	77.95	pthalate compound	10.6	90	1,2
3342	120.10	cholesterol isomer	18.0	90	1,2
-	-	$C_{15} - C_{33}$ n-alkanes	-	>95	3

### Table B3 Continued

Key:

1.	manual interpretation of MS data
2.	computerized matching of MS data
3.	GC retention time matched with known standards
ND	not determined because peaks are too broad
%	confidence in ID is a personal judgement
-	concentrations evaluated based on area response of similar
	classes of compounds.

(is) internal standard

ures B1 and B2 are the GC and GC/MS for the Whittier Narrows sample and Figures B3 and B4 are the corresponding figures for the Florida wastewater treatment plant. The large ECD response is quite noticeable for the Whittier Narrows sample (Figure B1). The most striking feature about the Florida plant chromatograph (Figure B3) is that it is primarily composed of fatty acids.

Figures B5 and B6 represent the gas chromatographs of fractions 1 and 2 of the Florida plant. The fraction 1 chromatograph shows a biomodal series of n-alkanes. The lighter series centered at  $C_{18}$ represents diesel fuel contamination. The heavier series with  $C_{29}$ ,  $C_{31}$ and  $C_{33}$  n-alkane contributions is most likely of biogenic origin. These aliphatic hydrocarbons were not identifiable by GC/MS (Figure B4) because of carryover from neighboring higher concentration compounds. The GC shown in Figure B5 however eliminates (by silica gel fractionation) many of these interfering compounds (fatty acids) and allows for GC analysis at higher sensitivities. Figure B6 (fraction w) clearly shows the surfactant series of compounds present in the extract. These surfactants are long chain alkyl phenolics. Again this chromatograph was run at higher sensitivities than Figures B3 and B4 after silica get fractionation.

The compounds which were identified by GC/MS for the Whittier Narrows and Florida plants are presented in Tables B2 and B3, respectively. Table 12 is a similar listing for the San Diego Wastewater Treatment Plant. There are several similarities and differences between the treatment plants. First, the San Diego and Whittier Nar-

Date	EBMUD Treatment Plant (mg/L)	MVSD Treatment Plant (mg/L)
4/84	5.15	11.21
7/84	6.98	8.23
	7.41	
10/84	6.64	11.41
11/84	3.78	6.98

## Table B4 Gravimetric Data from other Activated Sludge Plants

Key:

EBMUD	=	East Bay Municipal
MVSD	=	Mountain View Sanitation District



Fig. B1 GC of Whittier Narrows Wastewater Treatment Plant total extract. Axes are labeled for the FID. See Figure B2 and Table B2 for compound ID. GC conditions as previously described.

.

261







Fig. B2 GC/MS of Whitter Narrows Wastewater Treatment Plant Total extract. See Table B2 for compound ID.



Fig. B4 GC/MS of Florida Wastewater Treatment Plant total extract. See Table B3 for Compound ID.



Fig. B5 GC of Fraction 1 of the Florida Wastewater Treatment Plant extract. Aliphatic n-alkanes are labeled by the number of carbon atoms. Axes are labeled for the FID. GC conditions as previously described.



Fig. B5 GC of Fraction 1 of the Florida Wastewater Treatment Plant extract. Aliphatic n-alkanes are labeled by the number of carbon atoms. Axes are labeled for the FID. GC conditions as previously described. (Continued)



Fig. B6 GC of Fraction 2 of the Florida Wastewater Treatment Plant extract. Axes are labeled for the FID. GC Condition as previously described.

rows plants have comparable concentrations of fatty acids, whereas the Florida plant has much larger values. Although this observation is probably dependent on the treatment methodologies of the three plants, it must be partly attributable to the differing influents to the plants. The Florida influent is nearly 100% domestic, whereas the other two plants receive some industrial input (the fatty acids are of domestic origin).

Second, the Florida plant contains no dichlorobenzenes (DCB's) which at the other two plants probably result from industrial effluents. Third, all three wastewater treatment plants contain long chain alkyl phenolic surfactants. A phosphoric acid based surfactant was also found in the Whittier Narrows extract (phosphoric acid-tributyl-ester). Fourth, both water hyacinth based plants showed large concentrations (35.5  $\mu$ g/l in San Diego and 18.0  $\mu$ g/l in Florida) of the  $C_{31}$  n-alkane which most likely leaches off the plant leaf waxes.

Fifth, the Florida plant extract showed large concentrations of p-cresol (208  $\mu$ g/l), and phenol (19  $\mu$ g/l) which is somewhat surprising. It is possible that these compounds arise from solvents or paints used on the premises of the amusement park.

In summary, the effluents from the three plants show more similarities than differences. The differences are more likely due to influent variations than to the efficiencies of activated sludge treatment versus aquaculture treatment. Although the lower gravimetric value for the Whittier Narrows sample (2.61 mg/L) indicates high efficiency for activated sludge treatment, this may only be coincidental. In previously analyzed samples from other activated sludge based treatment plants, the gravimetric extracts showed much variability (Table B4).

-